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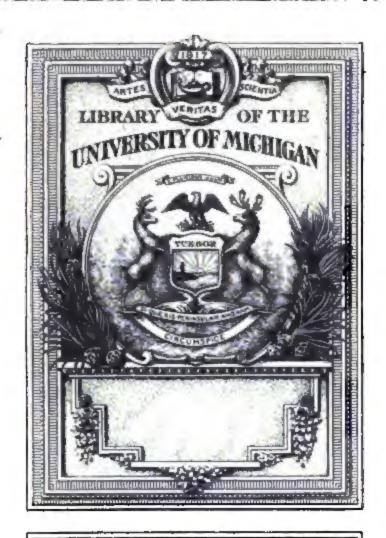
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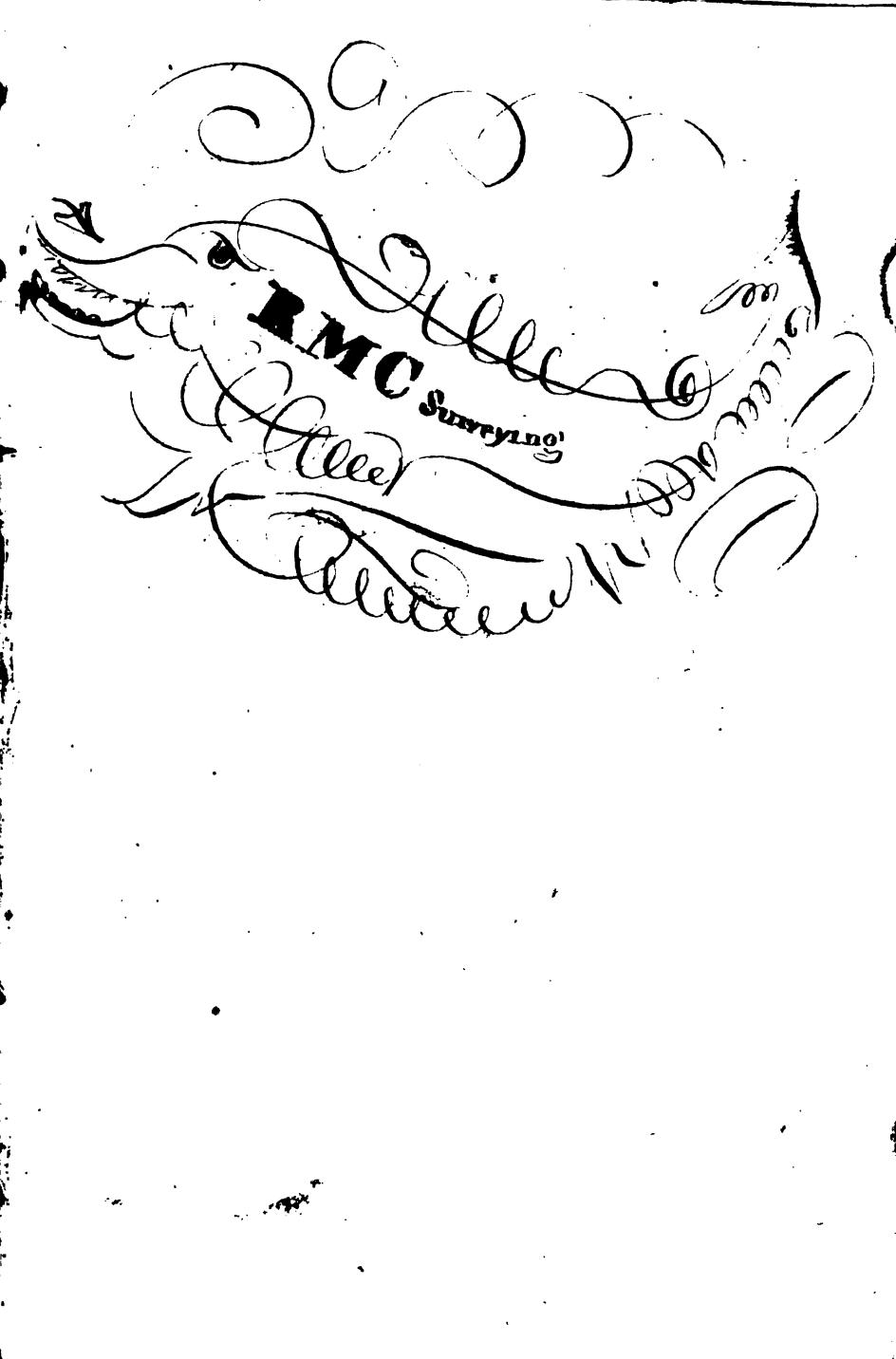
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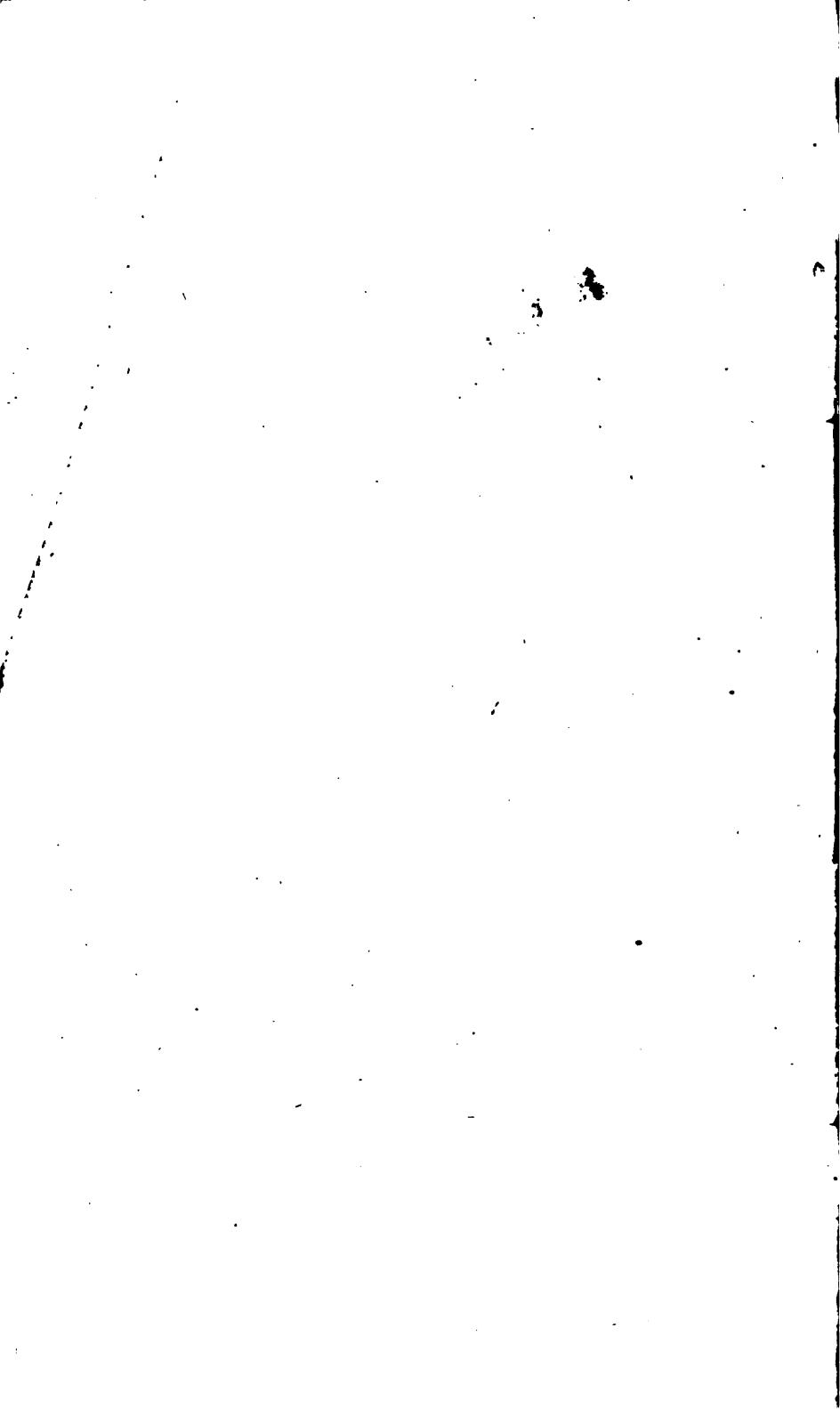
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THE

THEORY AND PRACTICE

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SURVEYING;

CONTAINING

All the Instructions requisite for the skilful practice of this Art.

27

ROBERT GIBSON.

ILLUSTRATED BY COPPER-PLATES:

THE

WHOLE CORRECTED, NEWLY ARRANGED, AND GREATLY ENLARGED;
WITH USEFUL SELECTIONS,

AND A NEW SET OF ACCURATE

MATHEMATICAL TABLES.

By D. P. ADAMS,
TRACKER OF THE MATERIATION

NEW-YORK:

PUBLISHED BY EVERT DUYCKINCK, NO. 102 PRARL-STREET.

G. Long, printer.

1814.

District of Nord-York, ex.

BE IT REMEMBERED, That on the twenty-eighth day of March, in the thirty-fifth year of the Independence of the United States of America, Evert Dwyckinck, of the said district, hath deposited in this office the title of a book, the right whereof he claims as proprietor, in the words following, to wit:

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CHARLES CLINTON,

Clerk of the District of New York.

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J. J. 36 N. 8. Y

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EXPLANATION

Of the Mathematical Characters used in this Work.

- + signifies plus, or addition.
- . . minus, or subtraction.
- × or . , . multiplication.
- . division.
- : 4:: proportion.
- equality.
- √ . . square root.
- . . cube root, &c.
- co. diff. between two numbers when it is not known which is the greater.

Thus,

- 5 + 3, denotes that 3 is to be added to 5.
- 6 2, denotes that 2 is to be taken from 6.
- 7×3 , or $7 \cdot 3$, denotes that 7 is to be multiplied by 3.
- 8 4, denotes that 8 is to be divided by 4.
- 2:3::4:6, shows that, 2 is to 3 as 4 is to 6.
- 6 + 4 = 10, shows that the sum of 6 and 4 is equal to 10.
- √ 3, or 3½, denotes the square root of the number 3.
- $\frac{3}{4}$ 5, or $5\frac{1}{3}$, denotes the cube root of the number 5.
- 72, denotes that the number 7 is to be squared.
- 83, denotes that the number 8 is to be cubed.

&c.

THE

THEORY AND PRACTICE

03

SURVEYING.

THE word Surveying, in the Mathematics, signifies the art of measuring land, and of

delineating its boundaries on a map.

The Surveyor, in the practice of this art, directs his attention, at first, to the tracing and measuring of lines; secondly, to the position of these lines in respect to each other, or the angles formed by them; thirdly, to the plan, or representation of the field, or tract, which he surveys; and fourthly, to the calculation of its area, or superficial content. When this art is employed in observing and delineating Coasts and Harbours, in determining their variation of the Compass, their Latitude, Longitude and soundings, together. with the bearings of their most remarkable places from each other, it is usually denominated Maritime Surveying. This branch of Surveying, however, demands no other qualifications than those, which should be thoroughly acquired by every Land-Surveyor, who aspires to the character of an accomplished and skilful practitioner. Surveying, therefore, requires an intimate acquaintance with the several parts of the Mathematics, which are here inserted as an introduction to this treatise.

PART 1.

Containing Decimal Fractions, Involution and Evolution, the Nature and Use of Logarithms, Geometry and Plane Trigonometry.

SECTION I.

DECIMAL FRACTIONS.

If we suppose unity or any one thing to be divided into any assigned number of equal parts, this number is called the denominator; and if we chuse to take any number of such parts less than the whole, this is called the numerator of a fraction.

The numerator, in the vulgar form, is always written over the denominator, and these are separated by a small line thus $\frac{1}{2}$, or $\frac{1}{4}$; the first of these is called three-fourths, and the latter five-eighths of an inch, yard, &c. or of whatever the whole thing originally consisted: the 4 and the 8 are the denominators, showing into how many equal parts the unit is divided; and the three and the five are the numerators, showing how many of those parts are under consideration.

Fractions are expressed in two forms, that is,

either vulgarly or decimally.

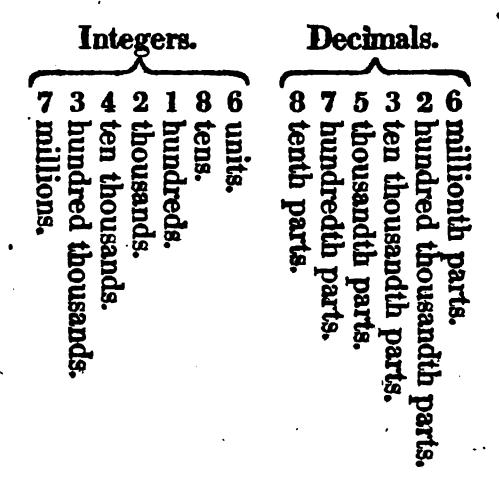
All fractions whose denominators do not consist of a cipher, or ciphers, set after unity, are called vulgar; and their denominators are always written under their numerators. The treatment of these, however, would be foreign to our present purpose. But fractions whose denominators consist of an unit prefixed to one or more ciphers, are called decimal fractions; the numerators of which are written without their denominators, and are distinguished from integers by a point prefixed: thus $\frac{2}{10}$, $\frac{4^{\circ}}{100}$ and $\frac{17^{\circ}}{1000}$, in the decimal form, are expressed by .2.42.172.

The denominators of such fractions consisting always of an unit, prefixed to as many ciphers as there are places of figures in the numerators, it follows, that any number of ciphers put after those numerators, will neither increase nor lessen, their value: for \$\frac{1}{10}\$, \$\frac{1}{100}\$ and \$\frac{1800}{1800}\$ are all of the same value, and will stand in the decimal form thus .3 .30 .300; but a cipher, or ciphers prefixed to those numerators lessen their value in a tenfold proportion: for \$\frac{1}{10}\$, \$\frac{1}{100}\$ and \$\frac{1600}{1600}\$, which in the decimal form we denote by .3 .03 and .003, are fractions, of which the first is ten times greater than the second; and the second, ten times greater than the third.

Hence it appears, that as the value and denomination of any figure, or number of figures, in common arithmetic is enlarged, and becomes ten, or an hundred, or a thousand times greater, by placing one or two, or three ciphers after it; so in decimal arithmetic, the value of any figure, or number of figures, decreases, and becomes ten, or a hundred, or a thousand times less, while the denomination of it increases, and becomes so many times greater, by prefixing one, or two, or three ciphers to it: and that any number of ciphers, before an integer, or after a decimal fraction, has no effect in changing their values.

DECIMAL FRACTIONS.

SCALE OF NOTATION.



ADDITION OF DECIMALS.

Write the numbers under each other according to the value or denomination of their places; which position will bring all the Decimal points into a column, or vertical line, by themselves. Then, beginning at the right hand column of figures, add in the same manner as in whole numbers, and put the decimal point, in the sum directly beneath the other points.

EXAMPLES.

Add 4.7832 3.2543 7.8251 6.03 2.857 and 3.251 together. Place them thus,

4.7832

3.2543

7,8251

6,03

2.857

3.251

Sum=28,0006,

Add 6.2 121.306 .75 2.7 and .0007 together. 121.306

.75 2.7 .0007

Sum = 130.9567

What is the sum of 6.57 1.026 .75 146.5 8.7 526. 3.97 and .0271?
Answer 693.5431.

What is the sum of 4.51 146.071 .507 .0006 132. 62.71 .507 7.9 and .10712?

Answer 354.31272.

SUBTRACTION OF DECIMALS.

Write the figures of the subtrahend beneath those of the minuend according to the denomination of their places, as directed in the rule of addition; then, beginning at the right hand, subtract as in whole numbers, and place the decimal point in the difference exactly under the other two points.

EXAMPLES.

From 38.765 take 25.3741 25.3741

Difference =13.3909

From 2.4 take .8472 .8472

Diff = 1.5528

From 71.45 take 8.4837248.

Difference = 62.9662752.

From 84 take 82.3412.

Diff. = 1.6588.

MULTIPLICATION OF DECIMALS.

Set the multiplier under the multiplicand without any regard to the situation of the decimal point; and having multiplied as in whole numbers, cut off as many places for decimals in the product, counting from the right hand towards the left, as there are in both the multiplicand and multiplier: but if there be not a sufficient number of places in the product, the defect may be supplied by prefixing ciphers thereto.

For the denominator of the product being an unit, prefixed to as many ciphers, as the denominators of the multiplier and multiplicand contain of ciphers, it follows, that the places of decimals in the product, will be as many as in the numbers

from whence it arose.

EXAMPLES.

Multiply 121.6 by 2.76 2.76

7296 8512 **24**32

Product = 335.616

Multiply .0089789 by 1085 Product = 9.7421065

Multiply .248723 by .13587 Product = .03379399401.

DIVISION OF DECIMALS.

Divide as in whole numbers; observing that the divisor and quotient together must contain as many decimal places as there are in the dividend. If, therefore, the dividend have just as many places of decimals as the divisor has, the quotient will be a whole number without any decimal figures. If there be more places of decimals in the dividend, than there are in the divisor, point off as . many figures in the quotient for decimals, as the decimal places in the dividend exceed those in the divisor; the want of places in the quotient being supplied by prefixing ciphers. But if there be more decimal places in the divisor, than in the dividend, annex ciphers to the dividend, so that the decimal places here may be equal, in number, to those in the divisor; and then the quotient will be a whole number, without fractions.

When there is a remainder, after the division has been thus performed, annex ciphers to this remainder, and continue the operation till nothing remains, or till a sufficient number of decimals shall be found in the quotient.

DECIMAL FRACTIONS:

EXAMPLES.

Divide .144 by .12

.12).144(1.2 = quotient.

O

Divide 63.72413456922 by 2718 2718)63.72413456922(.02344522979 = quotient.

There being 11 decimal figures in the dividend, and none in the divisor, 11 figures are to be cut off in the quotient; but as the quotient itself consists of but 10 figures, prefix to them a cipher to complete that number.

Divide 1.728 by .012 .012)1.728(144=quotient.

Because the number of decimal figures in the divisor and dividend, are alike, the quotient will be integers.

Divide 2 by 3.1416

3.1416)2.0000,0(0.636618+=quotient.

1 8849 6

	040 248
	7920 8496
_	94240 88496
	57440 31416
•	260240 251228
	9012+ C

In this example there are four decimal figures in the divisor, and none in the dividend; therefore, according to the rule, four ciphers are annexed to the dividend, which in this condition, is yet less than the divisor. A cipher must then be put in the quotient, in the place of integers, and other ciphers annexed to the dividend; and the division being now performed, the decimal figures of the quotient are obtained.

Divide 7234.5 by 6.5 Quotient=1113.

Divide 476.520 by .423 ——=1126.5+

Divide .45695 by 12.5 ——=.0365+

Divide 2.3 by 96 ——=.02395+

Divide 87446071 by .004387 —=19933000000.

Divide .624672 by 482 ——=.001296.

REDUCTION OF DECIMALS.

RULE I.

To reduce a Vulgar Fraction to a Decimal of the same value.

Having annexed a sufficient number of ciphers, as decimals, to the numerator of the vulgar fraction, divide by the denominator; and the quotient thence arising, will be the decimal fraction required.

EXAMPLES.

Reduce \(\frac{1}{4} \) to a decimal fraction. \(\frac{1}{4} \) \(\frac{1}{3} \).00

.75=decimal required.

For \(\frac{3}{4}\) of one acre, mile, yard, or any thing, is equal to \(\frac{1}{4}\) of 3 acres, miles, yards, &c. there-

fore if 3 be divided by 4, the quotient is the answer required.

Reduce ? to a decimal fraction. Answer .4

Reduce $\frac{12}{25}$ - - - .48

Reduce $\frac{33}{218}$ - - . .1146789

Reduce 3 - - - .7777+

Reduce $\frac{24}{3}$ - - - .9130434+

Reduce 1, 1, 1, 1, and so on to 10, to their corresponding decimal fractions; and in this operation the various modes of interminate decimals may be easily observed.

RULE II.

To reduce Quantities of the same, or of different Denominations to Decimal Fractions of higher denominations.

If the given quantity consist of one denomination only, write it as the numerator of a vulgar fraction; then consider how many of this make one of the higher denomination, mentioned in the question, and write this latter number under the former, as the denominator of a vulgar fraction. When this has been done, divide the numerator by the denominator, as directed in the foregoing rule, and the quotient resulting will be the decimal fraction required.

But if the given quantity contain several denominations, reduce them to the lowest term for the numerator; reduce likewise that quantity, whose fraction is sought, to the same denomination for the denominator of a vulgar fraction; then divide as before directed.

EXAMPLES.

Reduce 9 inches to the Decimal of a foot,

The foot being equal to 12 inches, the vulgar fraction will be $\frac{1}{12}$; then 12)9.00

.75=decimal frac-[tion required.

Reduce 8 inches to the decimal of a yard.
8 inches.

1 yard \times 3 \times 12 = 36 inches. 36)8.0(.22 + = Answer. 72 80 72

Reduce 5 furlongs 12 perches to the decimal of a mile.

1 mile 5 furlongs
40

8 fur. 200
40 = vulgar fraction,
320 per.

1600

Reduce 21 minutes 54 seconds to the decimal of a degree. Ans. .365
Reduce .056 of a pole to the decimal of an Acre, Ans. .00035

Reduce 13 cents to the dccimal of an Eagle. Ans. .013

Reduce 14 minutes to the decimal of a day. Ans. .00972+

Reduce 3 hours 46 minutes to the decimal of a week. Ans. .0224206+

RULE III.

To find the value of Decimal Fractions in terms of the lower denominations.

Multiply the given decimal by the number of the next lower denomination, which makes an integer of the present, and point off as many places at the right hand of the product, for a remainder, as there are figures in the given decimal. Multiply this remainder by the number of the next inferior denomination, and point off a remainder, as before. Proceed in this manner through all the parts of the integer, and the several denominations, standing on the left hand, are the value required.

EXAMPLES.

Required the value of .3375 of an acre.

 $\frac{4 = \text{number of roods}}{\text{[in an acre.}}$ $\frac{1.3500}{40 = \text{number of percha}}$ $\frac{40 = \text{number of percha}}{\text{[es in a roods]}}$

The value, therefore, is 1 rood 14 perches.

What is the value of .6875 of a yard?

3=number of feet in a [yard.

2.0625

12=number of inches in a foot.

.7500

12=number of lines in [an inch.

9.0000

The answer here is 2 feet 9 lines.

What is the value of .084 of a furlong? Ans. 3 per. 1 yd. 2 ft. 11 in.

What is the value of .683 of a degree? Ans. 40

m. 58 sec. 48 thirds.

What is the value of .0053 of a mile? Ans. 1 per. 3 yds. 2 ft. 5 in.+

What is the value of .036 of a day? Ans. 51' 50" 24".

PROPORTION

IN DECIMAL FRACTIONS.

Having reduced all the fractional parts in the given quantities to their corresponding decimals, and having stated the three known terms, so that the fourth, or required quantity, may be as much greater, or less than the third, as the second term is greater, or less than the first, then multiply the second and third terms together, and divide the product by the first term, and the quotient will be the answer;—in the same denomination with the third term.

EXAMPLES.

If 3 acres 3 roods of land can be purchased for 93 dollars 60 cts. how much will 15 acres 1 rood cost at that rate?

3 acs. 3 rds. = 3.75 acres. 15 acs. 1 rd. = 15.25 acres. \$93, 60 cts. = \$93.60 Then 3.75: 15.25:: 93.60: 15.25

468 00 - 1872 0 46800 9360

3.75)1427.4000(380.64=Answer. 1125

If a clock gain 14 seconds in 5 days 6 hours, how much will it gain in 17 days 15 hours? Ans. 47 seconds.

1500

If 187 dollars 85 cents gain 12 dollars 33 cents interest in a year, at what rate per cent is this interest? Ans. 6.56+

SECTION II.

INVOLUTION AND EVOLUTION.

Involution is the method of raising any number, considered as the root, to any required power.

Any number, whether given, or assumed at pleasure, may be called the root, or first power of this number; and its other powers are the products, that result from multiplying the number by itself, and the last product by the same number again; and so on to any number of multiplications.

The index, or exponent, is the number donoting the height, or degree of the power, being always greater by one, than the number of multiplications employed in producing the power. It is usually written above the root, as in the following example, where the method of involution is plainly exhibited.

Required the fifth power of 8 } the root, or first first multiply by - - 8 } = power.

then multiply the product $64 = 8^{\circ} = \text{square}$, or by 8 [second power.

&c. $512 = 8^3 = \text{cube}$, or third power.

4096 = 8 = biquadrate 8 [or fourth power.

 $32768 = 8^s =$ Answer.

EXAMPLES FOR EXERCISE.

What is the second power of 3.05? Ans. 9.3025

What is the third power of 85.3? Answer,

620650.477

What is the fourth power of .073? Answer,

090028398241

What is the eighth power of .09? Answer, .00.00.00.0043046721

Note. When two, or more powers are multiplied together, their product is that power, whose index is the sum of the indices of the factors, or powers multiplied.

Evolution is the method of extracting any re-

quired root from any given power.

Any number may be considered as a power of some other number; and the required root of any given power is that number, which, being multiplied into itself a particular number of times, produces the given power; thus if 81 be the given number, or power, its square, or second root, is 9; because $9 \times 9 = 9^3 = 81$; and 3 is its biquadrate, or fourth root, because $3 \times 3 \times 3 \times 3 = 3^4 = 81$. Again, if 729 be the given power, and its cube root be required, the answer is 9, for $9 \times 9 \times 9 = 729$; and if the sixth root of that number be required, it is found to be 3, for $3 \times 3 \times 3 \times 3 \times 3 = 729$.

The required power of any given number, or root, can always be obtained exactly, by multiplying the number continually into itself; but there are many numbers, from which a proposed root can never be completely extracted;—yet by approximating with decimals, these roots may be found as exact as necessity requires. The roots that are found complete, are denominated rational roots, and those, which cannot be found completed, or which only approximate, are called surd, or irrational roots.

Roots are usually represented by these characters or exponents;

√, or ½ which signifies the square root; thus,

$$\checkmark$$
 9, or 9½ = 3
 \checkmark or \checkmark cube root; \checkmark 64, or 64 \checkmark = 4
 \checkmark , or \checkmark biquadrate root; \checkmark 16, or 16 \checkmark = 2 &c.

Likewise 8³ signifies the square root of 8 cubed; and, in general, the fractional indices imply, that the given numbers are to be raised to such powers as are denoted by their numerators, and that such roots are to be extracted from these powers, as are denoted by their denominators.

RULE

For extracting the Square Root.

Separate the given number into periods of two figures, by putting a point over the place of units, another over the place of hundreds, and so on, over every second figure, both toward the left hand in whole numbers, and toward the right hand in the Decimal places.—When the number of integral places is odd, the first, or left hand period, will consist of one figure only.

Find the greatest square in the first period on the left hand, and write its root on the right hand of the given number, in the manner of a quotient

figure in division.

Subtract the square, thus found, from the said period, and to the remainder annex the two figures of the next following period, for a dividend.

Double the root above mentioned for a divisor, and find how often it is contained in the said dividend, exclusive of its right hand figure, and set this quotient both in the place of the quotient and in the divisor.—The best way of doubling the root, to form each new divisor, is to add the last figure always to the last divisor, as it is done in the subsequent examples.

Multiply the whole augmented divisor by this last quotient figure, and subtract the product from the said dividend, bringing down to it the next period of the given number for a new dividend.

Repeat the same operation again; that is, find another new divisor, by doubling all the figures now found in the root; from which, and the last dividend, find the next figure of the root as before; and so on through all the periods to the last.

- Note 1. After the figures belonging to the given number are all exhausted, the operation may be continued in decimals, by annexing any number of periods or ciphers to the remainder.
- 2. The number of integral places in the root, is always equal to the number of periods in the integral part of the resolvend.
- 3. When vulgar fractions occur in the given power, or number, they may be reduced to decimals, then the operation will be the same as before dictated.

EXAMPLES.

Required the square root of 1710864.

Required the square root of 16007.3104.

126.52= A nswer.

EXAMPLES FOR EXERCISE.

Required the square root of 298116. Ans. 546, Required the square root of 348.17320836. Ans. 18.6594.

Required the square root of 17.3056. Ans. 4.16. Required the square root of .000729. Ans. .027. Required the square root of 17% Ans. 4.168333+

A GENERAL RULE

For extracting any Root whatever.

Find by trial a number, which, when involved to the power denoted by the index of the required root, shall come nearest to the given number, whether greater or less; and let that number be called the assumed root, and when thus involved, the assumed power.

Let the given power, or number be repre-	la
sented by	G.
the index, or exponent, in the question by	X.
the assumed power, by	A.
the assumed root, by	Q.
and the required root by	R.

Then $\overline{X+1} \times A + \overline{X-1} \times G : \overline{X+1} \times G + \overline{X-1} \times A :: Q : R.$

That is, as the sum of X+1 times A and X—1 times G,

is to the sum of X+1 times G and X-1 times A,

so is the assumed root, Q,

to the required root, R,—nearly; and the operation may be repeated as many times as we chuse, by using always the root last found for the assumed root, and this, involved according to the given index, for the assumed power.*

EXAMPLES.

1. Required the Cube root of 789.

This is a very general approximating rule," says Dr. Hutton, "of which that for the cube root is a particular case, and is the best adapted for practice and for memory, of any that I have yet seen. It was first discovered in this form by myself, and the investigation and use of it were given at large in my Tracts—page 45 &cc."

Here
$$G=789$$
, $X=3$, $Q=9$, $A=9^{2}=729$, $X+1=4$ and $X-1=2$.

Then

4494

4614::9:9.240+

4494)41526(9.2403+[Ans. 40446

10800 8988

> 18120 17976

> > 144**0**0 13482

> > > 918 &c.

In the foregoing example the answer is strictly correct in its integral part and also in the three first decimal places; but if more decimals were wanted, and if their exactness were likewise requisite, the present answer might be taken for the assumed root, and the whole operation should be repeated.

2. Required the biquadrate root of 2.0743.

Here G=2.0743, Q=1.2, A= $\overline{1.2}$ =2.0736, X=4, $\overline{X+1}$ =5, and $\overline{X-1}$ =3.

And $5 \times 2.0736 = 10.3680$ $5 \times 2.0743 = 10.3715$ $3 \times 2.0743 = 6.2229$ $3 \times 2.0736 = 6.2208$

Then 16.5909 : 16.5923

[:: 1.2: 1.2001+Ans.

Required the fifth root of 21035.8 Ans. =7.3213±
Required the sixth root of 21035.8 Ans. =5.2540±
Required the cube root of 999 Ans. =9.9966±
Required the fourth root of 97.41 Ans. =3.1416
Required the cube root of .037 Ans. =.33322±
Required the cube root of 2 Ans. =1.2599±
Required the seventh root of 21035.8 Answer=
[4.1454:

SECTION III.

OF LOGARITHMS.

LOGARITHMS are a series of numbers, so contrived, that by them the work of multiplication may be performed by addition; and the operation of division may be done by subtraction. Or,—Logarithms are the indices, or series of numbers in arithmetical progression, corresponding to another series of numbers in geometrical progression. Thus,

(0,1,2,3, 4, 5, 6,&c. Indices or Logarithms. (1,2,4,8,16,32,64,&c. Geometrical progression. Or,

§ 0, 1, 2, 3, 4, 5, 6, &c. Ind. or Log.

(1, 3, 9, 27, 81, 243, 729, &c. Geometrical Series. Or.

\(\) 0, 1, 2, 3, 4, 5, 6,&c.I.orL. \(\) 1, 10, 100, 1000, 10000, 100000, 1000000, &c. Geometrical series,—where the same indices serve equally for any Geometrical series, or progression.

Hence it appears that there may be as many kinds of indices, or logarithms, as there can be taken kinds of geometrical series. But the Logarithms most convenient for common uses are those adapted to a geometrical series increasing in a ten-fold progression, as in the last of the foregoing

examples.

In the geometrical series 1, 10, 100, 1000, &c. if between the terms 1 and 10, the numbers 2, 3, 4, 5, 6, 7, 8, 9 were interposed, indices might also be adapted to them in an arithmetical progression, suited to the terms interposed between 1 and 10, considered as a geometrical progression. Moreover, proper indices may be found to all the numbers, that can be interposed between any two terms of the Geometrical series.

But it is evident that all the indices to the numbers under 10, must be less than 1; that is, they must be fractions. Those to the numbers between 10 and 100, must fall between 1 and 2; that is, they are mixed numbers, consisting of 1 and some fraction. Likewise the indices to the numbers between 100 and 1000, will fall between 2 and 3; that is, they are mixed numbers, consisting of 2 and some fraction; and so of the other indices.

Hereaster the integral part only of these indices will be called the Index; and the fractional part will be called the Logarithm. The computation of these fractional parts, is called making Logarithms; and the most troublesome part of this work is to make the Logarithms of Prime Numbers, or those which cannot be divided by any other numbers than themselves and unity.

RULE

For Computing the Logarithms of Numbers.

Let the sum of its proposed number and the next less number be called A. Divide 0.8685889638׆

† The number 0.86858896384 is the quotient of 2 divided by 2.302585093, which is the logarithm of 10, according to the first

by A, and reserve the quotient. Divide the reserved quotient by the square of A, and reserve this quotient. Divide the last reserved quotient by the square of A, reserving the quotient still; and thus proceed as long as division can be made. Write the reserved quotients orderly under one another, the first being uppermost. Divide these quotients respectively by the odd numbers 1, 3, 5, 7, 9, 11, &c.; that is, divide the first reserved quotient by 1, the second by 3, the third by 5, the fourth by 7, &c. and let these quotients be written orderly under one another; add them together, and their sum will be a logarithm. To this logarithm add the logarithm of the next less number, and the sum will be the logarithm of the number proposed.

form of Lord Napier, the inventor of logarithms. The manner in which Napier's logarithm of 10 is found, may be seen in most books of Algebra, but it is here omitted, because students of Surveying are too generally unacquainted with the principles of that science, and the subject is too extensive for the present treatise. Those, however, who have not an opportunity for entering thoroughly into this subject, may with more propriety grant the truth of one number, and thereby be enabled to try the correctness of any logarithm in the tables, than receive those tables, as truly computed, without any means of examining their accuracy.

EXAMPLE I.

Required the Logarithm of the number 2.

Here the next less number is 1, and 2+1=3= A. and A², or $3^2=9$; then

3)0.868588964

 $(9)0.289529654 \div 1 = 0.289529654$

9) $0.032169962 \div 3 = 0.010723321$

9) $0.003574440 \div 5 = 0.000714888$

9) $0.000397160 \div 7 = 0.000056737$

9) $0.000044129 \div 9 = 0.000004903$

9) $0.000004903 \div 11 = 0.000000446$

 $-9)0.000000545 \div 13 = 0.000000042$

 $0.000000061 \div 15 = 0.000000004$

To this Logarithm 0.301029995 add the Logarithm of 1 = 0.000000000

Their Sum = 0.301029995 = Log. of 2.

The manner in which the division is here carried on, may be readily perceived by dividing, in the first place, the given decimal by A, and the succeeding quotients by A²; then letting these quotients remain in their situation, as seen in the example, divide them respectively by the odd numbers, and place the new quotients in a column by themselves. By employing this process, the operation is considerably abbreviated.

EXAMPLE 2.

Required the Logarithm of the number 3.

Here the next less number is 2; and 3+25=A, and $A^2=25$.

5)0.868588964

 $25)0.173717793 \div 1 = 0.173717793$

 $25)0.006948712 \div 3 = 0.002316237$

 $25)0.000277948 \div 5 = 0.000055599$

 $25)0.000011118 \div 7 = 0.000001588$

 $25)0.000000445 \div 9 = 0.000000049$

 $0.000000018 \div 11 = 0.000000002$

To this Logarithm 0.176091259 add the Logarithm of 2=0.301029995

Their Sum = 0.477121254 = Log. of 3.

Then, because the sum of the logarithms of numbers, gives the logarithm of their product; and the difference of the logarithms, gives the logarithm of the quotient of the numbers: from the two preceding logarithms, and the logarithm of 10, which is 1, a great many logarithms can be easily made, as in the following examples.

Example 3. Required the Logarithm of 4.

Since $4=2\times2$, then to the Logarithm of

2 = 0.301029995

add the Logarithm of 2=0.301029995

The sum=Logarithm of 4=0.602059990

Example 4. Required the Logarithm of 5.

10÷2 being=5, therefore from the Log. of 10=1.000000000 subtract the Log. of 2=0.301029995

the remainder is the Log. of 5=0.698970005

Example 5. Required the Logarithm of 6.

 $6=3\times2$, therefore to the Logarithm of 3=0.477121254 add the Logarithm of 2=0.301029995

their sun=Log. of 6=0.778151249

Example 6. Required the Logarithm of 8.

8=2³, therefore multiply the Logarithm of 2=0.301029995 by 3

The product = Log. of 8 = 0.903089985

Example 7. Required the Logarithm of 9.

9=3, therefore the Logarithm of 3=0.477121254 being multiplied by 2

the product=Log. of 9=0.954242508

Example 8. Required the Logarithm of 7.

Here the next less number is 6, and 7+6=13= A, and $A^2=169$. 13)0.868588964

 $169)0.066814536 \div 1 = 0.066814536$

 $169)0.000395352 \div 3 = 0.000131784$

 $169)0.000002339 \div 5 = 0.000000468$

 $0.000000014 \div 7 = 0.000000002$

To this Logarithm=0.066946790 add the Log. of 6=0.778151249

Their sum=
$$0.845098039$$
=Log. of 7.

of 12
of 14
of 15 is equal to the sum
of 3 and 4.
of 3 and 5.
of 16
of 18
of 20
of 20

of 4 and 5.

The Logarithms of the prime numbers, 11, 13, 17, 19, &c. being computed by the foregoing general Rule, the Logarithms of the intermediate numbers are easily found by composition and division. It may, however, be observed, that the operation is shorter in the larger prime numbers; for when any given number exceeds 400, the first quotient, being added to the Logarithm of its next lesser number, will give the Logarithm sought, true to 8, or 9 places; and therefore it will be very easy to examine any suspected Logarithm in the Tables.

For the arrangement of Logarithms in a Table, the method of finding the Logarithm of any natural number, and of finding the natural number corres-

ponding to any given Logarithm, therein: likewise for particular rules concerning the Indices, the reader will consult Table 1, with its explanation, at the end of this Treatise.

MULTIPLICATION,

Two, or more numbers being given, to find their product by Logarithms.

RULE.

Having found the Logarithms of the given numbers in the Table, add them together, and their sum is the Logarithm of the product; which Logarithm, being found in the Table, will give a na-

tural number, that is, the product required.

Whatever is carried from the decimal part of the Logarithm is to be added to the affirmative indices; but subtracted from the negative. Likewise the indices must be added together, when they are all of the same kind, that is, when they are all affirmative, or all negative; but when they are of different kinds, the difference must be found, which will be of the same denomination with the greater.

Example 1. Required the product of 86.25 multiplied by 6.48

Log. of 86.25 = 1.935759Log. of 6.48 = 0.811575

Product = 558.9 = 2.747334

Example 2. Required the product of 46.75 and .3275

Log. of 46.75 = 1.669782 Log. of .3275 = -1.515211

Product = 15.31 + = 1.184993

Example 3. Required the product of 3.768, 2.053 and .007693.

Log. of 3.768 = 0.576111Log. of 2.053 = 0.312389Log. of .007693 = -3.886096

 $Product = .05951 \times = -2.774596$

Example 4. Required the product of 27.63, 1.859, .7258 and 0.3591.

Log. of 27.63 = 1.441381Log. of 1.859 = 0.269279Log. of .7258 = -1.860817Log. of .03591 = -2.555215

Product nearly=1.339 = 0.126692

DIVISION.

Two numbers being given, to find how many times one is contained in the other, by Logarithms.

RULE.

From the Logarithm of the Dividend subtract the Logarithm of the Divisor, and the remainder will be the Logarithm, whose corresponding natural number will be the Quotient required.

In this operation, the Index of the Divisor must be changed from affirmative to negative, or from negative to affirmative; and then the difference of the affirmative and negative Indices must be taken for the index to the Logarithm of the Quotient. Likewise when one has been borrowed in the left hand place of the Decimal part of the Logarithm, add it to the Index of the Divisor, if affirmative; but subtract it, if negative; and let the

Index, thence arising, be changed and worked with, as before.

Example 1. Divide 558.9 by 6.48. Log. of 558.9 =2.747334 Log. of 6.48 =0.811575

Quotient = 86.25 = 1.935759

Example 2. Divide 15.31 by 46.75. Log. of 15.31 = 1.184975Log. of 46.75 = 1.669782

Quotient = .3275 = -1.515193

Example 3. Divide .05951 by .007693. Log. of .05951 = -2.774590 Log. of .007693 = -3.886096

Quotient=7.735 = 0.888494

Example 4. Divide .6651 by 22.5. Log. of .6651 = -1.822887 Log. of 22.5 = 1.352183

Quotient = .02956 = -2.470704

PROPORTION,

Or the Rule of Three in Logarithms.

RULE.

Having stated the three given terms according to the rule in common Arithmetic, write them orderly under one another, with the signs of proportion; then add the Logarithms of the second and third terms together, and from their sum subtract the Logarithm of the first term, and the remainder will be the Logarithm of the fourth term, or Answer.

Or,—add together the Arithmetical Complement of the Logarithm of the first term, and the Logarithms of the second and third terms; the sum, rejecting 10 from the index, will be the Logarithm

of the fourth term, or term required.

N.B. The Arithmetical Complement of a Logarithm is what it wants of 10,000000, or 20,000000, and the easiest way to find it is to begin at the left hand, and subtract every figure from 9, except the last, which should be taken from 10; but if the index exceed 9, it must be taken from 19.—It is frequently used in the rule of Proportion and Trigonometrical calculations, to change Subtractions into Additions.

EXAMPLES.

1st. If a clock gain 14 seconds in 5 days 18 hours, how much will it gain in 17 days 15 hours?

5.75 days : Log.=0.759668

17.625 days :: Log.=1.246129 14 Seconds : Log.=1.146128

2.392257

Answer = 42''. 91 = 1.632589

Or thus; 5.75 days: Arith. Co. Log. = 9.240332

17.625 :: Log.=1.246129

14 Seconds: Log.= 1.146128

Answer=42''. 91 = 1.632589

2d. Find a fourth proportional to 9.485, 1.969 and 347.2.

> 98.45 Log. = 1.993216

347.2 : Log. = 2.5405801.969: Log. = 0.294246

2.834826

Answer=6.944 = 0.841610

3d. What number will have the same proportion to .8538 as .3275 has to .0131

> Log. = -2.117271.0131 :

Log. = -1.515211 Log. = -1.931356

·8538 :

-1.446567

1.366274

Answer=21.35= 1.329296

4th. Required a third proportional number to 9.642 and 4.821

> $Log_{\bullet} = 0.984167$ 9.642

Log = 0.6831374.821 : : Log. = 0.6831374,821 :

Answer=2.411 = 0.382107

INVOLUTION.

To find any proposed power of a given number by Logarithms.

Rule. Multiply the Logarithm of the given number by the Index of the proposed power, and the product will be the Logarithm, whose natural

number is the power required.

When a negative Index is thus multiplied, its product is negative, but what was carried from the decimal part of the Logarithm must be affirmative; consequently the difference is the index of the product, which difference must be considered of the same kind with the greater, or that which was made the minuend.

EXAMPLES,

1. What is the second power of 3.874?

Log. of 3.874=0.588160

Index = 2

Power required=15.01 =1.176320

2. Required the third power of the number 2.768. Log. of 2.768=0.442166

Index = 3

Answer=21.21 = 1,326498

3. Required the second power of the number .2857.

Log. of .2857 = -1.455910Index = 2

Answer=.08162=-2.911820

4. Required the third power of the number .7916.

Log. of $.791\hat{6} = -1.898506$ Index = 3

Answer = .4961 = -1.695518

EVOLUTION.

To extract any proposed Root of a given number by Logarithms.

RULE.

Find the Logarithm of the given number, and divide it by the Index of the proposed root; the quotient is a Logarithm, whose natural number is

the root-required.

When the index of the Logarithm to be divided, is negative, and does not exactly contain the divisor without some remainder, increase the index by such a number, as will make it exactly divisible by the index, carrying the units borrowed as so many tens to the left hand place of the decimal, and then divide as in whole numbers.

EXAMPLES.

1. Required the square root of 847. Index 2)2.927883=Log. of 847.

1.463941 = Quot. = Log. of 29.103 + = ans.

2. Required the cube root of 847. Index 3)2.927883=Log. of the given number.

0.975961 = Quot = Log. of 9.462 = ans. [nearly.

3. Required the square root of .093. Index 2)—2.968483=Log. of .093.

-1.484241 = Quot. = Log. of. 304959 = ans.

4. Required the cube root of 12345. Index 3)4.091491=Log. of 12345.

1.363830=Quot.=Log. of 23.116.=Ans

SECTION IV.

ELEMENTS OF

PLANE GEOMETRY.

DEFINITIONS.

See PLATE I.

- 1. Geometry is that science wherein we consider the properties of magnitude.
- 2. A point is that which has no parts, being of itself indivisible; as A.
- 3. A line has length but no breadth; as AB. figures 1 and 2.
- 4. The extremities of a line are points, as the extremities of the line AB are the points A and B. figures 1 and 2.
- 5. A right line is the shortest that can be drawn between any two points, as the line AB. fig. 1. but if it be not the shortest, it is then called a curve line, as AB. fig. 2.
- 6. A superficies or surface is considered only as having length and breadth, without thickness, as ABCD. fig. 3.
 - 7. The extremities of a superficies are lines.
 - 8. The inclination of two lines meeting one another (provided they do not make one continued

)

line) or the opening between them, is called an angle. Thus in fig. 4. the inclination of the line AB to the line BC meeting each other in the point B, or the opening of the two lines BA and BC, is called an angle, as ABC.

- Note, When an angle is expressed by three letters, the middle one is that at the angular point.
- 9. When the lines that form the angle are right ones, it is then called a right-lined angle, as ABC, fig. 4. If one of them be right and the other curved, it is called a mixed angle, as B. fig. 5. If both of them be curved, it is called a curved-lined or spherical angle, as C. fig. 6.
- 10. If a right line, CD (fig. 7.) fall upon another right line, AB, so as to incline to neither side, but make the angles ADC, CDB on each side equal to each other, then those angles are called right angles, and the line CD a perpendicular.
- 11. An obtuse angle is that which is wider or greater than a right one, as the angle ADE. fig. 7. and an acute angle is less than a right one, as EDB. fig. 7.
- 12. Acute and obtuse angles in general are called oblique angles.
- 13. If a right line CB. (fig. 8.) be fastened at the end C, and the other end B, be carried quite round, then the space comprehended is called a circle; and the curve line described by the point B, is called the circumference or the periphery of the circle; the fixed point C, is called its centre.

- 14. The describing line CB. (fig. 8.) is called the semidiameter or radius, so is any line from the centre to the circumference: whence all radii of the same or of equal circles are equal.
- 15. The diameter of a circle is a right line drawn thro' the centre, and terminating in opposite points of the circumference; and it divides the circle and circumference into two equal parts, called semicircles; and is double the radius, as AB or DE. fig. 8.
- 16. The circumference of every circle is supposed to be divided into 360 equal parts called degrees, and each degree into 60 equal parts called minutes, and each minute into 60 equal parts called ed seconds, and these into thirds, fourths, &c. these parts being greater or less as the radius is.
- 17. A chord is a right line drawn from one end of an arc or arch (that is, any part of the circumference of a circle) to the other; and is the measure of the arc. Thus the right line HG, is the measure of the arc HBG. fig. 8.
- 18. The segment of a circle is any part thereof, which is cut off by a chord: thus the space which is comprehended between the chord HG and the arc HBG, or that which is comprehended between the said chord HG and the arc HDAEG are called segments. Whence it is plain, fig. 8.
- 1. That any chord will divide the circle into two segments.
- 2. The less the chord is, the more unequal are the segments.

- 3. When the chord is greatest it becomes a diameter, and then the segments are equal; and each segment is a semicircle.
- 19. A sector of a circle is a part thereof less than a semicircle, which is contained between two radii and an arc: thus the space contained between the two radii *CH*, *CB*, and the arc *HB* is a sector. fig. 8.
- 20. The right sine of an arc, is a perpendicular line let fall from one end thereof, to a diameter drawn to the other end: thus HL is the right sine of the arc HB.

The sines on the same diameter increase till they come to the centre, and so become the radius; hence it is plain that the radius CD is the greatest possible sine, and thence is called the whole sine.

Since the whole sine CD (fig. 8.) must be perpendicular to the diameter (by def. 20.) therefore producing DC to E, the two diameters AB and DE cross one another at right angles, and thus the periphery is divided into four equal parts, as BD, DA, AE, and EB; (by def. 10.) and so BD becomes a quadrant or the fourth part of the periphery: therefore the radius DC is always the sine of a quadrant, or of the fourth part of the circle BD.

Sines are said to be of as many degrees as the arc contains parts of 360: so the radius being the sine of a quadrant becomes the sine of 90 degrees, or the fourth part of the circle, which is 360 degrees.

- 21. The versed sine of an arc is that part of the diameter that lies between the right sine and the circumference: thus LB is the versed sine of the arc HB: fig. 8.
- 22. The tangent of an arc is a right line touching the periphery, being perpendicular to the end of the diameter, and is terminated by a line drawn from the centre through the other end: thus BK is the tangent of the arc HB. fig. 8.
- 23. And the line which terminates the tangent, that is, CK, is called the secant of the arc HB. fig. 8.
- 24. What an arc wants of a quadrant is called the complement thereof: Thus DH is the complement of the arc HB. fig. 8.
- 25. And what an arc wants of a semicircle is called the supplement thereof: thus AH is the supplement of the are HB. fig. 8.
- 26. The sine, tangent, or secant of the complement of any arc, is called the co-sine, co-tangent, or co-secant of the arc itself: thus FH is the sine, DI the tangent, and CI the secant of the arc DH: or they are the co-sine, co-tangent, or co-secant of the arc HB. fig. 8.
- 27. The sine of the supplement of an arc, is the same with the sine of the arc itself; for drawing them according to def. 20, there results the self-same line; thus HL is the sine of the arc HB, or of its supplement ADII. fig. 8.
- 28. The measure of a right-lined angle, is the arc of a circle swept from the angular point, and

contained between the two lines that form the angle: thus the angle HCB (fig. 8.) is measured by the arc HB; and is said to contain so many degrees as the arc HB does; so if the arc HB is 60 degrees, the angle HCB is an angle of 60 degrees.

Hence angles are greater or less according as the arc described about the angular point, and terminated by the two sides, contains a greater or less number of degrees of the whole circle.

- 29. The sine, tangent, and secant of an arc, is also the sine, tangent, and secant of an angle whose measure the arc is: thus because the arc HB is the measure of the angle HCB, and since HL is the sine, BK the tangent, and CK the secant, BL the versed sine, HF the co-sine, DI the co-tangent, and CI the co-secant, &c. of the arc BH; then HL is called the sine, BK the tangent, CK the secant, &c. of the angle HCB, whose measure is the arc HB. fig. 8.
- 30. Parallel lines are such as are equi-distant from each other, as AB, CD. fig. 9.
- 31. A figure if a space bounded by a line or lines. If the lines be right it is called a rectilineal figure, if curved it is called a curvilineal figure; but if they be partly right and partly curved lines, it is called a mixed figure.
- 32. The most simple rectilineal figure is a triangle, being composed of three right lines, and is considered in a double capacity; 1st, with respect to its sides; and 2d, to its angles.
- 33. In respect to its sides it is either equilateral, having the three sides equal, as A. fig. 10.

- 34. Or isosceles, having two equal sides, as B. fig. 11.
- 35. Or scalene, having the three sides unequal, as C. fig. 12.
- 36. In respect to its angles, it is either right-angled, having one right angle, as D. fig. 13.
- 37. Or obtuse angled, having one obtuse angle, as E. fig. 14.
- 38. Or acute angled, having all the angles acute, as F. fig. 15.
- 39. Acute and obtuse angled triangles are in general called oblique angled triangles, in all which any side may be called the base, and the other two the sides.
- 40. The perpendicular height of a triangle is a line drawn from the vertex to the base perpendicularly: thus if the triangle ABC, be proposed, and BC be made its base, then if from the vertex A the perpendicular AD be drawn to BC, the line AD will be the height of the triangle ABC, standing on BC as its base. Fig. 16.

Hence all triangles between the same parallels have the same height, since all the perpendiculars are equal from the nature of parallels.

- 41. Any figure of four sides is called a quadrilateral figure.
- 42. Quadrilateral figures, whose opposite sides are parallel, are called parallelograms: thus

ABCD is a parallelogram. Fig. 3. 17, and AB. fig. 18 and 19.

- 43. A parallelogram whose sides are all equal and angles right, is called a square, as ABCD. fig. 17.
- 44. A parallelogram whose opposite sides are equal and angles right, is called a rectangle, or an oblong, as ABCD. fig. 3.
- 45. A rhombus is a parallelogram of equal sides, and has its angles oblique, as A. fig. 18. and is an inclined square.
- 46. A rhomboides is a parallelogram whose opposite sides are equal and angles oblique; as B. fig. 19. and may be conceived as an inclined rectangle.
- 47. Any quadrilateral figure that is not a parallelogram, is called a trapezium. Plate 7. fig. 3.
- 48. Figures which consist of more than four sides are called polygons; if the sides are allequal to each other, they are called regular polygons. They sometimes are named from the number of their sides, as a five-sided figure is called a pentagon, one of six sides a hexagon, &c. but if their sides are not equal to each other, then they are called irregular polygons, as an irregular pentagon, hexagon, &c.
- 49. Four quantities are said to be in proportion when the product of the extremes is equal to that of the means: thus if A multiplied by D, be equal to B multiplied by C, then A is said to A as C is to D.

POSTULATES OR PETITIONS.

- 1. That a right line may be drawn from any one given point to another.
- 2. That a right line may be produced or continued at pleasure.
- 3. That from any centre and with any radius, the circumference of a circle may be described.
- 4. It is also required that the equality of lines and angles to others given, be granted as possible: that it is possible for one right line to be perpendicular to another, at a given point or distance; and that every magnitude has its half, third, fourth, &c. part.

Note, Though these postulates are not always quoted, the reader will easily perceive where, and in what sense they are to be understood.

AXIOMS or self-evident TRUTHS.

- 1. Things that are equal to one and the same thing, are equal to each other.
 - 2. Every whole is greater than its part.
- 3. Every whole is equal to all its parts taken together.
- 4. If to equal things, equal things be added, the whole will be equal.
- 5. If from equal things, equal things be deducted, the remainders will be equal.

- 6. If to or from unequal things, equal things be added or taken, the sums or remainders will be unequal.
 - 7. All right angles are equal to one another.
- 8. If two right lines not parallel, be produced towards their nearest distance, they will intersect each other.
- 9. Things which mutually agree with each other, are equal.

NOTES.

A theorem is a proposition, wherein something is proposed to be demonstrated.

A problem is a proposition, wherein something is to be done or effected.

A lemma is some demonstration, previous and necessary, to render what follows the more easy.

A corollary is a consequent truth, deduced from a foregoing demonstration.

A scholium, is a remark or observation made upon something going before.

GEOMETRICAL THEOREMS.

THEOREM I.

Pz. 1, fig. 20.

IF a right line falls on another, as AB, or EB, does on CD, it either makes with it two right angles, or two angles equal to two right angles.

- 1. If AB be perpendicular to CD, then (by def. 10.) the angles CBA, and ABD, will be each a right angle.
- 2. But if EB fall slantwise on CD, then are the angles DBE+EBC=DBE+EBA (=DBA)+ ABC, or two right angles. $Q.\ E.\ D.$
- Corollary 1. Whence if any numbers of right lines were drawn from one point, on the same side of a right line; all the angles made by these lines will be equal to two right lines.
 - 2. And all the angles which can be made about a point, will be equal to four right angles.

THEO. II.

PL. 1. fig. 21.

If one right line cross another, (as AC does BD) the opposite angles made by those lines, will be equal to each other: that is, AEB to CED, and BEC to AED.

By theorem 1. BEC + CED = 2 right angles. and CED + DEA = 2 right angles.

Therefore (by axiom 1.) BEC+CED=CED+

DEA: take CED from both, and there remains BEC=DEA. (by axiom 5.) Q. E. D.

After the same manner CED + AED = 2 right angles; and AED + AEB = two right angles; wherefore taking AED from both, there remains CED = AEB. Q. E. D.

THEO. III.

PL. 1. fig. 22.

If a right line cross two parallels, as GH dees AB and CD, then,

- 1. Their external angles are equal to each other, that is, GEB = CFH.
- 2. The alternate angles will be equal, that is, AEF = EFD and BEF = CFE.
- 3. The external angle will be equal to the internal and opposite one on the same side, that is, GEB = EFD and AEG = CFE.
- 4. And the sum of the internal angles on the same side, are equal to two right angles; that is, BEF+DFE are equal to two right angles, and AEF+CFE are equal to two right angles.
- 1. Since AB is parallel to CD, they may be considered as one broad line, crossed by another line, as GH; (then by the last theo.) GEB = CFH, and AEG = HFD.
- 2. Also GEB = AEF, and CFH = EFD; but GEB = CFH (by part 1. of this theo.) therefore AEF = EFD. The same way we prove FEB = EFC.
- 3. AEF=EFD; (by the last part of this theo.) but AEF=GEB (by theo. 2.) Therefore GEB=EFD. The same way we prove AEG=CFE.

4. For since GEB = EFD, to both add FEB, then (by axiom 4.) GEB + FEB = EFD + FEB, but GEB + FEB, are equal to two right angles (by theo. 1.) Therefore EFD + FEB are equal to two right angles: after the same manner we prove that AEF + CFE are equal to two right angles. Q.E.D.

THEO. IV.

PL. 1. fig. 23.

In any triangle ABC, one of its legs, as BC, being produced towards D, it will make the external angle ACD equal to the two internal opposite angles taken together. Viz. to B and A.

Through C, let CE be drawn parallel to AB; then since BD cuts the two parallel lines BA, CE; the angle ECD = B, (by part 3. of the last theo.) and again, since AC cuts the same parallels, the angle ACE = A (by part. 2. of the last.) Therefore ECD + ACE = ACD = B + A. Q. E. D.

THEO. V.

PL. 1. fig. 23.

In any triangle ABC, all the three angles, taken together, are equal to two right angles, viz. A + B + ACB = 2 right angles.

Produce CB to any distance, as D, then (by the last) ACD = B + A; to both add ACB; then ACD + ACB = A + B + ACB; but ACD + ACB = 2 right angles (by theo. 1.); therefore the three angles A + B + ACB = 2 right angles. Q. E. D.

Cor. 1. Hence if one angle of a triangle be known, the sum of the other two is also known: for since the three angles of every triangle contain two right ones, or 180 degrees, therefore 180

—the given angle will be equal to the sum of the other two; or 180—the sum of two given angles, gives the other one.

Cor. 2. In every right-angled triangle, the two acute angles are = 90 degrees, or to one right angle: therefore 90 — one acute angle, gives the other.

THEO. VI.

PL. 1. fig. 24.

If in any two triangles, ABC, DEF, there be two sides, AB. AC in the one, severally equal to DE, DF in the other, and the angle A contained between the two sides in the one, equal to D in the other; then the remaining angles of the one, will be severally equal to those of the other, viz. B = E and C = F; and the base of the one BC, will be equal to EF, that of the other.

If the triangle ABC be supposed to be laid on the triangle DEF, so as to make the points A and B coincide with D and E, which they will do, because AB = DE (by the hypothesis); and since the angle A = D, the line AC will fall along DF, and inasmuch as they are supposed equal, C will fall in F; seeing therefore the three points of one coincide with those of the other triangle, they are manifestly equal to each other; therefore the angle B = E and C = F, and BC = EF. Q. E. D.

LEMMA.

Pr. 1. fig. 11.

If two eider of a triangle a b c be equal to each other, that is, ac = cb, the angles which are opposite to those equal sides, will also be equal to each other; viz. a = b.

For let the triangle a b c be divided into two

triangles a c d, d c b, by making the angle a c d = d c b (by postulate 4.) then because a c = b c, and cd common, (by the last) the triangle a d c = d c b; and therefore the angle a = b. Q. E. D.

Cor. Hence if from any point in a perpendicular which bisects a given line, there be drawn right lines to the extremeties of the given one, they with it will form an isosceles triangle.

THEO. VII.

PL. 1. fig. 25.

The angle BCD at the centre of a circle ABED, is double the angle BAD at the circumference, etanding upon the same are BED.

Through the point A, and the centre C, draw the line ACE: then the angle ECD = CAD, + CDA; (by theo. 4.) but since AC = CD being radii of the same circle, it is plain (by the preceding lemma) that the angles subtended by them will be also equal, and that their sum is double to either of them, that is, DAC + ADC is double to CAD, and therefore ECD is double to CAD; after the same manner BCE is double to CAB, wherefore, BCE + ECD, or BCD is double to BAC + CAD or to BAD. Q. E. D.

Cor. 1. Hence an angle at the circumference is measured by half the arc it subtends or stands on.

Fig. 26.

Cor. 2. Hence all angles at the circumference of a circle which stands on the same chord as AB, are equal to each other, for they are all measured by half the arc they stand on, vis. by half the arc AB.

Fig. 26.

Cor. 3. Hence an angle in a segment greater than a semicircle is less than a right angle; thus ADB is measured by half the arc AB, but as the arc AB is less than a semicircle, therefore half the arc AB, or the angle ADB is less than half a semicircle, and consequently less than a right angle.

Fig. 27.

Cor. 4. An angle in a segment less than a semicircle, is greater than a right angle, for since the arc AEC is greater than a semicircle, its half, which is the measure of the angle ABC, must be greater than half a semicircle, that is, greater than a right angle.

Fig. 28.

Cor. 5. An angle in a semicircle is a right angle, for the measure of the angle ABD, is half of a semicircle AED, and therefore a right angle.

THEO. VIII.

PL. 1. fig. 29.

If from the centre C of a circle ABE, there be let fall the perpendicular CD on the chord AB, it will bisect it in the point D.

Let the lines AC and CB be drawn from the centre to the extremities of the chord, then since CA=CB, the angles CAB=CBA (by the lemma.) But the triangles ADC, BDC are right angled ones, since the line CD is a perpendicular; and so the angle ACD=DCB; (by cor. 2. theo. 5.) then have we AC, CD, and the angle ACD in one triangle; severally equal to CB, CD, and the angle

BCD in the other: therefore (by theo. 6.) A = DB. Q. E. D.

Cor. Hence it follows, that any line bisecting a chord at right angles, is a diameter; for a line drawn from the centre perpendicular to a chord, bisects that chord at right angles; therefore, conversely, a line bisecting a chord at right angles must pass through the centre, and consequently be a diameter.

THEO, IX.

PL. 1. fig. 29.

If from the centre of a circle ABE there be drawn a perpendicular CD on the chord AB, and produced till it meets the circle in F, that line CF, will bisect the arc AB in the point F.

Let the lines AF and BF be drawn, then in the triangles ADF, BDF; AD=BD (by the last;) DF is common, and the angle ADF=BDF being both right, for CD or DF is a perpendicular. Therefore (by theo. 6.) AF=FB; but in the same circle, equal lines are chords of equal arcs, since they measure them (by def. 19.): whence the arc AF=FB, and so AFB is bisected in F, by the line CF.

Cor. Hence the sine of an arc is half the chord of twice that arc. For AD is the sine of the arc AF, (by def. 22.) AF is half the arc, and AD half the chord AB (by theo. 8.) therefore the corollary is plain.

THEO. X.

PL. 1. fig. 30.

In any triangle ABD, the half of each side is the sine of the opposite angle.

Let the circle ADB be drawn through the points A, B, D; then the angle DAB is measured by half the arc BKD, (by cor 1 theo. 7.) viz. the chord of BK is the measure of the angle BAD; therefore (by cor. to the last) BE the half of BD is the sine of BAD: the same way may be proved that half of AD is the sine of ABD, and the half of AB the sine of ADB. Q. E. D.

THEO. XL

PL. 1. fig. 22.

If a right line GH cut two other right lines AB, CD, so at to make the alternate angles AEF, EFD equal to each other, then the lines AB and CD will be parallel.

If it be denied that AB is parallel to CD, let IK be parallel to it; then IEF=(EFD)=AEF (by part 2. theo. 3.) a greater to a less, which is absurd, whence IK is not parallel; and the like we can prove of all other lines but AB; therefore AB is parallel to CD. Q.E.D.

THEO. XII.

PL. 1. fig. 3.

If two equal and parallel lines AB, CD, be joined by two other lines AD, BC, those shall be also equal and parallel.

Let the diameter or diagonal BD be drawn, and we will have the triangles ABD, CBD: whereof AB in one is=to CD in the other, BD common to both, and the angle ABD=CDB (by part 2. theo. 3.;) therefore (by theo. 6.) AD=CB, and the angle CBD=ADB, and thence the lines AD and BC are parallel, by the preceding theorem.

Cor. 1. Hence the quadrilateral figure ABCD is a parallelogram, and the diagonal BD bisects the

same, inasmuch as the triangle ABD = BCD, as now proved.

- Cor. 2. Hence also the triangle ABD on the same base AB, and between the same parallels with the parallelogram ABCD, is half the parallelogram.
- Cor. 3. It is hence also plain, that the opposite sides of a parallelogram are equal; for it has been proved that ABCD being a parallelogram, AB will be = CD and AD = BC.

THEO. XIII.

PL. 1. fig. 31.

All parallelograms on the same or equal bases and between the same parallels, are equal to one another, that is, if BD = GH, and the lines BH and AF parallel, then the parallelogram ABDC = BDFE = EFHG.

For AC=BD=EF (by cor. the last;) to both add CE then AE=CF. In the triangles ABE, CDF; AB=CD and AE=CF and the angle BAE=DCF (by part 3. theo. 3.;) therefore the triangle ABE=CDF, (by theo. 6.) let the triangle CKE be taken from both, and we will have the trapezium ABKC=KDFE; to each of these add the triangle BKD, then the parallelogram ABCD=BDEF; in like manner we may prove the parallelogram EFGH=BDEF. Wherefore ABDC=BDEF=EFHG. Q. E. D.

Cor. Hence it is plain that triangles on the same or equal bases, and between the same parallels, are equal, seeing (by cor. 2. theo. 12.) they are the halves of their respective parallelogram.

THEO. XIV.

PL. 1. fig. 32.

In every right-angled triangle, ABC, the square of the hypothenuse or longest side, BC, or BCMH, is equal to the sum of the squares made on the other two sides AB and AC, that is, ABDE and ACGF.

Through A draw AKL perpendicular to the hypothenuse BC, join AH, AM, DC and BG; in the triangles, BDC, ABH, BD = BA, being sides of the same square, and also BC = BH, and the included angles DBC = ABH, (for DBA =CBH being both right, to both add ABC, then DBC = ABH) therefore the triangle DBC =ABH (by theo. 6.) but the triangle DBC is half of the square ABDE (by cor. 2 theo. 12.) and the triangle ABH is half the parallelogram BKLH. The same way it may be proved, that the square ACGF, is equal to the parallelogram KCLM. So ABDE+ACGF the sum of the squares=BKLH+ KCML, the sum of the two parallelograms or square BCMH; therefore the sum of the squares on AB and AC is equal to the square on BC. Q. E. D.

- Cor. 1. Hence the hypothenuse of a right-angled triangle may be found by having the sides; thus, the square root of the sum of the squares of the base and perpendicular, will be the hypothenuse.
- Cor. 2. Having the hypothenuse and one side given to find the other; the square root of the difference of the squares of the hypothenuse and given side, will be the required side.

THEO. XV.

Ps. 1. fig. 33.

In all circles the chord of 60 degrees is always equal in length to the radius.

Thus in the circle AEBD, if the arc AEB be an arc of 60 degrees, and the chord AB be drawn: then AB = CB = AC.

In the triangle ABC, the angle ACB is 60 degrees, being measured by the arc AEB; therefore the sum of the other two angles is 120 degrees (by Cor. 1. theo. 5.) but since AC=CB, the angle CAB=CBA (by lemma preceding theo. 7.) consequently each of them will be 60, the half of 120 degrees, and the three angles will be equal to one another, as well as the three sides: wherefore AB=BC=AC. Q. E. D.

Cor. Hence the radius, from whence the lines on any scale are formed, is the chord of 60 degrees on the line of chords.

THEO. XVI.

PL. 1. fig. 34.

If in two triangles ABC, abc, all the angles of one be each respectively equal to all the angles of the other, that is, A=a, B=b, C=c: then the sides opposite to the equal angles will be proportional, viz.

AB: ab:: AC: ac
AB: ab:: BC: bc
and AC: ac:: BC: bc

For the triangles being inscribed in two circles, it is plain since the angle A=a, the arc $BDC=b\ d\ c$, and consequently the chord BC is to $b\ c$, as the radius of the circle ABC is to the radius of the circle $a\ b\ c$; (for the greater the radius is, the greater is the circle described by that radius; and consequently the greater any particular arc of that circle is, so the chord, sine, tangent, &c. of that arc will be also greater. Therefore, in general, the chord, sine, tangent, &c. of any arc is proportional to the radius of the circle;) the same way the chord

AB is to the chord ab, in the same proportion. So AB:ab::BC:bc; the same way the rest may be proved to be proportional.

THEO. XVIL

PL. 1. fig. 35.

If from a point A without a circle DBCE there be drawn two lines ADE, ABC, each of them cutting the circle in two points; the product of one whole line into its external part, viz. AC into AB, will be equal to that of the other line into its external part, viz. AE into AD.

Let the lines DC, BE, be drawn in the two triangles ABE, ADC; the angle AEB = ACD (by cor. 2. theo. 7.) the angle A is common, and (by cor. 1. theo. 5.) the angle ADC = ABE; therefore the triangles ABE, ADC, are mutually equiangular, and consequently (by the last) AC : AE :: AD : AB; wherefore AC multiplied by AB, will be equal to AE multiplied by AD. Q.E.D.

THEO. XVIII.

PL. 2. fig. 1.

Triangles ABC, BCD, and parallelograms ABCF and BDEC, having the same altitude, have the same proportion between themselves as their bases BA and BD.

Let any aliquot part of AB be taken, which will also measure BD: suppose that to be Ag, which will be contained twice in AB, and three times in BD, the parts Ag, gB, Bh, hi, and iD being all equal, and let the lines gC, hC, and iC, be drawn: then (by cor. to theo. 13.) all the small triangles AgC, gCB, BCh, &c. will be equal to each other; and will be as many as the parts into which their bases were divided; therefore it will be as the sum of the parts in one base, is to the

sum of those in the other, so will be the sum of the small triangles in the first, to the sum of the small triangles in the second triangle; that is, AB:BD:ABC:BDC.

Whence also the parallelograms ABCF and BDEC, being (by cor. 2. theo. 12.) the doubles of the triangles, are likewise as their bases. Q. E. D.

Note. Wherever there are several quantities connected with the sign (::) the conclusion is always drawn from the first two and last two proportionals,

THEO. XIX.

PL. 2. fg. 2,

Triangles ABC, DEF, standing upon equal bases AB and DE, are to each other as their altitudes CG and FH.

Let BI be perpendicular to AB and equal to CG, in which let KB = FH, and let AI and AK be drawn.

The triangle AIB = ACB (by cor. to theo. 13.) and AKB = DEF; but (by theo. 18.) BI: BK:: ABI: ABK. That is, CG: FH:: ABC: DEF. Q. E. D,

THEO. XX.

PL. 2. fig. 3.

If a right line BE be drawn parallel to one side of a triangle ACD, it will cut the two other sides proportionally, viz. AB: BC: AE: ED.

Draw CE and BD; the triangles BEC and EBD being on the same base BE and under the same parallel CD, will be equal (by cor. to theo. 13.)

therefore (by theo. 18) AB:BC::(BEA:BEC) or BEA:BED)::AE:ED. Q. E. D.

- Cor. 1. Hence also AC:AB::AD:AE: For AC:AB::(AEC:AEB::ABD:AEB): :AD:AE.
- Cor. 2. It also appears that a right line, which divides two sides of a triangle proportionally, must be parallel to the remaining side.
- Cor. 3. Hence also, theo. 16. is manifest; since the sides of the triangles ABE, ACD, being equiangular, are proportional.

THEO. XXI.

PL. 2. fig. 4.

If two triangles ABC, ADE, have an angle BAC, in the one, equal to an angle DAE, in the other, and the sides about the equal angles, proportional; that is, AB: AD:: AC: AE; then the triangles will be mutually equiangular.

In AB take Ad = AD, and let de be parallel to BC, meeting AC in e.

Because (by the first cor. to the foregoing theo.) AB:Ad (or AD): AC:Ae, and (by the hypothesis, or what is given in the theorem) AB:AD:AC:AE; therefore Ae=AE seeing AC bears the same proportion to each; and (by theo. 6.) the triangle Adc=ADE, therefore the angle Ade=D and Aed=E, but since ed and ed=D and ed=D.

THEO. XXIL

PL. 2. fig. 5.

Equiangular triangles ABC, DEF, are to one another in

a duplicate proportion of their homologous or like sides; or as the squares AK, and DM of their homologous sides.

Let the perpendiculars CG and FH be drawn as well as the diagonals BI and EL.

The perpendiculars make the triangles ACG and DFH equiangular, and therefore similar (by theo. 16.) for because the angle CAG=FDH, and the right angle AGC=DHF, the remaining angle ACG=DFH, (by cor. 2. theo. 5.)

Therefore GC: FH: (AC:DF::)AB:DE, or which is the same thing, GC:AB::FH:DE for FH multiplied by AB = AB multiplied by FH.

By theo. 19. ABC: ABI:: (CG: AI or AB as before :: FH DE or DL::) DFE: DLE, therefore ABC: ABI:: DFE: DLE, or ABC: AK:: DFE: DM, for AK is double the triangle ABI, and DM double the triangle DEL, by cor. 2. theo. 12. Q.E.D.

THEO. XXIII.

PL. 2. fig. 6.

Like polygons ABCDE, a b c d e, are in a duplicate proportion to that of the sides AB, a b, which are between the equal angles A and B and a and b, or as the squares of the sides AB, ab.

Draw AD, AC, ad, ac.

By the hypothesis AB : ab :: BC : bc; and thereby also the angle B = b; therefore (by theo. 21.) BAC = b a c; and ACB = a c b: in like manner EAD = e a d, and EDA = e da. If therefore from the equal angles A, and a, we take the equal ones

EAD + BAC = c a d, + b a c the remaining angle DAC = d a c, and if from the equal angles D and d, EDA = c d a, be taken, we shall have ADC = a d c: and in like manner if from C and c be taken BCA, = b c a, we shall have ACD = a c d; and so the respective angles in every triangle, will be equal to those in the other.

By theo. 22. ABC: abc:: the square of AC to the square of ac, and also ADC: adc:: the square of AC, to the square of ac; therefore from equality of proportions ABC: abc:: ADC: adc: in like manner we may shew that ADC: adc: in like manner we may shew that ADC: adc: EAD: cad: Therefore it will be as one antecedent is to one consequent, so are all the antecedents to all the consequents. That is, ABC is to abc as the sum of the three triangles in the first polygon, is to the sum of those in the last. Or ABC will be to abc, as polygon to polygon.

The proportion of ABC to abc (by the foregoing theo.) is as the square of AB is to the square of ab, but the proportion of polygon to polygon, is as ABC to abc, as now shown: therefore the proportion of polygon to polygon is as the square of AB to the square of ab.

THEO. XXIV.

PL. 1. fig. 8.

Let DHB be a quadrant of a circle described by the radius CB; HB an arc of it, and DH its complement; HL or FC the sine, FH or CL its co-sine, BK its tangent, DI its co-tangent; CK its secant, and CI its co-secant. Fig. 8.

1. The co-sine of an arc is to the sine, as the radius is to the tangent.

- 2. The radius is to the tangent of an arc, as the co-sine of it is to the sine.
- 3. The sine of an arc is to its co-sine, as the radius to its co-tangent;
- 4. Or the radius is to the co-tangent of an arc, as its sine to its co-sine.
- 5. The co-tangent of an arc is to the radius, as the radius to the tangent.
- 6. The co-sine of an arc is to the radius, as the radius is to the secant.
- 7. The sine of an arc is to the radius, as the tangent is to the secant.

The triangles CLH and CBK, being similar, (by theo. 16.)

- 1. CL: LH:: CB: BK.
- 2. Or, CB : BK:: CL: LH.

The triangles CFH and CDI, being similar.

- 3. CF (or LH): FH:: CD: DI.
- 4. CD : DI :: CF (or LH) : FH.

The triangles CDI and CBK are similar: for the angle CID = KCB, being alternate ones (by part 2. theo. 3.) the lines CB and DI being parallel: the angle CDI = CBK being both right, and consequently the angle DCI = CKB, wherefore,

5. DI: CD:: CB: BK.

And again, making use of the similar triangle CLH and CBK.

6. CL : CB : : CH : CK.

7. HL:CH:BK:CK.

GEOMETRICAL PROBLEMS.

PROB. I.

PL. 2. fig. 7.

To make a triangle of three given right lines BO, LB, LO, of which any two must be greater than the third.

Lay BL from B to L; from B with the line BO, describe an arc, and from L with LO describe another arc; from O, the intersecting point of those arcs, draw BO and OL, and BOL is the triangle required.

This is manifest from the construction.

PROB. II.

PL. 2. fig. 8.

At a point B in a given right line BC, to make an angle equal to a given angle A.

Draw any right line ED to form a triangle, as EAD, take BF=AD, and upon BF make the triangle BFG, whose side BG=AE, and GF=ED (by the last) then also the angle B=A; if we suppose one triangle be laid on the other, the sides

will mutually agree with each other, and therefore be equal; for if we consider these two triangles to be made of the same three given lines, they are manifestly one and the same triangle.

Otherwise,

Upon the centres A and B, at any distance, let two arcs, DE, FG, be described; make the arc FG=DE, and through B and G draw the line BG, and it is done.

For since the chords ED, GF, are equal, the angles A and B are also equal, as before (by def.17.)

PROB. III.

PL. 2. fig. 9.

To bisect or divide into two equal parts, any given rightlined angle, BAC.

In the lines AB and AC, from the point A set off equal distances AE, =AD, then, with any distance more than the half of DE, describe two arcs to cut each other in some point F; and the right-line AF, joining the points A and F, will bisect the given angle BAC.

For if DF and FE be drawn, the triangles ADF, AEF, are equilateral to each other, viz. AD=AE, DF=FE, and AF common, wherefore DAF=EAF, as before.

PROB. IV.

PL. 2. fig. 10.

To bisect a right-line. AB.

With any distance, more than half the line, from K

A and B, describe two circles CFD, CGD, cutting each other in the points C and D; draw CD intersecting AB in E, then AE = EB.

For, if AC, AD, BC, BD, be drawn, the triangles ACD, BCD, will be mutually equilateral, and consequently the angle ACE=BCE: therefore the triangle ACE, BCE, having AC=BC, CE common, and the angle ACE=BCE; (by theo. 6.) the base AE the base BE.

Cor. Hence it is manifest, that CD not only bisects AB, but is perpendicular to it, (by def. 11.)

PROB. V.

PL. 2. fig. 11.

On a given point A, in a right line EF, to erect a perpendicular.

From the point A lay off on each side, the equal distances, AC, AD; and from C and D, as centres, with any interval greater than AC or AD, describe two arcs intersecting each other in B; from A to B draw the line AB, and it will be the perpendicular required.

For, let CB, and BD be drawn; then the triangles CAB, DAB, will be mutually equilateral and equiangular, so CAB = DAB, a right angle, (by def. 10.)

PROB. VI.

PL. 2. fig. 12.

To raise a perpendicular on the end B of a right line AB.

From any point D not in the line AB, with the distance from D to B, let a circle be described cut-

ting AB in E; draw from E through D the right line EDC, cutting the periphery in C, and join CB; and that is the perpendicular required.

EBC being a semicircle, the angle EBC will be a right angle (by cor. 5. theo. 7.)

PROB. VII.

PL. 2. fig. 13.

From a given point A, to let fall a perpendicular upon a given right line BC.

From any point D, in the given line, take the distance to the given point A, and with it describe a circle AGE, make GE = AG, join the points A and E, by the line AFE, and AF will be the perpendicular required.

Let DA, DE, be drawn; the angle ADF = FDE, DA = DE, being radii of the same circle, and DF common; therefore (by theo. 6.) the angle DFA = DFE, and FA a perpendicular. (By def. 10.)

PROB. VIII.

PL. 2. fig. 14.

Through a given point A, to draw a right line AB, parallel to a given right line CD.

From the point A, to any point F, in the line CD, draw the line AF; with the interval FA, and one foot of the compasses in F, describe the arc AE, and with the like interval and one foot in A, describe the arc BF, making BF = AE; through A and B draw the line AB, and it will be parallel to CD.

By prob. 2. The angle BAF=AFE, and by theo. 11. BA and CD are parallel.

PROB. IX.

PL. 1. fig. 17.

Upon a given line AB to describe a square ABCB.

Make BC perpendicular and equal to AB; and from A and C, with the line AB, or BC, let two arcs be described, cutting each other in D; from whence to A and C, let the lines AD, DC be drawn; so is ABCD the square required.

For all the sides are equal by construction; therefore the triangles ADC and BAC, are mutually equilateral and equiangular, and ABCD is an equilateral parallelogram, whose angles are right. For B being right, D is also right, and DAC, DCA, BAC, ACB, each half a right angle, (by lemma preceding theo. 7. and cor. 2. theo. 5.) whence DAB and BCD will each be a right angle, and (by def. 44.) ABCD is a square.

scholium.

By the same method a rectangle or oblong, may be described, the sides thereof being given.

PROB. X.

PL. 2. fig. 15.

To divide a given right line AB, into any proposed number of equal parts.

Draw the indefinite right line AP, making any angle with AB, also draw BQ parallel to AP, in

each of which, let there be taken as many equal parts AM, MN, &c. Bo, on, &c. as you would have AB divided into; then draw Mm, Nn, &c. intersecting AB in E, F, &c. and it is done.

For MN and mn being equal and parallel, FN will be parallel to EM; and in the same manner, GO to FN (by theo. 12.) therefore AM, MN, NO, being all equal by construction, it is plain (from theo. 10.) that AE, EF, FG, &c. will likewise be equal.

PROB. XI.

PL. 2. fig. 16.

To find a third proportional to two given right lines, A and B.

Draw two indefinite blank lines CE, CD, anywise to make any angle. Lay the line A, from C to F; and the line B, from C, to G; and draw the line FG; lay again the line A, from C to H; and through H, draw HI parallel to FG (by prob. 8.) so is CI the third proportional required.

For by cor. 1. theo. 20, CG: CH:: CF: CI.

Or, B:A::A:CI.

PROB. XII.

PL. 2. fig. 17.

Three right lines A, B, C, given to find a fourth proportional.

Having made an angle DEF anywise, by two indefinite blank right lines, ED, EF, as before; lay the line A; from E to G; the line B, from E to I; and draw the line IG; lay the line C, from E to

H, and (by prob. 8.) draw HK parallel thereto, so will EK be the fourth proportional required.

For, by cor. 1. theo. 20. EG:EI::EH:EK.

Or, A:B::C:EK.

PROB. XIII.

PL. 3. fig. 1.

Two right lines, A and B, given to find a mean proportional.

Draw an indefinite blank line, as AF, on which lay the line A, from B to B, and the line B, from B to C, on the point B, which is the joining point of the lines A and B; erect a perpendicular BD (by prob. 5.) bisect AC in E (by prob. 4.) and describe the semicircle ADC; and from the point D, where the periphery cuts the perpendicular BD, draw the line BD, and that will be the mean proportional required.

For if the lines AD, DC, be drawn, the angle ADC is a right angle (by cor. 5. theo. 7.) being an angle in a semicircle.

The angles ABD, DBC, are right ones (by def. 10.) the line BD being a perpendicular; wherefore the triangles ABD, DBC, are similar: thus the angle ABD = DBC, being both right, the angle DAC is the complement of BDA to a right angle (by cor. 2. theo. 5.) and is therefore equal to BDC, the angle ADC being a right angle as before; consequently (by cor. 1. theo. 5.) the angle ADB = DCB, wherefore (by theo. 16.)

AB:BD::BD:BC: Or, A:BD::BD:B.

PROB. XIV.

PL. 3. fig. 2.

To divide a right line AB, in the point E, so that AE shall have the same proportion to EB, as two given lines C and D have.

Draw an indefinite blank line, AF, to the extremity of the line AB, to make with it any angle; lay the line C, from A to C; and D, from C to D; and join the points B and D, by the line BD; through C draw CE parallel to BD (by prob. 8.) so is E the point of division.

For, by cor. 1. theo. 20. AC:AD::AE:AB. Or, C:D::AE:EB.

PROB. XV.

PL. 3. fig. 3.

To describe a circle about a triangle ABC, or (which is the same thing) through any three points, A, B, C, which are not situated in a right line.

By prob. 4. Bisect the line AC by the perpendicular DE, and also CB, by the perpendicular FG, the point of intersection H, of these perpendiculars, is the centre of the circle required; from which take the distance to any of the three points A, B, C, and describe the circle ABC, and it is done.

For, by cor. to theo. 8. The lines DE and FG, must each pass through the centre, therefore, their point of intersection H, must be the centre.

SCHOLIUM.

By this method the centre of a circle may be found, by having only a segment of it given.

PROB, XVI.

PL. 3. fig. 4.

To make an angle of any number of degrees, at the point A, of the line AB, suppose of 45 degrees.

From a scale of chords take 60 degrees, for 60° is equal to the radius (by cor. theo. 15.) and with that distance from A, as a centre, describe a circle from the line AB; take 45 degrees, the quantity of the given angle, from the same scale of chords, and lay it on that circle from a to b; through A and b, draw the line AbC, and the angle A will be an angle of 45 degrees, as required.

If the given angle be more than 90°, take its half (or divide it into any two parts less than 90) and lay them after each other on the arc, which is described with the chord of 60 degrees; through the extremity of which, and the centre, let a line be drawn, and that will form the angle required, with the given line.

PROB. XVII.

P1. 3. fig. 5.

To measure a given angle, ABC.

If the lines which include the angle, be not as long as the chord of 60° on your scale, produce them to that or a greater length, and between them so produced, with the chord of 60° from B, describe the arc ed; which distance ed, measured on the same line of chords, gives the quantity of the angle BAC, as required; this is plain from def. 17.

PROB. XVIII.

PL. 3. fig. 6.

To make a triangle BCE equal to a given quadrilateral figure ABCD.

Draw the diagonal AC, and parallel to it (by prob. 8.) DE, meeting AB produced in E; then draw CE, and ECB will be the triangle required.

For the triangles ADC, AEC, being upon the same base AC, and under the same parallel ED, (by cor. to theo. 13.) will be equal, therefore if ABC be added to each, then ABCD = BEC.

PROB. XIX.

PL. 3. fig. 7,

To make a triangle DFH, equal to a given five-sided figure ABCDE.

Draw DA and DB, and also EH and CF, parallel to them (by prob. 8.) meeting AB produced in H and F; then draw DH, DF, and the triangle HDF is the one required.

For the triangle DEA = DHA, and DBC = DFB (by cor. to theo. 13.) therefore by adding these equations, DEA + DBC = DHA + DFB if to each of these ADB be added; then DEA + ADB + DBC = ABCDE = (DHA + ABD + DFB) = DHF.

PROB. XX.

PL. 3, fig. 8.

To project the lines of chords, sines, tangents and secants, with any radius.

On the line AB, let a semicircle ADB be described; let CDF be drawn perpendicular to this line from the centre C; and the tangent BE perpendicular to the end of the diameter; let the quadrants, AD, DB, be each divided into 9 equal parts, every one of which will be 10 degrees; if then from the centre C, lines be drawn through 10, 20, 30, 40, &c. the divisions of the quadrant BD, and continued to BE, we shall there have the tangents of 10, 20, 30, 40, &c. and the secants C 10, \check{C} 20, C 30, &c. are transferred to the line CF, by describing the arcs 10, 10: 20, 20: 30, 30, &c. If from 10, 20, 30, &c. the divisions of the quadrant BD, there be let fall perpendiculars, let these be transferred to the radius CB, and we shall have the sines of 10, 20, 30, &c. and if from A we describe the arcs 10, 10: 20, 20: 30, 30, &c. from every division of the arc AD; we shall have a line of chords. The same way we may have the sine, tangent, & c. to every single degree on the quadrant, by subdividing each of the 9 former divisions into 10 equal parts. By this method the sines, tangents, &c. may be drawn to any radius; and then, after they are transferred to lines on a rule, we shall have the scales of sines, tangents, &c. ready for use.

MATHEMATICAL

DRAWING INSTRUMENTS.

The strictness of geometrical demonstration admits of no other instruments, than a rule and a pair of compasses. But, in proportion as the practice of geometry was extended to the different arts, either connected with, or dependent upon it, new instruments became necessary, some to answer peculiar

purposes, some to facilitate operation, and others

to promote accuracy.

As almost every artist, whose operations are connected with mathematical designing, furnishes himself with a case of drawing instruments suited to his peculiar purposes, they are fitted up in various modes, some containing more, others, fewer instruments. The smallest collection put into a case, consists of a plane scale, a pair of compasses with a moveable leg, and two spare points, which may be applied occasionally to the compasses; one of these points is to hold ink; the other, a porte crayon, for holding a piece of black-lead pencil.

What is called a full pocket case, contains the

following instruments.

A pair of large compasses with a moveable point, an ink point, a pencil point, and one for dotting; either of those points may be inserted in the compasses, instead of the moveable leg.

A pair of plain compasses somewhat smaller

than those with the moveable leg.

A pair of bow compasses.

A drawing pen with a protracting pin in the upper part.

A sector.

A plain scale.

A protractor.

A parallel rule.

A pencil and screw-driver.*

Large collections are called, magazine cases of instru-

ments; these generally contain

A pair of six inch compasses with a moveable leg, an ink point, a dotting point, the crayon point, so contrived as to hold a whole pencil, two additional pieces to lengthen occasionally one leg of the compasses, and thereby enable them to measure greater extents, and describe circles of a larger radius.

A pair of hair compasses. A pair of bow compasses.

A pair of triangular compasses.

In a case with the best instruments, the protractor and plain scale are always combined. The instruments in most general use are those of six inches; instruments are seldom made longer, but often smaller. Those of six inches are, however, to be preferred, in general, before any other size; they will effect all that can be performed with the shortest ones, while, at the same time, they are better adapted to large work.

OF DRAWING COMPASSES.

Compasses are made either of silver or brass, but with steel points. The joints should always be framed of different substances; thus, one side, or part, should be of silver or brass, and the other of

A sector.

A parallel rule.

A protractor.

A pair of proportional compasses, either with or without an adjusting screw.

A pair of wholes and halves.

Two drawing pens, and a pointril.

A pair of small hair compasses, with a head similar to those of the bow compasses.

A knife, a file, key, and screw-driver, or the compasses in one piece.

A small set of fine water colours.

To these some of the following instruments are often added.

A pair of beam compasses. A pair of gunners callipers.

A pair of elliptical compasses.

A pair of spiral ditto.

A pair of perspective compasses.

A pair of compasses with a micrometer screw.

A rule for drawing lines, tending to a centre at a great distance.

A protractor and parallel rule.

One or more parallel rules.

A pantographer, or Pentagraph.

A pair of sectoral compasses, forming, at the same time, a pair of beam and calliper compasses.

steel. The difference in the texture and pores of the two metals causes the parts to adhere less together, diminishes the wear, and promotes uniformity in their motion. The truth of the work is ascertained by the smoothness and equality of the motion at the joint, for all shake and irregularity is a certain sign of imperfection. The points should be of steel, so tempered, as neither to be easily bent or blunted; not too fine and tapering, and yet meeting closely when the compasses are shut.

As an instrument of art, compasses are so well known, that it would be superfluous to enumerate the various uses; suffice it then to say, that they are used to transfer small distances, measure given

spaces, and describe arches and circles.

If the arch or circle is to be described obscurely, the steel points are best adapted to the purpose; if it is to be in ink or black lead, either the draw-

ing pen, or crayon points are to be used.

To use a pair of compasses. Place the thumb and middle finger of the right hand in the opposite hollows in the shanks of the compasses, then press the compasses, and the legs will open a little way; this being done, push the innermost leg, with the third finger, elevating, at the same time, the furthermost, with the nail of the middle finger, till the compasses are sufficiently opened to receive the middle and third finger; they may then be extended at pleasure, by pushing the furthermost leg outwards with the middle, or pressing it inwards with the four finger. In describing circles, or arches, set one foot of the compasses on the centre, and then roll the head of the compasses between the middle and four finger, the other point pressing at the same time upon the paper. They should be held as upright as possible, and care should be taken not to press forcibly upon them, but rather to let them act by their own weight; the legs should never be so far extended, as to form

an obtuse angle with the paper or plane, on which

they are used.

The ink and crayon points have a joint just under that part which fits into the compasses; by this they may be always so placed as to be set nearly perpendicular to the paper; the end of the shank of the best compasses is framed so as to form a strong spring, to bind firmly the moveable points, and prevent them from shaking. This is found to be a more effectual method than that by a screw.

Two additional pieces are often applied to these compasses; these, by lengthening the leg, enable them to strike larger circles, or measure greater extents, than they would otherwise perform, and that without the inconveniences attending longer compasses. When compasses are furnished with this additional piece, the moveable leg has a joint, that it may be placed perpendicular to the paper.

The bow compasses, are a small pair, usually with a point for ink; they are used to describe small arches or circles, which they do much more conveniently than large compasses, not only on account of their size, but also from the shape of the head, which rolls with great ease between the fingers.

Of the drawing pen and protracting pin. The pen part of this instrument is used to draw strait lines: it consists of two blades with steel points fixed to a handle; the blades are so bent, that the ends of the steel points meet, and yet leave a sufficient cavity for the ink; the blades may be opened more or less by a screw, and, being properly set, will draw a line of any assigned thickness. One of the blades is framed with a joint, that the points may be separated, and thus cleaned more conveniently; a small quantity only of ink should be put at one time into the drawing pen, and this should be placed in the cavity, between the blades, by a common pen, or feeder; the drawing pen acts

better, if the pen, by which the ink is inserted, be made to pass through the blades. To use the drawing pen, first feed it with ink, then regulate it to the thickness of the required line by the screw. In drawing lines, incline the pen a small degree, taking care, however, that the edges of both the blades touch the paper, keeping the pen close to the rule, and in the same direction during the whole operation: the blades should always be wiped very clean, before the pen is put away.

These directions are equally applicable to the ink point of the compasses, only observing, that when an arch or circle is to be described, of more than an inch radius, the point should be so bent, that the blades of the pen may be nearly perpendicular to the paper, and both of them touch it at

the same time.

The protracting pin, is only a short piece of steel wire, with a very fine point, fixed at one end of the upper part of the handle of the drawing pen. It is used to mark the intersection of lines, or to set off divisions from the plotting scale, and protractor.

OF THE SECTOR.

Amidst the variety of mathematical instruments that have been contrived to facilitate the art of drawing, there is none so extensive in its use, or of such general application, as the sector. It is an universal scale, uniting, as it were, angles and parallel lines, the rule and the compass, which are the only means that geometry makes use of for measuring, whether in speculation or practice. The real inventor of this valuable instrument is unknown; yet of so much merit has the invention appeared, that it was claimed by Galileo, and disputed by nations.

This instrument derives its name from the tenth definition of the third book of *Euclid*, where he defines the sector of a circle. It is formed of two equal rules called legs; these legs are moveable about the centre of a joint, and will, consequently, by their different openings, represent every possible variety of plane angles. The distance of the extremities of these rules are the subtenses or chords,

or the arches they describe.

Sectors are made of different sizes, but their length is usually denominated from the length of the legs when the sector is shut. Thus a sector of six inches, when the legs are close together, forms a rule of 12 inches when opened; and a foot sector is two feet long, when opened to its greatest extent. In describing the lines usually placed on this instrument, I refer to those commonly laid down on the best six-inch brass sectors. But as the principles are the same in all, and the differences little more than in the number of subdivisions, it is to be presumed that no difficulty will occur in the application of what is here said to sectors of a larger radius.

The scales, or lines graduated upon the faces of the instrument, and which are to be used as sectoral lines, proceed from the centre; and are, 1. Two scales of equal parts, one on each leg, marked LIN. or L. Each of these scales, from the great extensiveness of its use, is called the line of lines.

2. Two lines of chords, marked cho. or c. 3. Two lines of secants, marked sec. or s. A line of polygons, marked pol. Upon the other face, the sectoral lines are, 1. Two lines of sines marked sin. or s.

2. Two lines of tangents, marked tan. 3. Between the lines of tangents and sines, there is another line of tangents to a lesser radius, to supply the defect of the former, and extending from 45° to 75°.

Each pair of these lines (except the line of polygons) is so adjusted as to make equal angles at the centre, and consequently at whatever distance the sector be opened, the angles will be always respectively equal. That is, the distance between 10 and 10 on the line of lines, will be equal to 60 and 60 on the line of chords, 90 and 90 on the line of sines, and 45 and 45 on the line of tangents.

Besides the sectoral scales, there are others on each face, placed parallel to the outward edges, and used as those of the common plain scale. There are on the one face, 1. A line of inches. 2. A line of latitudes. 3. A line of hours. 4. A line of inclination of meridians. 5. A line of chords. On the other face, three logarithmic scales, namely, one of numbers, one of sines, and one of tangents; these are used when the sector

is fully opened, the legs forming one line.

To read and estimate the divisions on the sectoral lines. The value of the divisions on most of the lines are determined by the figures adjacent to them; these proceed by tens, which constitute the divisions of the first order, and are numbered accordingly; but the value of the divisions on the line of lines, that are distinguished by figures, is entirely arbitrary, and may represent any value that is given to them; hence the figures 1, 2, 3, 4, &c. may denote either 10, 20, 30, 40; or 100, 200, 300, 400, and so on.

The line of lines is divided into ten equal parts, numbered 1, 2, 3, to 10; these may be called divisions of the first order; each of these are again subdivided into 10 other equal parts, which may be called divisions of the second order; and each of these is divided into two equal parts, forming divisions of the third order.

The divisions on all the scales are contained between four parallel lines; those of the first order extend to the most distant; those of the third, to the least; those of the second, to the intermediate

parallel.

When the whole line of lines represents 100, the divisions of the first order, or those to which the figures are annexed, represent tens; those of the second order, units; those of the third order, the halves of these units. If the whole line represents ten, then the divisions of the first order are units; those of the second, tenths, and the thirds, twentieths.

In the line of tangents, the divisions to which the numbers are affixed, are the degrees expressed by those numbers. Every fifth degree is denoted by a line somewhat longer than the rest; between every number and each fifth degree, there are four divisions, longer than the intermediate adjacent ones, these are whole degrees; the shorter ones, or those of the third order, are 30 minutes.

From the centre, to 60 degrees, the line of sines is divided like the line of tangents; from 60 to 70, it is divided only to every degree; from 70 to 80, to every two degrees; from 80 to 90, the division

must be estimated by the eye.

The divisions on the line of chords are to be es-

timated in the same manner as the tangents.

The lesser line of tangents is graduated every two degrees from 45 to 50; but from 50 to 60, to every degree; from 60 to the end, to half degrees.

The line of secants from 0 to 10, is to be estimated by the eye; from 20 to 50 it is divided to every two degrees; from 50 to 60, to every degree; and from 60 to the end, to every half degree.

The solution of questions on the sector is said to be *simple*, when the work is begun and ended on the same line; *compound*, when the operation begins on one line, and is finished on the other.

The operation varies also by the manner in which the compasses are applied to the sector. If a mea-

gure be taken on any of the sectoral lines, beginning at the centre, it is called a lateral distance. But if the measure be taken from any point in one line, to its corresponding point on the line of the same denomination, on the other leg, it is called a transverse or parallel distance.

The divisions of each sectoral line are bounded by three parallel lines; the innermost of these is that on which the points of the compasses are to be placed, because this alone is the line which goes to the centre, and is alone, therefore, the sectoral line.

We shall now proceed to give a few general instances of the manner of operating with the sector.

Multiplication by the line of lines. Make the lateral distance of one of the factors the parallel distance of 10; then the parallel distance of the

other factor is the product.

Example. Multiply 5 by 6, extend the compasses from the centre of the sector to 5 on the primary divisions, and open the sector till this distance become the parallel distance from 10 to 10 on the same divisions; then the parallel distance from 6 to 6, extended from the centre of the sector, shall reach to 3, which is now to be reckoned 30. At the same opening of the sector, the parallel distance of 7 shall reach from the centre to 35, that of 8 shall reach from the centre to 40, &c.

Division by the line of lines. Make the lateral distance of the dividend the parallel distance of the divisor, the parallel distance of 10 is the quotient. Thus, to divide 30 by 5, make the lateral distance of 30, viz. 3 on the primary divisions, the parallel distance of 5 of the same divisions; then the parallel distance of 10, extended from the centre,

shall reach to 6.

Proportion by the line of lines. Make the lateral distance of the second term the parallel distance

of the first term; the parallel distance of the third

term is the fourth proportional.

Example. To find a fourth proportional to 8, 4, and 6, take the lateral distance of 4, and make it the parallel distance of 8; then the parallel distance of 6, extended from the centre, shall reach

to the fourth proportional 3.

In the same manner a third proportional is found to two numbers. Thus, to find a third proportional to 8 and 4, the sector remaining as in the former example, the parallel distance of 4, extended from the centre, shall reach to the third proportional 2. In all these cases, if the number to be made a parallel distance be too great for the sector, some aliquot part of it is to be taken, and the answer multiplied by the number by which the first number was divided. Thus, if it were required to find a fourth proportional to 4, 8, and 6; because the lateral distance of the second term 8 cannot be made the parallel distance of the first term 4, take the lateral distance of 4, viz. the half of 8, and make it the parallel distance of the first term 4; then the parallel distance of the third term 6, shall reach from the centre to 6, viz. the half of 12. Any other aliquot part of a number may be used in the same way. In like manner, if the number proposed be too small to be made the parallel distance, it may be multiplied by some number, and the answer is to be divided by the same number.

To protract angles by the line of Chords. Case
1. When the given degrees are under 60. 1. With
any radius on a centre, describe the arch. 2. Make
the same radius a transverse distance between 60
and 60 on the line of chords. 3. Take out the
transverse distance of the given degrees, and lay
this on the arch, which will mark out the angular

distance required.

Case 2. When the given degrees are more than

60. 1. Open the sector, and describe the arch as before. 2. Take $\frac{1}{2}$ or $\frac{1}{3}$ of the given degrees, and take the transverse distance of this $\frac{1}{2}$ or $\frac{1}{3}$, and lay it off twice, if the degrees were halved, three times if the third was used as a transverse distance.

Case 3. When the required angle is less than 6 degrees; suppose 3. 1. Open the sector to the given radius, and describe the arch as before. 2. Set off the radius. 3. Set off the chord of 57 degrees backwards, which will give the arc of three degrees.

Given the radius of a circle, (suppose equal to two inches,) required the sine and tangent of 28° 30'

to that radius.

Solution. Open the sector so that the transverse distance of 90 and 90 on the sines, or of 45 and 45 on the tangents, may be equal to the given radius, viz. two inches; then will the transverse distance of 38° 30', taken from the sines, be the length of that sine to the given radius; or if taken from the tangents; will be the length of that tangent to the given radius.

But if the secant of 28° 30' was required?

Make the given radius, two inches, a transverse distance to 0 and 0, at the beginning of the line of secants; and then take the transverse distance of the degrees wanted, viz. 28° 30′.

A tangent greater than 45° (suppose 60°) is

found thus.

Make the given radius, suppose two inches, a transverse distance to 45 and 45 at the beginning of the scale of upper tangents; and then the required number 60°00′may be taken from this scale.

Given the length of the sine, tangent, or secant of any degrees; to find the length of the radius to that

sine, tangent, or secant.

Make the given length a transverse distance to its given degrees on its respective scale: then,

In the sines. The transverse distance of 90 and

90 will be the radius sought.

In the lower tangents. The transverse distance of 45 and 45, near the end of the sector, will be the radius sought.

In the upper tangents. The transverse distance of 45 and 45, taken towards the centre of the sector on the line of upper tangents, will be the centre sought.

In the secant. The transverse distance of 0 and 0, or the beginning of the secants, near the centre of the sector, will be the radius sought.

Given the radius and any line representing a sine, tangent, or secant; to find the degrees corresponding to that line.

Solution. Set the sector to the given radius, according as a sine, or tangent, or secant is concerned.

Take the given line between the compasses; apply the two feet transversely to the scale concerned, and slide the feet along till they both rest on like divisions on both legs; then will those divisions shew the degrees and parts corresponding to the given line.

To find the length of a versed sine to a given number of degrees, and a given radius.

Make the transverse distance of 90 and 90 on

the sines, equal to the given radius.

Take the transverse distance of the sine com-

plement of the given degrees.

If the given degrees are less than 90, the difference between the sine complement and the radius gives the versed sine.

If the given degrees are more than 90, the sum of the sine complement and the radius gives the

versed sine.

To open the legs of the sector, so that the corres-

ponding double scales of lines, chords, sines, and

tangents, may make each a right angle.

On the lines, make the lateral distance 10, a distance between eight on one leg, and six on the other leg.

On the sines, make the lateral distance 90 a transverse distance from 45 to 45; or from 40 to 50; or from 30 to 60; or from the sine of any degrees to their complement.

Or on the sines, make the lateral distance of 45

a transverse distance between 30 and 30.

OF THE PLAIN SCALE.

The divisions laid down on the plain scale are of two kinds, the one having more immediate relation to the circle and its properties, the other being merely concerned with dividing straight lines.

Though arches of a circle are the most natural measures of an angle, yet in many cases right lines are substituted, as being more convenient; for the comparison of one right line with another, is more natural and easy, than the comparison of a right line with a curve; hence it is usual to measure the quantities of angles not by the arch itself, which is described on the angular point, but by certain lines described about that arch.

The lines laid down on the plain scales for the measuring of angles, or the protracting scales, are, 1. A line of chords marked cho. 2. A line of sines marked sin. of tangents marked tan. of semitangents marked st. and of secants marked sec. this last is often upon the same line as the sines, because its gradations do not begin till the sines end.

There are two other scales, namely, the rhumbs, marked RU. and longitudes, marked LON. Scales of latitude and hours are sometimes put upon the

plain scale; but, as dialling is now but seldom

studied, they are only made to order.

The divisions used for measuring straight lines are called scales of equal parts, and are of various lengths for the convenience of delineating any figure of a large or smaller size, according to the fancy or purposes of the draughts-man. They are, indeed, nothing more than a measure in miniature for laying down upon paper, &c. any known measure, as chains, yards, feet, &c. each part on the scale answering to one foot, one yard, &c. and the plan will be larger or smaller, as the scale contains a smaller or a greater number of parts in an inch. Hence a variety of scales is useful to lay down lines of any required length, and of a convenient proportion with respect to the size of the drawing. If none of the scales happen to suit the purpose, recourse should be had to the line of lines on the sector; for, by the different openings of that instrument, a line of any length may be divided into as many equal parts as any person chooses.

Scales of equal parts are divided into two kinds,

the one simple, the other diagonally divided.

Six of the simply divided scales are generally placed one above another upon the same rule; they are divided into as many equal parts as the length of the rule will admit of; the numbers placed on the right hand, shew how many parts in an inch each scale is divided into. The upper scale is sometimes shortened for the sake of introducing another, called the line of chords.

The first of the larger, or primary divisions, on every scale is subdivided into 10 equal parts, which small parts are those which give a name to the scale: thus it is called a scale of 20, when 20 of these divisions are equal to one inch. If, therefore, these lesser divisions be taken as units, and each represents one league, one mile, one chain, or one yard.

&c. then will the larger divisions be so many tens; but if the subdivisions are supposed to be tens, the

larger divisions will be hundreds.

To illustrate this, suppose it were required to set off from either of the scales of equal parts \$\frac{12}{10}\$, 36, or 360 parts, either miles or leagues. Set one foot of your compasses on 3, among the larger or primary divisions, and open the other point till it falls on the 6th subdivision, reckoning backwards or towards the left hand. Then will this extent represent, \$\frac{36}{10}\$ 36, or 360 miles or leagues, &c. and bear the same proportion in the plan as the line measured does to the thing represented.

To adapt these scales to feet and inches, the first primary division is often duodecimally divided by an upper line; therefore, to lay down any number of feet and inches, as for instance, eight feet eight inches, extend the compasses from eight of the larger to eight of the upper small ones, and that distance laid down on the plan will repre-

sent eight feet eight inches.

Of the scale of equal parts diagonally divided. The use of this scale is the same as those already described. But by it a plane may be more accurately divided than by the former; for any one of the larger divisions may by this be subdivided into 100 equal parts; and, therefore, if the scale contains 10 of the larger divisions, any number under

1000 may be laid down with accuracy.

The diagonal scale is seldom placed on the same side of the rule with the other plotting scale. The first division of the diagonal scale, if it be a foot long, is generally an inch divided into 100 equal parts, and at the opposite end there is usually half an inch divided into an 100 equal parts. If the scale be six inches long, one end has commonly half an inch, the other a quarter of an inch subdivided into 100 equal parts.

N

The nature of this scale will be better understood by considering its construction. For this

purpose:

First. Draw eleven parallel lines at equal distances; divide the upper of these lines into such a number of equal parts, as the scale to be expressed is intended to contain; from each of these divisions draw perpendicular lines through the eleven parallels.

Secondly. Subdivide the first of these divisions into ten equal parts, both in the upper and lower

lines.

Thirdly. Subdivide again each of these subdivisions, by drawing diagonal lines from the 10th below to the 9th above; from the 8th below to the 7th above; and so on, till from the first below to the 0 above; by these lines each of the small divisions is divided into ten parts, and, consequently, the whole first space into 100 equal parts; for, as each of the subdivisions is one-tenth part of the whole first space or division, so each parallel above it is one-tenth of such subdivision, and, consequently, one-hundreth part of the whole first space: and if there be ten of the larger divisions, one-thousandth part of the whole space.

If, therefore, the larger divisions be accounted as units, the first subdivisions will be tenth parts of an unit, and the second, marked by the diagonal upon the parallels, hundreth parts of the unit. But, if we suppose the larger divisions to be tens, the first subdivisions will be units, and the second tenths. If the larger are hundreds, then will the

first be tens, and the second units.

The numbers therefore, 576, 57,6, 5,76, are all expressible by the same extent of the compasses: thus setting one foot in the number five of the larger divisions, extend the other along the sixth parallel to the seventh diagonal. For, if the five

larger divisions be taken for 500, seven of the first subdivisions will be 70, which upon the sixth parallel, taking in six of the second subdivisions for units, makes the whole number 576. Or, if the five larger divisions be taken for five tens, or 50, seven of the first subdivisions will be seven units, and the six second subdivisions upon the sixth parallel, will be six tenths of an unit. Lastly, if the five larger divisions be only esteemed as five units, then will the seven first subdivisions be seven tenths, and the six second subdivisions be the six hundredth parts of an unit.

Of the line of chords. This line is used to set off an angle from a given point in any right line, or to measure the quantity of an angle already

laid down.

Thus to draw a line that shall make with another line an angle, containing a given number of

degrees, suppose 40 degrees.

Open your compasses to the extent of 60 degrees upon the line of chords, (which is always equal to the radius of the circle of projection,) and setting one foot in the angular point, with that extent describe an arch; then taking the extent of 40 degrees from the said chord line, set it off from the given line on the arch described; a right line drawn from the given point, through the point marked upon the arch, will form the required angle.

The degrees contained in an angle already laid down, are found nearly in the same manner; for instance, to measure an angle. From the centre describe an arch with the chord of 60 degrees, and the length of the arch, contained between the lines measured on the line of chords, will give the num-

ber of degrees contained in the angle.

If the number of degrees are more than 90, they must be measured upon the chords at twice: thus, if 120 degrees were to be practised,60 may be taken from the chords, and those degrees be laid off

twice upon the arch. Degrees taken from the chords are always to be counted from the begin-

ning of the scale.

Of the rhumb line. This is, in fact, a line of chords constructed to a quadrant divided into eight parts or points of the compass, in order to facilitate the work of the navigator in laying

down a ship's course.

Of the line of longitudes. The line of longitudes is a line divided into sixty unequal parts, and so applied to the line of chords, as to shew, by inspection, the number of equatorial miles contained in a degree on any parallel of latitude. The graduated line of chords is necessary, in order to shew the latitudes; the line of longitude shews the quantity of a degree on each parallel in sixtieth parts of an equatorial degree, that is, miles.

The lines of tangents, semitangents, and secants, serve to find the centres and poles of projected circles in the stereographical projection of the sphere.

The line of sines is principally used for the or-

thographic projection of the sphere.

The lines of latitudes and hours are used conjointly, and serve very readily to mark the hour lines in the construction of dials; they are generally on the most complete sorts of scales and sectors; for the uses of which see treatises on dialling.

OF THE PROTRACTOR.

This is an instrument used to protract, or lay down an angle containing any number of degrees, or to find how many degrees are contained in any given angle. There are two kinds put into cases of mathematical drawing instruments; one in the form of a semicircle, the other in the form of a parallelogram. The circle is undoubtedly the only natural measure of angles; when a straight line is therefore used, the divisions thereon are derived

from a circle, or its properties, and the straight line is made use of for some relative convenience: it is thus the parallelogram is often used as a protractor, instead of the semicircle, because it is in some cases more convenient, and that other scales, &c.

may be placed upon it.

The semicircular protractor, is divided into 180 equal parts or degrees, which are numbered at every tenth degree each way, for the conveniency of reckoning either from the right towards the left, or from the left towards the right; or the more easily to lay down an angle from either end of the line, beginning at each end with 10, 20, &c. and proceeding to 180 degrees. The edge is the diameter of the semicircle, and the mark in the middle points out the centre, in a protractor in the form of a parallelogram: the divisions are as in the semicircular one, numbered both ways; the blank side represents the diameter of a circle. The side of the protractor to be applied to the paper is made flat, and that whereon the degrees are marked, is chamfered or sloped away to the edge, that an angle may be more easily measured, and the divisions set off with greater exactness.

Application of the protractor to use. 1. A number of degrees being given, to protract, or lay down an angle, whose measure shall be equal thereto.

Thus, to lay down an angle of 60 degrees from the point of a line, apply the diameter of the protractor to the line, so that the centre thereof may coincide exactly with the extremity; then with a protracting pin make a fine dot against 60 upon the limb of the protractor; now remove the protractor, and draw a line from the extremity through that point, and the angle contains the given number of degrees.

2. To find the number of degrees contained in a given angle.

Place the centre of the protractor upon the angular point, and the fiducial edge, or diameter, exactly upon the line; then the degree upon the limb that is cut by the line will be the measure of the given angle, which, in the present instance, is found to be 60 degrees.

3. From a given point in a line, to erect a perpen-

dicular to that line.

Apply the protractor to the line, so that the centre may coincide with the given point, and the division marked 90 may be cut by the line; then a line drawn against the diameter of the protractor will be the perpendicular required.

OF PARALLEL RULES.

Parallel lines occur so continually in every species of mathematical drawing, that it is no wonder so many instruments have been contrived to delineate them with more expedition than could be effected by the general geometrical methods. For this purpose, rules of various constructions have been made; and particularly recommended by their inventors; their use however is so apparent as to need no explanation.

GUNTER'S SCALE.

The scale generally used is a ruler of two feet in length, having drawn upon it equal parts, chords, sines, tangents, secants, &c. These are contained on one side of the scale, and the other side contains the logarithms of these numbers. Mr. Edmund Gunter was the first who applied the logarithms of numbers, and of sines and tangents to straight lines drawn on a scale or ruler; with which, proportions in common numbers, and trigonometry, may be solved by the application of a pair of compasses

only. The method is founded on this property, That the logarithms of the terms of equal ratios are equidifferent. This was called Gunter's Proportion, and Gunter's Line; hence the scale is generally called the Gunter.

Of the Logarithmical Lines, or Gunter's Scale. The logarithmical lines, on Gunter's scale, are

the eight following:

S. Rhumb, or fine rhumbs, is a line containing the logarithms of the natural sines of every point and quarter point of the compass, numbered from a brass pin on the right hand towards the left with

8, **7**, **6**, **5**, **4**, **3**, **2**, **1**.

T*Rhumb, or tangent rhumbs, also corresponds to the logarithm of the tangent of every point and quarter point of the compass. This line is numbered from near the middle of the scale with 1.2.3.4 towards the right hand, and back again with the numbers 5, 6, 7 from the right hand towards the left. To take off any number of points below four, we must begin at 1, and count towards the right hand; but to take off any number of points above four, we must begin at four, and count towards the left hand.

Numbers, or the line of numbers, is numbered from the left hand of the scale towards the right, with 1, 2, 3, 4, 5, 6, 7, 8, 9, 1 which stands exactly in the middle of the scale; the numbers then go on 2, 3, 4, 5, 6, 7, 8, 9, 10 which stands at the right hand end of the scale. These two equal parts of the scale are divided equally, the distance between the first or left hand 1, and the first 2, 3, 4, &c. is exactly equal to the distance between the middle 1 and the numbers 2, 3, 4, &c. which follow it. The subdivisions of these scales are likewise similar, viz. they are each one-tenth of the primary divisions, and are distinguished by lines of about half the length of the primary divisions.

These subdivisions are again divided into tent parts, where room will permit; and where that is not the case, the units must be estimated, or guessed at, by the eye, which is easily done by a little

practice.

The primary divsions on the second part of the scale, are estimated according to the value set upon the unit on the left hand of the scale: If you call it one, then the first 1, 2, 3, &c. stand for 1, 2, 3, &c. the middle 1 is 10, and the 2. 3. 4. &c. following stand for 20, 30, 40, &c. and the ten at the right hand is 100: If the first 1 stand for 10, the first 2, 3, 4, &c. must be counted 20, 30, 40, &c. the middle 1 will be 100, the second 2, 3, 4, 5, &c. will stand for 200, 300, 400, 500, &c. and the ten at the right hand for 1000.

If you consider the first 1 as $\frac{1}{10}$ of an unit, the 2, 3, 4, &c. following will be $\frac{1}{10}$, $\frac{1}{10}$, &c. the middle 1 will stand for an unit, and the 2, 3, 4, &c. following will stand for 2, 3, 4, &c. also the division at the right-hand end of the scale will stand for 10. The intermediate small divisions must be estimated according to the value set upon the primary ones.

Sine. The line of sines is numbered from the left hand of the scale towards the right, 1, 2, 3, 4, 5, &c. to 10; then 20, 30, 40, &c. to 90, where it terminates just opposite 10 on the line of numbers.

Versed sine. This line is placed immediately under the line of sines, and numbered in a contrary direction, viz. from the right hand towards the left 10, 20, 30, 40, 50, to about 169; the small divisions are here to be estimated according to the number of them to a degree. By comparing the line of versed sines with the line of sines, it will appear that the versed sines do not belong to the arches with which they are marked, but are the half versed sines of their supplements. Thus, what is marked the versed sine of 90 is only half the versed sine of 90,

the versed sine of 120° is half the versed sine of 60°, and the versed sine marked 100° is half the versed sine of 80°, &c.

The versed sines are numbered in this manner to render them more commodious in the solution of trigonometrical, and astronomical problems.

Tangents. The line of tangents begins at the left hand, and is numbered 1, 2, 3, &c. to 10, then 20, 30, 45, where there is a little brass pin just under 90 in the line of sines; because the sine of 90° is equal to the tangent of 45°. It is numbered from 45° towards the left hand 50, 60, 70, 80, &c. The tangents of arches above 45° are therefore counted backward on the line, and are found at the same points of the line as the tangents of their complements.

Thus, the division at 40 represents both 40 and 50, the division at 30 serves for 30 and 60, &c.

Meridional Parts. This line stands immediately above a line of equal parts, marked Equal Pt. with which it must always be compared when used. The line of equal parts is marked from the right hand to the left with 0, 10, 20, 30, &c.; each of these large divisions represents 10 degrees of the equator, or 600 miles. The first of these divisions is sometimes divided into 40 equal parts, each representing 15' minutes or miles.

The extent from the brass pin on the scale of meridional parts to any division on that scale, applied to the line of equal parts, will give (in degrees) the meridional parts answering to the latitude of that division. Or the extent from any division to another, on the line of meridional parts, applied to the line of equal parts, will give the meridional difference of latitude between the two places denoted by the divisions. These degrees are reduced to leagues by multiplying by 20, or to miles by multiplying by 60.

The use of the logarithmical lines on Gunter's Scale.

By these lines and a pair of compasses, all the problems of Trigonometry, &c. may be solved.

These problems are all solved by proportion; Now in natural numbers, the quotient of the first term by the second is equal to the quotient of the third by the fourth: therefore logarithmically speaking the difference between the first and second term is equal to the difference between the third and fourth, consequently on the lines on the scale, the distance between the first and second term will be equal to the distance between the third and fourth. And for a similar reason, because four proportional quantities are alternately proportional, the distance between the first and third terms, will be equal to the distance between the second and fourth. Hence the following

General.Rule.

The extent of the compasses from the first term to the second, will reach, in this same direction, from the third to the fourth term. Or, the extent of the compasses from the first term to the third, will reach, in the same direction, from the second to the fourth.

By the same direction in the foregoing rule, is meant that if the second term lie on the right hand of the first, the fourth will lie on the right hand of the third, and the contrary. This is true, except the two first or two last terms of the proportion are on the line of tangents, and neither of them under 45°; in this case the extent on the tangents is to be made in a contrary direction: For had the tangents above 45° been laid down in their proper direction, they would have extended beyond the length of the scale towards the right hand; they are therefore as it were folded back up-

on the tangents below 45°, and consequently lie in a direction contrary to their proper and natural order.

If the two last terms of a proportion be on the line of tangents, and one of them greater and the other less than 45°; the extent from the first term to the second will reach from the third beyond the scale. To remedy this inconvenience, apply the extent between the two first terms from 45° backward upon the line of tangents, and keep the left hand point of the compasses where it falls; bring the right hand point from 45° to the third term of the proportion; this extent now in the compasses applied from 45° backward will reach to the fourth term, or the tangent required. For, had the line of tangents been continued forward beyond 45°, the divisions would have fallen above 45° forward; in the same manner as they fall under 45° backward.

SECTION V.

TRIGONOMETRY.

The word Trigonometry signifies the measuring of triangles. But, under this name is generally comprehended the art of determining the positions and dimensions of the several unknown parts of extension, by means of some parts, which are already known. If we conceive the different points, which may be represented in any space, to be joined together by right lines, there are three things offered for our consideration; 1. the length of these lines; 2. the angles which they form with one another; 3. the angles formed by the planes, in which these lines are drawn, or are supposed to be traced. On the comparison of these three objects,

depends the solution of all questions, that can be proposed concerning the measure of extension, and its parts; and the art of determining all these things from the knowledge of some of them, is reduced to the solution of these two general questions.

1. Knowing three of the six parts, the sides and angles—which constitute a rectilineal triangle; to

find the other three.

2. Knowing three of the six parts, which compose a spherical triangle; that is a triangle formed on the surface of a sphere by three arches of circles, which have their centre in the centre of the

same sphere—to find the other three.

The first question is the object of what is called Plane Trigonometry, because the six parts, considered here, are in the same plane: it is also denominated Rectilineal Trigonometry. The second question belongs to Spherical Trigonometry, wherein the six parts are considered in different planes. But the only object here is to explain the solutions of the former question: viz.

PLANE TRIGONOMETRY.

Plane Trigonometry is that branch of geometry, which teaches how to determine, or calculate three of the six parts of a rectilineal triangle by having the other three parts given or known. It is usually divided into Right angled and Oblique angled Trigonometry, according as it is applied to the mensuration of Right or Oblique angled Triangles.

In every triangle, or case in trigonometry, three of the parts must be given, and one of these parts, at least, must be a side; because, with the same angles, the sides may be greater or less in any

proportion,

RIGHT ANGLED PLANE TRIGONOMETRY.

· P1.5. Fig. 1.

1. In every right-angled plane triangle ABC, if the hypothenuse AC be made the radius, and with it a circle, or an arc of one, be described from each end; it is plain (from def. 20.) that BC is the sine of the angle A, and AB is the sine of the angle C; that is, the legs are the sines of their opposite angles.

Fig. 2.

If one leg AB be made the radius, and with it, on the point A, an arc be described; then BC is the tangent, and AC is the secant of the angle A, by def. 22 and 25.

Fig. 3.

3. If BC be made the radius, and an arc be described with it on the point C; then is AB the tangent, and AC is the secant of the angle C, as before.

Because the sine, tangent, or secant of any given arc, in one circle, is to the sine, tangent, or secant of a like arc (or to one of the like number of degrees) in another circle; as the radius of the one is to the radius of the other; therefore the sine, tangent, or secant of any arc is proportional to the sine, tangent, or secant of a like arc, as the radius of the given arc is to 10.000000, the radius from whence the logarithmic sines, tangents, and secants, in most tables, are calculated, that is;

If AC be made the radius, the sines of the angle A and C, described by the radius AC, will be proportional to the sines of the like arcs, or angles in the circle, that the tables now mentioned were

calculated for. So if BC was required, having the angles and AB given, it will be,

Fig. 1.

As S.C:AB::S.A:BC.

That is, as the sine of the angle C in the tables, is to the length of AB; (or sine of the angle C, in a circle whose radius is AC;) so is the sine of the angle A in the tables, to the length of BC. (or sine of the same angle, in the circle, whose radius is AC.)

In like manner the tangents and secants represented by making either leg the radius, will be proportional to the tangents and secants of a like arc, as the radius of the given arc is to 10.000000,

the radius of the tables aforesaid.

Hence it is plain, that if the name of each side of the triangle be placed thereon, a proportion will arise to answer the same end as before: thus if AC be made the radius, let the word radius be written thereon; and as BC and AB, are the sines of their opposite angles; upon the first let SA, or sine of the angle A, and on the other let SC, or sine of the angle C, be written. Then,

When a side is required, it may be obtained by

this proportion, viz.

As the name of the side given

is to the side given,

So is the name of the side required

to the side required.

Thus, if the angles \mathcal{A} and \mathcal{C} , and the hypothenuse $\mathcal{A}\mathcal{C}$ were given, to find the sides; the proportion will be

Fig. 1.

1. R : AC :: S.A : BC.

That is, as radius is to AC, so is the sine of the angle A, to BC. And,

 $\mathbf{\tilde{2}}.\ \mathbf{R}:\mathbf{AC}::\mathbf{S.C}:\mathbf{AB}.$

That is, as radius is to AC, so is the sine of the angle C to AB.

When an angle is required, we use this propor-

tion, viz.

As the side that is made the radius,

is to radius,

So is the other given side,

to its name.

Thus, if the legs were given to find the angle A, and if AB be made the radius, it will be

Fig. 2.

AB:R::BC:TA.

That is, as AB, is to radius, so is BC, to the tan-

gent of the angle A:

After the same manner, the sides or angles of all right angled plane triangles may be found, from their proper data.

We here, in plate 4, give all the proportion requisite for the solution of the six cases in right-angled trigonometry; making every side possible

the radius.

In the following triangles this mark—in an angle denotes it to be known, or the quantity of degrees it contains to be given; and this mark' on a side, denotes its length to be given in feet, yards, perches, or miles, &c. and this mark', either in an angle or on a side, denotes the angle or side to be required.

From these proportions it may be observed; that to find a side, when the angles and one side are given, any side may be made the radius; and

to find an angle, one of the given sides must be made the radius. So that in the 1st, 2d, and 3d cases, any side as well required as given may be made the radius, and in the first statings of the 4th, 5th, and 6th cases, a given side only is made the radius.

RIGHT ANGLED TRIANGLES.

CASE I.

The angles and hypothenuse given, to find the base and per-

PL. 5. Fig. 4.

In the right angled triangle ABC, suppose the angle $A = 46^{\circ}$. 30. and consequently the angle $C = 43^{\circ}$. 30'. (by cor. 2. theo. 5.); and AC 250 parts, (as feet, yards, miles, &c.) required the sides AB and BC.

1st. BY CONSTRUCTION.

Make an angle of 46°. 30′, in blank lines, (by prob. 16. geom.) as CAB; lay 250, which is the given hypothenuse, from a scale of equal parts, from A to C; from C, let fall the perpendicular (BC, by prob. 7. geom.) and that will constitute the triangle ABC. Measure the lines BC, and AB, from the same scale of equal parts that AC was taken from; and you have the answer.

2d. BY CALCULATION.

1. Making AC the radius, the required sides are found by these propositions, as in plate 4, case 1.

R:AC::S.A:BC. R:AC::S.C:AB.

That is, as radius,	=90°	10.000000
is to AC	$=250_{\circ}$	2.397940
is to AC So is the sine	of $A=46^{\circ}$. $30'$	9.860562
to BC,	=181. 4	2.258502
As radius,	· =90°	10.000000
is to AC ,	$\cdot = 250$.	2.39794Q
So is the sine	of $C=43^{\circ}$. 30'	9.837812
to AB,	=172. 1	2.235752

If from the sum of the second and third logs. that of the first be taken, the number will be the log. of the fourth; the number answering to which will be the thing required; but when the first log. is radius, or 10.000000, reject the first figure of the sum of the other two logs. (which is the same thing as to subtract 10.000000;) and that will be the log. of the thing required.

2. Making AB the radius.

Secant A:AC::R:AB. Secant A:AC::T.A:BC.

That is, As the secant	of.	$A=46^{\circ}\ 30'$	10.162188
is to AC,		=250	2.397940
So is the radius		≕90°	10.000000
	•		12.397940
to AB,	, P	=172. 1	2.235762

As the secant of A is to AC, So is the tangent of A	$=46^{\circ} 30'$ $=250$ $=46^{\circ} 30'$	10.162188 2.397940 10.022750
		12.420690
to <i>BC</i> ,	=181.34.	2.258502

3. Making BC the radius.

Sec. C: AC:: Sec. C: AC:: That is, as the secant of is to AC, So is radius	T.C: AB.	10.139438 2.397940 10.0000 0 0
		12.397940
to BC ,	= 181.34	2.258502
As the secant of C	$=43^{\circ}\ 30'$	10.139438
is to AC ,	= 250	2.397940
So is the tangent of C	$=43^{\circ} \ 30'$	9.977250
•		12.375190
to AR	• 179 1	9 935759

Or, having found one side, the other may be obtained by cor. 2. theo. 14. sect. 4.

3d. By Gunter's scale.

The first and third terms in the foregoing proportions, being of a like nature, and those of the second and fourth being also like to each other; and the proportions being direct ones, it follows; that if the third term be greater or less than the first, the fourth term will be also greater or less

than the second; therefore the extent in your compasses, from the first to the third term, will reach from the second to the fourth.

Thus, to extend the first of the foregoing proportions;

- 1. Extend from 90° to 46° 30′, on the line of sines; that distance will reach from 250 on the line of numbers, to 181, for BC.
- 2. Extend from 90° to 43° 30′, on the line of sines; that distance will reach from 250 on the line of numbers, to 172, for AB.

If the first extent be from a greater to a less number; when you apply one point of the compasses to the second term, the other must be turned to a less; and the contrary.

By def. 20. sect. 4. The sine of 90° is equal to the radius; and the tangent of 45° is also equal to the radius; because if one angle of a right angled triangle be 45°, the other will be also 45°; and thence (by the lemma preceding theo. 7. sect. 4.) the tangent of 45° is equal to the radius: for this reason the line of numbers of 10.0000000, the sine of 90°, and tangent of 45° being all equal, terminate at the same end of the scale.

The two first statings of this case, answers the question without a secant: the like will be also made evident in all the following cases.

4th. Solution by Natural Sines.

From the foregoing analogies, or statements, it

is obvious that if the hypothenuse be multiplied by the natural sine of either of the acute angles, the product will be the length of the side opposite to that angle; and multiplied by the natural cosine of the same angle, the product will be the length of the other side, or that which is contiguous to the angle. Thus:

Nat. Sine = .725374 Hyp. = 250	Nat. Cos. = .688355 250
36268700	34417750

36268700 344177 1450748 1376710

Perpend.=181.343500

Base = 172.088750

CASE II.

The base and angles given; to find the perpendicular and kypothenuse.

PL. 5. fig. 5.

In the triangle ABC there is the angle A 42° 20′, and of course the angle C 47° 40′ (by cor. 2. theo. 5,) and the side AB 190, given; to find BC and AC.

1st. By Construction.

Make the angle CAB (by prob. 16. sect. 4.) in blank lines, as before. From a scale of equal parts lay 190 from A to B: on the point B, erect a perpendicular BC (by prob. 5. sect. 4.) the point where this cuts the other blank line of the angle, will be C: so is the triangle ABC constructed; let AC and BC be measured from the same scale of equal parts that AB was taken from, and the answers are found.

2d. By Calculation.

1. Making AC the radius.

S.C:AB::R:AC.S.C:AB::S.A:BC.

That is, as the sine of C $=47^{\circ} 40'$ 9.868785 is to AB, 2.278754 190 So is radius **90°** 10.000000 12.278754 257 2.409969 As the sine of C $=47^{\circ} 40'$ 9.868785 is to AB, 2.278754 190 So is the sine of $A = 42^{\circ} 20'$ 9.828301 12.107055

to BC, =173.12.238270

2. Making AB the radius.

R:AB::T.A:BC.R:AB:: Sec. A:AC.

90 That is, as radius 10.000000 is to AB, 2.278754 So is the tangent of $A=42^{\circ} 20'$ 9.959516 to BC, =173.12.238270 As radius =9010.000000 is to AB, 2.278754 =190So is the secant of $A=42^{\circ}$ 20' 10.131215 to AC, 2.409969 257

3. Making BC the radius.

T. C : AB :: Sec. C : AC.T.C:AB::R:BC.That is, as the tangent of $C=47^{\circ}$ 40' 10.040484 is to AB, **2.278754** So is the Secant of $C=47^{\circ}$ 40' 10.171699 12.450453 to AC, =2572.409969 As the tangent of $C=17^{\circ}$ 40 10.040484 is to AB, = 190**2.278754** So is the radius =90° 10.000000 12.278754 to BC = 173.12.238270

Or, having found one of the required sides, the other may be obtained, by one, or the other of the cors. to theo. 14. sect. 4.

3d. By Gunter's Scale:

1. When AC is made the radius.

Extend from 47° 40′, to 90° on the line of sines; that distance will reach from 190 to 257, on the line of numbers, for AC.

2. When AB is made the radius, the first stating is thus performed:

Extend from 45° on the tangents (for the tangent of 45° is equal to the radius, or to the sine of 90° as before) to $42^{\circ} 20'$; that extent will reach from 190, on the line of numbers, to 173, for BC.

3. When BC is made the radius, the second stating is thus performed:

Extend from 47° 40′ on the line of tangents, to 45° , or radius; that extent will reach from 190 to 173, on the line of numbers, for BC; for the tangent of 47° 40′, is more than the radius, therefore the fourth number must be less than the second, as before.

The two first statings of this case, answer the question without a secant.

4th. Solution by Natural Sines.

 $AB \times R$. $AB \times S \text{ of } A$ S of C. S of C. Nat. S of C, side $AB \times R$. Thus .739239) 190.000000 (257.02 & c.= AC. 147.8478

> 5190250 5174673

3696195

1557700 1478478

and, .673443=Nat. S. of A. 190=side AB.

60609870

Nat. S. of C. 673443

.739239) 127.954170 (173.09=BC. 739239

5403027 5174673

> 2283540 2217717

> > 6502300 6653151

CASE III.

The angle's and perpendicular given; to find the base and hypothenuse.

PL. 5. fig. 6.

In the triangle ABC, there is the angle A 40°, and consequently the angle C 50°, with BC 170, given: to find AC and AB.

1st. By Construction.

Make an angle CAB of 40° in blank lines; (by prob. 16. sect. 4.) with BC 170, from a line of equal parts draw the lines EF parallel to AB (by prob. 8. sect. 4.) the lower line of the angle, and from the point where it cuts the other line in C, let fall a perpendicular BC (by prob. 7. sect 4.) and the triangle is constructed: the measures of AC and AB, from the same scale that BC was taken, will answer the question.

What has been said in the two foregoing cases, is sufficient to render the operations in this, both by calculation, Gunter's scale, and Natural sines, so obvious, that it is needless to insert them; however, for the sake of the learner, we give for

Answers; AC 264. 5, and AB 202. 6.

CASE IV.

The base and hypothenuse given; to find the angles and perpendicular.

PL. 5. fig. 7.

In the triangle ABC, there is given, AB 300 and AC 500: the angles A and C, and the perpendicular BC, are required.

1st. By Construction.

From a scale of equal parts lay 300 from A to B; on B erect an indefinite blank perpendicular line, with AC 500, from the same scale, and one foot of the compass, in A, cross the perpendicular line in C; and the triangle is constructed.

By prob. 17. sect. 4. measure the angle A, and let BC be measured from the same scale of equal parts that AC and AB were taken from; and the answers are obtained.

2d. By Calculation.

1. Making AC the radius.

 $egin{array}{ll} AC:R::AB:S.C.\ R:AC::S.A.:BC.\ Q. \end{array}$

That is, as AC		500	2.698970
is to radius,	223	90°	10.000000
So is AB	==	300	2.477121
			12.477121
to the sin	e of C,	=36° 52′	9.778151
By cor. 2. theo. angle A .	5. 90%-	-36° 52′ =	= 53°08′ the
\mathbf{A}_{s} radius $=$	90°		10.000000
is to AC , =			2.698970
So is the sine of A			9.903108
to BC			

2. Making AB the radius.

AB : R : : AC : sec. A.R : AB : : T.A : BC.

That is, as AB	==	300	2477121
is to radius		90°	10.000000
So is AC	=	500	2.698970
			12.698970
to the secar	nt of A,	=53°. 08′	10.221849
As radius	*	90°	10.000000
is to AB ,	===	300	2.477121
So is the tange	nt of A	$=53^{\circ}.08'$	10.124990
to BC ,	=	400	2.602111

Or BC may be found from cor. 2. theo. 14. sect. 4.

3d. By Gunter's Scale.

1. Making AC the radius.

Extend from 500 to 300, on the line of numbers; that extent will reach from 90°, on the line of sines, to 36°. 52' for the angle C.

Again, extend from 90° to 53°. 08′, on the line of sines, that extent will reach from 500 to 400, on the line of numbers, for BC.

2. Making AC the radius, the second stating is thus performed.

Extend from radius, or the tangent of 45°, to 53°. 08', that extent will reach from 300 to 400, for BC.

4th. Solution by Natural Sines.

$$R \times AB$$
. $AC \times S \text{ of } A$.
 $AC = S \text{ of } C$; and $R = BC$.
 $AC = R$
Thus, $AC = AB$
 $5,00) 300.0000,00$
 $600000 = \text{Nat. sine } 36^{\circ} 52'$

and.

Nat. sine of
$$A = 53^{\circ} 8' = .800034$$

 $AC = 500$
 $400.017000 = BC$

1

CASE F.

The perpendicular and hypothenuse given, to find the angles and base.

PL. 5. fig. 8.

In the triangle ABC there is BC 306, and AC 370 given; to find the angles A and C; and the base AB.

1st. By Construction.

Draw a blank line from any point, in which, at B, erect a perpendicular, on which lay BC 306, from a scale of equal parts: from the same scale, with AC 370, in the compasses, cross the first drawn blank line in A, and the triangle ABC is constructed.

Measure the angle A (by prob. 17. sect. 4.); and also AB, from the same scale of equal parts the other sides were taken from, and the answers are now found.

The operations by calculation, the square root, Gunter's scale, and Natural sines, are here omitted, as they have been heretofore fully explained: the statings, or proportions, must also be obvious, from what has already been said.

Answers; The angle A 55° 48'; therefore the angle C 34° 12', and AB 208.

CASE VI.

The base and perpendicular given; to find the angles and hypothenuse.

PL. 5. fig. 9.

In the triangle ABC, there is AB 225, and BC 272, given; to find the angles A and C, and the hypothenuse AC.

1st. By Construction,

Draw a blank line, on which lay AB 225, from a scale of equal parts; at B, erect a perpendicular; on which lay BC, 272, from the same scale: join A and C, and the triangle is constructed.

As before, let the angle \tilde{A} , and the hypothenuse AC be measured; in order to find the answers.

2d. By Calculation.

1. Making AB the radius.

AB:R::BC:T.A. $R::AB::\sec A:AC.$

2. Making BC the radius.

BC:R::AB:T.C. $R.:BC::Sec.\ C:AC.$

By calculation; the answers from the foregoing proportions are easily obtained, as before.

But because AC, by either of the said proportions is found by means of a secant; and since there is no line of secants on Gunter's scale; after

having found the angles as before, let us suppose AC the radius, and then

1. S.
$$A : BC :: R :: AC$$
. or 2. S. $C : AB :: R :: AC$.

These proportions may be easily resolved, either by calculation, or Gunter's scale, as before; and thus the hypothenuse AC may be found without a secant.

From the two given sides, the hypothenuse may be easily obtained, from cor. 1. theo. 14. sect. 4.

Thus the square of
$$AB = 50625$$

Add the square of $BC = 73984$

$$\begin{array}{r}
 124609 (353 = AC) \\
 9 \\
 \hline
 65)346 \\
 325 \\
 \hline
 703)2109 \\
 2109 \\
 \end{array}$$

From what has been said on logarithms, it is plain,

1. That half the logarithm of the sum of the squares of the two sides, will be the logarithm of the hypothenuse. Thus,

The sum of squares, as before, is 124609; its log. is 5.095549, the half of which is 2.547774.;

and the corresponding number to this, in the ta-

bles, will be 353, for AC.

2. And that half of the logarithm of the difference of the squares of AC and AB, or of AC and BC, will be the logarithm of BC, or of AB.

The following examples are inserted for the ex-

ercise of the learner.

1. Given,
$$\left\{\begin{array}{c} \text{the angle } C \ 64^{\circ} \ 40' \\ AC \ 3876 \end{array}\right\} \left\{\begin{array}{c} AB \\ BC \end{array}\right\}$$
 required.

2. Given, $\left\{\begin{array}{c} \text{the angle } C \ 47^{\circ} \ 20' \\ AB \ 17 \end{array}\right\} \left\{\begin{array}{c} AC \\ BC \end{array}\right\}$ required.

3. Given, $\left\{\begin{array}{c} \text{the angle } C \ 28^{\circ} \ 30' \\ BC \ 27187 \end{array}\right\} \left\{\begin{array}{c} AB \\ AC \end{array}\right\}$ required.

4. Given, $\left\{\begin{array}{c} AB \ 2 \\ AC \ 3 \end{array}\right\} \left\{\begin{array}{c} \text{the angles required.} \\ \text{and } BC \end{array}\right\}$ required.

5. Given, $\left\{\begin{array}{c} BC \ 17 \\ AC \ 21.6 \end{array}\right\} \left\{\begin{array}{c} \text{the angles nequired.} \\ \text{and } AB \end{array}\right\}$ required.

6. Given, $\left\{\begin{array}{c} AB \ 2871.64 \\ BC \ 3176.2 \end{array}\right\} \left\{\begin{array}{c} \text{the angles required.} \\ \text{and } AC \end{array}\right\}$ required.

The answers are omitted, that the learner may esolve them for himself by the foregoing methods; by which means he will find and see more distinctly their mutual agreements: and become more expert, and better acquainted with the subject.

OBLIQUE ANGLED

PLANE TRIGONOMETRY.

BEFORE we proceed to the solution of the four cases of Oblique angled triangles, it is necessary to premise the following theorems.

THEO. I.

PL. 5. fig. 10.

In any plane triangle ABC, the sides are proportional to the sines of their opposite angles; that is, S. C: AB:: S. A: BC, and S. C: AB:: S. B: AC; also S. B: AC:: S. A: BC.

By theo. 10. sect. 4. the half of each side is the sine of its opposite angle; but the sines of those angles, in tabular parts, are proportional to the sines of the same in any other measure; and therefore the sines of the angles will be as the halves of their opposite sides; and since the halves are as the wholes, it follows, that the sines of their angles are as their opposite sides; that is, S. C: AB: S. A: BC, &c. Q. E. D.

THEO. II.

Fig. 11.

In any plane triangle ABC, the sum of the two given sides AB and BC, including a given angle ABC, is to their difference, as the sangent of half the sum of the two unknown angles A and C is to the tangent of half their difference.

Produce AB, and make HB=BC, and join HC: let fall the perpendicular BE, and that will bisect

the angle HBC (by theo. 9. sect. 4.) through B draw BD parallel to AC, and make HF = DC, and join BF; take BI = BA, and draw IG parallel to BD or AC.

It is then plain that AH will be the sum, and HI the difference of the sides AB and BC: and since HB=BC, and BE perpendicular to HC, therefore HE = EC (by theo. 8. sect. 4.); and since BA=BI, and BD and IG parallel to AC, therefore GD = DC = FH, and consequently HG = FD, and $\frac{1}{2}HG = \frac{1}{2}FD$ or ED. Again, EBC being half HBC, will be also half the sum of the angles A and C (by theo. 4. sect. 4.) also, since HB, HF, and the included angle H, are severally equal to BC, CD, and the included angle BCD: therefore (by theo. 6. sect. 4.) HBF = DBC = BCA (by part 2. theo. 3. sect. 4.) and since HBD=A (by part. 3. theo. 3. sect. 4.) and HBF=BCA: therefore BFDis the difference, and EBD, half the difference of the angles A and C: then making BE the radius, it is plain, that EC will be the tangent of half the sum, and ED the tangent of half the difference of the two unknown angles A and C: now IG being parallel to AC; AH: IH: CH: GH. (by cor. 1. theo. 20. sect. 4.) But the wholes are as their halves, that is, AH: IH: CE: ED, that is as the sum of the two sides AB and BC, is to their difference; so is the tangent of half the sum of the two unknown angles A and C, to the tangent of half their difference. Q. E. D.

THEO. III.

Fig. 12.

In any right lined plane triangle ABD; the base AD will be to the sum of the other sides, AB, BD, as the difference of those sides is to the difference of the segments of the base, made by the perpendicular BE; viz. the difference between AE and ED.

Produce BD, till BG=AB the lesser leg; and on B as a centre, with the distance BG or BA, describe a circle AGHF; which will cut BD, and AD in the points H and F; then it is plain, that GD will be the sum, and HD the difference of the sides AB and BD; also since AE=EF (by theo. 8. sect. 4.) therefore, FD is the difference of AE ED, the segments of the base; but (by theo. 17. sect. 4.) AD: GD: HD: FD; that is, the base is to the sum of the other sides, as the difference of those sides is to the difference of the segments of the base. Q. E. D.

THEO. IV.

Fig. 13.

If to half the sum of two quantities, be added half their difference; the sum will be the greatest of them; and if from half the sum be subtracted half their difference; the remainder will be the least of them.

Let the two quantities be represented by AB and BC: (making one continued line;) whereof AB is the greatest, and BC the least; bisect the whole line AC in E; and make AD = BC; then

it is plain, that AC is the sum, and DB the difference of the two quantities; and AE or EC, their half sum, and DE or EB their half difference. Now if to AE we add EB, we shall have AB the greatest quantity; and if from EC we take EB, we shall have BC the least quantity. Q.E.D.

Cor. Hence, if from the greatest of two quantities, we take half the difference of them, the remainder will be half their sum; or if to half their difference be added the least quantity, their sum will be half the sum of the two quantities.

OBLIQUE ANGLED TRIANGLES.

CASE I.

TWO sides, and an angle opposite to one of them given; to find the other angles and side.

PL. 5. fig. 11.

In the triangle ABC, there is given AB 240, the angle A 46° 30, and BC 200; to find the angle C, being acute, the angle B, and the side AC.

1st. By Construction.

Draw a blank line, on which set AB 240, from a scale of equal parts; at the point A, of the line AB, make an angle of 46° 30, by an indefinite blank line; with BC 200, from a like scale of equal parts that AB was taken, and one foot in B, describe the arc DC to cut the last blank line in the points D and C. Now if the angle C had been required obtuse, lines from D to B, and to A, would constitute the triangle; but as it is required acute,

draw the lines from C to B and to A, and the triangle ABC is constructed. From a line of chords let the angles B and C be measured; and AC from the same scale of equal parts that AB and BC were taken; and you will have the answers required.

2d. By Calculation.

This is performed by theo. 1. of this sect. thus;

As $BC = $ is to the sine of $A = $ So is $AB = $	200 46°. 30′ 240	2.301030 9.860562 2.380211
to the sine of C , =	60°. 31′	12.240773 9.939743

180°—the sum of the angles A and C, will give the angle B, by cor. 1. theo. 5. sect. 4.

A 46°. 30′ C 60. 31

180°—107°. As the sine is to <i>BC</i> , So is the sin	of A =	= 46°. 30′ 200	9.860562 2.301030 9.980555
		•	12.281585
to AC,	===	263 , 7	2.421023

3d. By Gunter's Scale.

Extend from 200 to 240, on the line of numbers; that distance will reach from 46° 30' on the line of sines, to 60° 31' for the angle C_n

Extend from 46° 30′, to 72° 59′, on the line of sines; that distance will reach from 200 to 263.7 on the line of numbers, for AC.

Note. The method by Natural Sines will be obvious from the foregoing analogies.

CASE II.

Two angles and a side given; to find the other sides.

PL. 5. fig. 15.

In the triangle ABC, there is the angle A 46° 30' AB 230; and the angle B 37° 30', given to find AC and BC.

1st. By Construction.

Draw a blank line, upon which set AB 230, from a scale of equal parts; at the point A of the line AB, make an angle of 46° 30′, by a blank line; and at the point B of the line AB make an angle of 37° 30′, by another blank line: the intersection of those lines gives the point C, then the triangle ABC is constructed. Measure AC and BC from the same scale of equal parts that AB was taken; and you have the answer required.

2d. By Calculation.

By (cor. 1. theo. 5. sect. 4.) 180°—the sum of the angles A and B=C.

A 46° 30′

B 37. 30

 $180^{\circ} - 84^{\circ}$. $00' = 96^{\circ}$ 00' = C.

By def. 27. sect. 4. The sine of 96°=the sine of 84°, which is the supplement thereof; therefore instead of the sine of 96°, look in the tables for the sine of 84°.

By theo. 1. of this sect.

As the sine of C	= 96° 00′	. 9.997614
is to AB ,	= 230	2.361728
So is the sine of A	$= 46^{\circ} 30'$	9.860562
	•	12.222290
to BC , =	167.8	2.224676
As the sine of C	96° 00'	9.997614
is to AB ,	= 230	2.361728
So is the sine of B		9.784447
	•	12.146175
to AC , =	140.8	2.148561

3d. By Gunter's Scale.

Extend from 84° (which is the supplement of 96°) to 46° 30′ on the sines; that distance will reach from 230 to 168, on the line of numbers, for BC.

Extend from 84° to 37°. 30′, on the sines; that extent will reach from 230 to 141, on the line of numbers, for AC.

CASE III.

Two sides and a contained angle given; to find the other angles and side.

PL. 5. fig. 16.

In the triangle ABC, there is AB 240, the angle A 36° 40' and AC 180, given; to find the angles C and B, and the side BC.

1st. By Construction.

Draw a blank line, on which from a scale of equal parts, lay AB 240; at the point A of the line AB, make an angle of 36° 40′, by a blank line; on which from A, lay AC 180, from the same scale of equal parts; measure the angles C and B, and the side BC, as before; and you have the answers required.

2d. By Calculation.

By cor. 1. theo. 5. sect. 4. 180° —the angle A 36° . $40' = 143^{\circ}$. 20' the sum of the angles C and B: therefore half of 143° . 20', will be half the sum of the two required angles, C and B.

By theo. 2. of this sect.

As the sum of the two sides AB and AC = 420 is to their difference, = 60

So is the tangent of half the sum of the two unknown angles C and B = 71° 40° to the tangent of half their difference = 23° 20°

By theo. 4.

To half the sum of the angles C and $B=71^{\circ}40'$. Add half their difference as now found = 23 20.

The sum is the greatest angle, or ang. C=9500

Subtract, and you have the least angle, or B=4820

The angle C and B being found; BC is had, as before, by theo. 1. of this sect. Thus,

S. B : AC :: S : A : BC. 48° 20′: 180 :: 36° 40 : 143. 9.

3d. By Gunter's Scalo.

Because the two first terms are of the same kind, extend from 420 to 60 on the line of numbers; lay that extent from 45° on the line of tangents, and keeping the left leg of your compasses fixed, move the right leg to 71°. 40′; that distance laid from 45° on the same line will reach to 23°. 30′, the half difference of the required angles. Whence the angles are obtained, as before.

The second proportion may be easily extended, from what has been already said.

CASE IV.

PL. 5. fig. 17.

The three sides given, to find the angles.

In the triangle ABC, there is given, AB 64, AC 47, BC 34; the angles A, B, C, are required.

1st. By Construction.

The construction of this triangle must be manifest, from prob. 1. sect. 4.

2d. By Calculation.

From the point C, let fall the perpendicular CD on the base AB; and it will divide the triangle into two right angled ones, ADC and CBD; as well as the base AB, into the two segments, AD and DB.

AC 47 BC 34

Sum 81

Difference 13

By theo. 3. of this sect.

As the base or the longest side, AB	64
is to the sum of the other sides, ACa	nd BC, 81
So is the difference of those sides	13
to the difference of the segments of	16.46
the base $ADDB$.	

By theo. 4. of this sect.

To half the base, or to half the sum)	32
of the segments AD and DB .	<u> </u>
Add half their difference, now found,	8.23

Their sum will be the greatest segment AD 40.23

Subtract, and their difference will be the least segment DB, 23.77

In the right angled triangle ADC, there is AC47, and AD 40. 23, given, to find the angle A.

This is resolved by case 4. of right angled plane trigonometry, thus,

AD: R: :AC: Sec. A40. 23: 90°: :47: 31° 08′

Or it may be had by finding the angle ACD, the complement of the angle A; without a secant, thus,

AC: R:: AD: S. ACD. 47: 90°:: 40_23: 58° 52'

 $90 - 58^{\circ} 52' = 31^{\circ}$. 08', the angle A.

Then by theo. 1. of this sect.

BC: S. A: :AC: S. B. 34: 31° 08': :47: 45° 37.

By cor. 1. theo. 5. sect. 4. 180° —the sum of A and B=C.

A 31°. 08′ B 45. 37

180°-76. 45=103°. 15′, the angle C:

3d. By Gunter's Scale.

The first proportion is extended on the line of numbers; and it is no matter whether you extend from the first to the third, or to the second term, since they are all of the same kind: If you extend to the second, that distance applied to the third, will give the fourth; but if you extend from the first to the third, that extent will reach from the second to the fourth.

The methods of extending the other proportions have been already fully treated of.

An example in each case of oblique angled triangles.

1. Given,
$$\begin{cases} AC & 290 \\ C69 & 30' \\ AB & 350 \end{cases} \stackrel{A}{B}$$
 required.

2. Given, $\begin{cases} C & 24^{\circ} \cdot 20' \\ B & 128^{\circ} \cdot 30 \\ AC & 3246 \end{cases} \stackrel{AB}{BC}$ required.

3. Given, $\begin{cases} AC & 6 \\ C & 124^{\circ} \cdot 30' \\ BC & 4 \cdot 5 \end{cases} \stackrel{A}{B}$ required.

4. Given, $\begin{cases} AB & 46 \\ AC & 92 \\ BC & 52 \end{cases} \stackrel{A}{C}$ required.

Additional Exercises with their Answers.

QUESTIONS FOR EXERCISE.

1. Given the Hypothenuse 108 and the Angle opposite the Perpendicular 25° 36; required the Base and Perpendicular.

Answer. The Base is 97.4, and the Perpendi-

cular 46.66.

2. Given the Base 96 and its opposite Angle 71° 45'; required the Perpendicular and the Hypothenuse.

Answer. The Perpendicular is 31.66 and the Hypothenuse 101.1.

3. Given the Perpendicular 360 and its opposite Angle 58° 20'; required the Base and the Hypothenuse.

Answer. The Base is 222, and the Hypothenuse 423.

4. Given the Base 720 and the Hypothenuse 980; required the Angles and the Perpendicular.

Answer. The Angles are 47° 17'. and 42° 43', and the Perpendicular 664.8

5. Given the Perpendicular 110.3 and the Hypothenuse 176.5; required the Angles and the Base.

Answer. The Angles are 38°41' and 51°19', and the Base 137.8.

6. Given the Base 360 and the Perpendicular 480; required the Angles and the Hypothenuse.

Answer. The Angles are 53° 8′ and 36° 52′, and the Hypothenuse 600.

7. Given one Side 129, an adjacent Angle 56° 30, and the opposite Angle 81° 36': required the third Angle and the remaining Sides.

Answer. The third Angle is 41° 54', and the

remaining Sides are 108.7 and 87.08.

8. Given one Side 96.5, another Side 59.7, and the Angle opposite the latter Side 31° 30′: required the remaining Angles and the third Side.

Answer. This Question is ambiguous; the given Side opposite the given Angle being less than the other given Side (see Rule I.;) hence, if the Angle opposite the Side 96.5 be acute, it will be 57° 38′, the remaining Angle 90° 52′, and the third Side 114.2; but if the Angle opposite the Side 96.5 be obtuse, it will be 122° 22′, the remaining Angle 26° 8′, and the third Side 50.32.

9. Given one Side 110, another Side 102, and the contained Angle 113° 36: required the remaining Angles and the third Side.

Answer. The remaining Angles are 34° 37' and

31° 47', and the third Side is 177.5.

10. Given the three Sides respectively, 120.6, 125.5, and 146.7: required the Angles.

Answer. The Angles are 51° 53', 54° 58', and

73° 9′. ...

The student, who has advanced thus far in this work with diligence and active curiosity, is now prepared to study, with ease and pleasure, the following part; which comprehends all the necessary directions for the practice of Surveying.

PART II,

Or the Practical Surveyor's Guide.

SECT. I.

Containing a particular Description of the several Instruments used in Surveying, with their respective Uses.

THE CHAIN,

THE stationary distance, or merings of ground, are measured either by Gunter's chain of four poles or perches, which consists of 100 links; (and this is the most natural division) or by one of 50 links, which contains two poles or perches: but because the length of a perch differs in many places, therefore the length of chains and their respective links will differ also.

The English statute-perch is 5½ yards, the two-pole chain is 11 yards, and the four-pole one is 22 yards; hence the length of a link in a statute-chain is 7.92 inches.

There are other perches used in different parts of England, as the perch of woodland measure, which is 6 yards; that of church-land measure, which is 7 yards, and the forest measure perch, which is 8 yards.

For the more ready reckoning the links of a four-pole chain, there is a large ring, or sometimes a round piece of brass, fixed at every 10 links; and at 50 links, or in the middle, there are two large rings. In such chains as have a brass piece at every 10 links, there is the figure 1 on the first piece, 2 on the second, 3 on third, &c. to 9. leading therefore that end of the chain forward which has the least number next to it, he who carries the hinder end may easily determine any number of links: thus, if he has the brass piece number 8, next to him, and six links more in a distance, that distance is 86 links. After the same manner 10 may be counted for every large ring of a chain which has not brass pieces on it; and the number of links is thus readily determined.

The two-pole chain has a large ring at every 10 links, and in its middle, or at 25 links, there are 2 large rings; so that any number of links may be the more readily counted off, as before.

The surveyer should be careful to have his chain measured before he proceeds on business, for the rings are apt to open by frequently using it, and its length is thereby increased, so that no one can be too circumspect in this point,

In measuring a stationary distance, there is an object fixed in the extreme point of the line to be measured; this is a direction for the hinder chainman to govern the foremost one by, in order that the distance may be measured in a right line; for if the hinder chainman causes the other to cover the object, it is plain the foremost is then in a right line towards it. For this reason it is necessary to have a person that can be relied on, at the hinder

end of the chain, in order to keep the foremost man in a right line; and a surveyor who has no such person, should chain himself. The inaccuracies of most surveys arise from bad chaining, that is, from straying out of the right line, as well as from other omissions of the hinder chainman: no person, therefore, should be admitted at the hinder end of the chain, of whose abilities in this respect, the surveyor was not previously convinced; since the success of the survey, in a grest measure, depends on his care and skill.

In setting out to measure any stationary distance, the foreman of the chain carries with him 10 iron pegs pointed, each about ten inches long; and when he has stretched the chain to its full length, he at the extremity thereof sticks one of those pegs perpendicularly in the ground; and leaving it there, he draws on the chain till the hinder man checks him when he arrives at that peg: the chainbeing again stretched, the fore man sticks down another peg, and the hind man takes up the former; and thus they proceed at every chain's length contained in the line to be measured, counting the surplus links contained between the last peg, and the object at the termination of the line, as before: so that, the number of pegs taken up by the hinder chainman, expresses the number of chains; to which, if the odd links be annexed, the distance line required in chains and links is obtained, which must be registered in the field book, as will hereafter be shewn.

If the distance exceeds 10, 20, 30, &c. chains, when the leader's pegs are all exhausted, the hinder chainman, at the extremity of the 10 chains, delivers him all the pegs; from whence they pro-

ceed to measure as before, till the leader's pegs are again exhausted, and the hinder chainman at the extremity of these 10 chains again delivers him the pegs; from whence they proceed to measure the whole distance line in the like manner; then it is plain, that the number of pegs the hinder chainman has, being added to 10, if he had delivered all the pegs once to the leader, or to 20 if twice, or to 30 if thrice, &c. will give the number of chains in that distance; to which if the surplus links be added, the length of the stationary distance is known in chains and links.

It is customary, and indeed necessary, to have red, or other coloured cloth, fixed to the top of each peg, that the hinder man at the chain may the more readily find them; otherwise, in chaining through corn, high grass, briars, rushes, & c. it would be extremely difficult to find the pegs which the leader puts down: by this means no time is lost, which otherwise must be, if no cloths are fixed to the pegs, as before.

It will be necessary here to observe, that all slant, or inclined surfaces, as sides of hills, are measured horizontally, and not on the plane or surface of the hill, and is thus effected.

PL. 8, Ag. 4.

Let ABC be a hill, the hindmost chainman is to hold the end of the chain perpendicularly over the point A (which he can'the better effect with a plummet and line, than by letting a stone drop, which is most usual) as d is over A, while the leader puts down his peg at e: the eye can direct the horizontal position near enough, but if greater accuracy

were required, a quadrant applied to the chain, would settle that. In the same manner the rest may be chained up and down; but in going down, it is plain the leader of the chain must hold up the end thereof, and the plummet thence suspended, will mark the point where he is to stick his peg. The figure is sufficient to render the whole evident; and to shew that the sum of the chains will be the horizontal measure of the base of the hill; for de=Ao, fg=op, hi=pq, &c. therefore $de\times fg\times hi$, &c.= $Ao\times op\times pq$, &c.=AC, the base of the hill. If a whole chain cannot be carried horizontally, half a chain, or less, may, and the sum of these half chains, or links, will give the base, as before.

If the inclined side of the hill be the plane surface, the angle of the hill's inclination may be taken, and the slant height may be measured on the surface; and thence (by case 1. of right-angled trigonometry) the horizontal line answering to the top, may be found; and if we have the angle of inclination given on the other side, with those already given; we can find the horizontal distance across the hill, by case 2. of oblique trigonometry.

All inclined surfaces are considered as horizontal ones; for all trees which grow upon any inclined surface, do not grow perpendicular thereto, but to the plane of the horizon: thus if Ad, ef, gh, &c. were trees on the side of a hill, they grow perpendicular to the horizontal base AC, and not to the surface AB: hence the base will be capable to contain as many trees as are on the surface of the hill, which is manifest from the continuation of them thereto. And this is the reason that the area of the base of a hill, is considered to be equal in value to the hill itself.

Besides, the irregularities of the surfaces of hills in general are such, that they would be found impossible to be determined by the most able mathematicians. Certain regular curve surfaces have been investigated with no small pains, by the most eminent; therefore an attempt to determine in general the infinity of irregular surfaces which offer themselves to our view, to any degree of certainty, would be idle and ridiculous, and for this reason also, the horizontal area is only attempted.

Again, if the circumjacent lands of a hill be planned or mapped, it is evident we shall have a plan of the hill's base in the middle: but were it possible to put the hill's surface in lieu thereof, it would extend itself into the circumjacent lands, and render the whole an heap of confusion: so that if the surfaces of hills could be determined, no more than the base could be mapped

Roads are usually measured by a wheel for that purpose, called the Perambulator, to which there is fixed a machine, at the end whereof there is a spring, which is struck by a peg in the wheel, once in every rotation; by this means the number of rotations is known; if such a wheel were 3 feet 4 inches in diameter, one rotation would be 104 feet, which is half a plantation perch; and because 320 perches make a mile, therefore 640 rotations will be a mile also; and the machinery is so contrived, that by means of a hand, which is carried round by the work, it points out the miles, quarters, and perches, or sometimes the miles, furlongs, and perches.

Or roads may be measured by a chain more accurately; for 80 four-pole, 160 two-pole chains, or 320 perches, make a mile as before: and if roads

are measured by a statute-chain, it will give you the miles English, but if by a plantation chain, the miles will be Irish. Hence an English mile contains 1760, and an Irish mile 2240 yards; and because 14 half yards is an Irish, and 11 half yards is an English perch, therefore 11 Irish perches, of Irish miles, are equal to 14 English ones.

Since some surveys are taken by a four-pole, and others by a two-pole chair; and as ground for houses is measured by feet, we will shew how to reduce one to the other, in the following problems.

PROB. I.

To reduce two-hole chains and links to four-hole once.

If the number of chains be even, the half of them will be the four-pole ones, to which annex the given links, thus,

Ch. L.

1. In 16. 37 of two pole chains, how many fourpole ones?

Ch. L. Answer 8, 37.

But if the number of chains be odd, take the half of them for chains, and add 50 to the links, and they will be four-pole chains and links, thus,

Ch. L.
2. In 17. 42 of two-pole chains, how many four-pole ones?

Ch. L, Answer 8. 92,

PROB. IL.

To reduce four-pole chains and links, to two-pole ones:

Double the chains, to which annex the links, if they be less than 50; but if they exceed 50, double the chains, add one to them, and take 50 from the links, and the remainder will be the links, thus,

Ch. E.

1. In 8. 37 of four-pole chains, how many

2. two-pole ones?

16. 37

Ch. L.

2. In 8. 82 of four-pole chains, how many
2. 50 two-pole ones?

17. 32 Answer,

PROB. III.

To reduce four-pole chains and links, to perches and decimals of a perch.

The links of a four-pole chain are decimal parts of it, each link before the hundreth part of a chain; therefore if the chain and links be multiplied by 4, (for 4 perches are a chain) the product will be the perches and decimal parts of a perch. Thus,

Ch. L. How many perches in 13. 64 of four-pole chains,

Answer 54, 56 perches.

PROB. IV.

To reduce two-pole chains and links, to perches and decimals of a perch.

They may be reduced to four-pole ones (by prob. 1.) and thence to perches and decimals (by the last,) or,

If the links be multiplied by 4, carrying one to the chains, when the links are, or exceed 25; and the chains by 2, adding one, if occasion be; the product will be perches, and decimals of a perch. Thus,

Ch. L.

1. In 17. 21 of two-pole chains, how many 2. 4 perches.

Answer, 34. 84 perches.

Ch. L.

2. In 15. 38 of two-pole chains, how mnay2. 4 perches.

Answer, 31. 52 perches.

PROB. V.

To reduce perches, and decimals of a perch, to four-pole chains and links.

Divide by 4, so as to have two decimal places in the quotient, and that will be four-pole chains and links. Thus, In 31. 52 perches, how many four-pole chains and links?

Ch. L.
4)31.52(7. 88 Answer.

35

32

PROB. VI.

To reduce perches and decimals of a perch, to two-pole chains and links.

The perches may be reduced to four-pole chains (by the last) and from thence to two-pole chains (by prob. 2.) or,

Divide the whole number by 2, the quotient will be chains; to the remainder annex the given decimals, and divide by 4, the last quotient will be the links. Thus,

In 31.52 perches, how many two-pole chains and links?

Ch. L.
2)31.52(15. 38 Answer.

11
4)152(38
32

PROB. VII.

To reduce chains and links, to feet and decimal parts of a foot.

If they be two-pole chains, reduce them to four-pole ones: (by prob. 1.) these being multiplied by the feet in a four-pole chain, will give the feet and decimals of a foot. Thus,

Ch. L. In 17. 21 of two-pole chains, how many feet?

Ch. L.
8. 71 of four-pole chains.
66 feet = 1 chain.

5226. Feet Inches 5226 Answer 574. 101.

Feet 574.86 12 Inches 10.32 4 1.28

PROB. VIII.

To reduce feet and inches to chains and links.

Reduce the inches to the decimal of a foot, and annex that to the feet; that divided by the feet in a four-pole chain, will give the four-pole chains and

links in the quotient: these may be reduced to two-pole chains and links, if required, by prob. 2. Thus,

Feet. Inches.

In 217. 9 how many two-pole chains? 12)9.00.(75 the decimal of 9 inches. .

60

66)217.75(3. 29 of four-pole chains, or

How to take a Survey by the CHAIN only.

PROB. I.

To survey a piece of ground, by going round it, and the meathod of taking the angles of the field, by the chain only.

PL. 6. fig. 6.

Let ABCDEFG be a piece of ground to be surveyed: beginning at the point A, let one chain be laid in a direct line from A, towards G, where let a peg be left, as at c; and again, the like distance from A in a direct line towards B; where another peg is also to be left, as at d: let the distance from d to c be measured, and placed in the field-book, in

the second column under the denomination of angles, in a line with station No. 1; and in the same line, under the title of distances, in the third column, let the measure of the line AB in chains and links be inserted. Being now arrived at B, let one chain be laid in a direct line from B towards A, where let a peg be left, as at f, and again, the like distance from B in a direct line towards C, where let also another peg be left, as ate; the distance from e to f is to be inserted in the field-book in the second column, under angles, in a line with station No. 2; and in the same line, under the title of distances in the third column, let the measure of the line BC, in chains and links, be inserted: after the same manner we may proceed from C to D, and thence to E; but because the angle at E, vis. FED, is an external angle, after having laid one chain from E to h, and to g, the distance from g to h is measured, and inserted in the column of angles, in a line with station No. 5. and on the side of the field-book against that station, we make an asterisk, thus *, or any other mark, to signify that to be an external angle, or one measured out of the ground. Proceed we then as before, from E to F, to G, and thence to A, measuring the angles and distances, and placing them as before, in the field-book, opposite to their respective stations; so will the fieldbook be completed in manner following.

N. B. After this manner the angles for inaccessible distances may be taken, and the method of constructing or laying them down, as well as the construction of the map, from the following field-notes, must be obvious from the method of taking them.

The form of the field-book, with the title.

A field-book of part of the land of Grange, in the parish of Portmarnock, barony of Coolock, and county of Dublin; being part of the estate of L. P. Esq. let to C. D. farmer. Surveyed January 30, 1782.

Taken by a four-pole chain.

Remarks.	No. Sta.	Angles Ch. L.	Distan. Ch. L.	
Mr. J. D's part of Grange	1	1.80	17.65	
,	2	1.79	18.50	
Mr. L. P's part of Portmar-	3	1.76	28.00	
nock strand	4	1.413	20.00	
*	5	1.874	14.83	
Widow J. G's part of Grange	6	1.14	19.41	
	7	1.89	24.53	
•		Close at the first station.		

Explanation of the remarks.

Mr. J. D's part of Grange bounds, or is adjacent to the surveyed land from the first to the third station; Mr. L. P's part of Portmarnock bounds it from the third to the fourth station; the strand then is the boundary from thence to the sixth, and from the sixth to the first station, the widow J. G's part of Grange is the boundary.

It is absolutely necessary to insert the persons' names, and town-lands, strands, rivers, bogs, rivulets, &c. which bound or circumscribe the land which is surveyed, for these must be expressed in the map.

In a survey of a town-land, or estate, it is sufficient to mention only the circumjacent town-lands, without the occupiers' names: but when a part only of a town-land is surveyed, then it is necessary to insert the person or persons' names, who hold any particular parcel or parcels, of such townland, as bound the parts surveyed.

When an angle is very obtuse, as most in our present figure are, viz. the angles at A, B, C, E, and G: it will be best to lay a chain from the angular point, as at A, on each of the containing sides to c and to d; and any where nearly in the middle of the angle, as at e: measuring the distances ce and ed; and these may be placed for the angle in the field-book. Thus,

No. Sta. Angle. Ch. L. Ch. L.
$$1.03$$
 17.65

For when an angle is very obtuse, the chord line, as ed, will be nearly equal to the radii Ac and Ad; so if the arc ced be swept, and the chord line ed be laid on it, it will be difficult to determine exactly that point in the arc where ed cuts it: but if the angle be taken in two parts, as ce, the arc, and the angle thence, may be truly determined and constructed.

After the same manner any piece of ground may be surveyed by a two-pole chain.

PROB. II.

To take a survey of a piece of ground from any point within it, from whence all the angles can be seen; by the chain only.

PL. 6. fig. 6.

Let a mark be fixed at any point in the ground, as at H, from whence all the angles can be seen; let the measures of the lines HA, HB, HC, &c. be taken to every angle of the field from the point H; and let those be placed opposite to No. 1, 2, 3, 4, &c. in the second column of the radii: the measures of the respective lines of the mearing, vis. AB, BC, CD, DE, &c. being placed in the third column of distances, will complete the field-book. Thus,

Remarks.	No. Radii. Distan. Ch. L. Ch. L.
	1 20.00 17.65
	2 21.72 18.50 3 21.74 28.00
	4 25.34 20.00 5 17.20 14.83
	6 29.62 19.41
	7 21.20 24.53 Close at the first station.

If any line of the field be inaccessible, as suppose CD to be, then by way of proof that the distance CD is true, let the measure of the angle CHD be taken by the line oo, with the chain: if this angle corresponds with its containing sides, the length of the line DCD truly obtained, and the whole work is truly taken.

Note, That in setting off an angle, it is necessary to use the largest scale of equal parts, viz. that of the inch, which is diagonally divided into 100 parts, in order that the angle should be accurately laid down; or if two inches were thus divided for angles, it would be the more exact; for it is by no means necessary that the angles should be laid from the said scale with the stationary distances.

PROB. III.

To take a survey by the chain only, when all the angles cannot be seen from one point within.

PL. 6. fig. 7.

Let the ground to be surveyed be represented by 1, 2, 3, 4, &c. Since all the angles cannot be seen from one point, let us assume 3 points, as A, B, C, from whence they may be seen; at each of which let a mark be put, and the respective sides of the triangle be measured and set down in the field-book; let the distance from A to 1, and from B to 1, be measured, and these will determine the point 1; let the other lines which flow from A, B, C, as well as the circuit of the ground, be then measured as the figure directs; and thence the map may be easily constructed.

There are other methods which may be used; as dividing the ground into triangles, and measuring the 3 sides of each; or by measuring the base and perpendicular of each triangle. But this we shall speak of hereafter.

PROB. IV.

How to take any inaccessible distance by the chain only.

PL. 8. fig. 8.

Suppose AB to be the breadth of a river, or any other inaccessible distance, which may be required.

Let a staff or any other object be set at B, draw yourself backward to any convenient distance C, so that B may cover A: from B, lay off any other distance by the river's side to E, and complete the parallelogram EBCD: stand at D, and cause a mark to be set at F, in the direction of A; measure the distance in links from E to F, and FB will be also given. Wherefore EF:ED::FB:AB. Since it is plain (from part 1. theo. 3. sect. 4. and theo. 2. sect. 4.) the triangles EFDBFA are mutually equiangular.

If part of the chain be drawn from B to C, and the other part from B to E; and if the ends at E and C be kept fast, it will be easy to turn the chain over to D, so as to complete a parallelogram; by reckoning off the same number of links you had in BC, from E to D, and pulling each part straight.

THE

CIRCUMFERENTOR.

THIS instrument is composed of a brass circular box, about five or six inches in diameter; within which is a brass ring, divided on the top into 360 degrees, and numbered 10, 20, 30, &c. to 360: in the centre of the box is fixed a steel pin finely pointed, called a centre-pin, on which is placed a needle touched by a loadstone, which always retains the same situation; that is, it always points to the North and South points of the horizon nearly, when the instrument is horizontal, and the needle at rest.

The box is covered with a glass lid, in a brass rim, to prevent the needle being disturbed by wind or rain, at the time of surveying: there is also a brass lid or cover, which is laid over the former to preserve the glass in carrying the instrument.

This box is fixed by screws, to a brass index, or ruler, of about 14 or 15 inches in length, to the ends whereof are fixed brass sights, which are screwed to the index, and stand perpendicular thereto: in each sight is a large and a small aperture, or slit, one over the other; but these are changed, that is, if the large aperture be uppermost in the one sight, it will be lowest in the other, and

so of the small ones: therefore the small aperture in one is opposite to the large one in the other; in the middle of which last, there is placed a horse hair, or fine silk thread.

The instrument is then fixed on a ball and socket; by the help of which and a screw, you can readily fix it horizontally in any given direction; the socket being fixed on the head of a three-legged staff, whose legs, when extended, support the instrument whilst it is used.

To take field notes by the Circumferentor.

PL. 6. fig. 6.

Let your instrument be fixed at any angle as A, your first station; and let a person stand at the next angle B, or cause a staff, with a white sheet, to be set there perpendicularly for an object to take your view to: then having placed your instrument horizontally (which is easily done by turning the box so that the ends of the needle may be equidistant from its bottom, and it traverses or plays freely) turn the flower-de-luce, or north part of the box, to your eye, and looking through the small aperture, turn the index about, till you cut the person or object in the next angle B, with the horse hair, or thread of the opposite sight; the degrees then cut by the south end of the needle, will give the number to be placed in the second column of your field-book in a line with station No. 1, and expresses the number of degrees the stationary line is from the north, counting quite round with the sun.

Most needles are pointed at the south end, and have a small ring at the north: such needles are

better than those which are pointed at each end, because the surveyor cannot mistake by counting to a wrong end; which error may be frequently committed, in using a two-pointed needle.

Two-pointed needles have sometimes a ring, but more usually a cross towards the north end: and the south end is generally bearded towards its extremity, and sometimes not, but its arm is a naked right line from the cap at the centre.

Having taken the degrees or bearing of the first stationary line AB, let the line be measured, and the length thereof in chains and links be inserted in the third column of your field-book, under the title of distances, opposite to station No. 1.

It is customary, and even necessary, to cause a sod to be dug up at each station, or place where you fix the instrument: to the end, that if any error should arise in the field-book, it may be the more readily adjusted and corrected, by trying over the former bearings and stationary distances.

Having done with your first station, set the instrument over the hole or spot where your object stood, as at B, for your second station, and send him forward to the next angle of the field, as at C; and having placed the instrument in an horizontal direction, with the sights directed to the object at C, and the north of the box next your eye, count your degrees to the south end of the needle, which register in your field-book, in the second column opposite to station No. 2; then measure the stationary distance BC, which insert in the third column, and thus proceed from angle to angle, sending your object before you, till you

return to the place where you began, and you will have the field-book complete; observing always to signify the parties names who hold the contiguous lands, and the names of the town-lands, rivers, roads, swamps, lakes, &c. that bound the land you survey, as before; and this is the manner of taking field-notes by what is called foresights.

But the generality of mearsmen frequently set themselves in disadvantageous places, so as often to occasion two or more stations to be made, where one may do, which creates much trouble and loss of time; we will therefore shew how this may be remedied, by taking back-sights, thus: let your object stand at the point where you begin your survey, as at A; leaving him there, proceed to your next angle B, where fix your instrument so, that you may have the longest view possible towards C. Having set the instrument in an horizontal position, turn the south part of the box next your eye, and having cut your object at A, reckon the degrees to the south point of the needle, which will be the same as if they were taken from the object to the instrument, the direction of the index being the same. Let the degree be inserted in the fieldbook, and the stationary distance be measured and annexed thereto, in its proper column; and thus proceed from station to station, leaving your object in the last point you left, till you return to the first station A,

By this method your stations are laid out to the best advantage, and two men may do the business of three, for one of those who chain, may be your object; but in fore-sights, you must have an object before you, besides two chainmen.

It was said before, that a surveyor should have a person with him to carry the hinder end of the chain, on whom he can depend: this person should be expert and ready at taking off-sets, as well as exact in giving a faithful return of the length of every stationary line. One who has such a person, and who uses back-sights, will be able to go over near double the ground he could at the same time, by taking fore-sights, because of overseeing the chaining; for should he take back-sights, he must be obliged, after taking his degree, to go back to the foregoing station, to oversee the chaining, and by this means to walk three times over every line, which is a labour not to be borne.

Or a back and a fore-sight may be taken at one station, thus; with the south of the box to your eye, observe from B the object A, and set down the degree in your field-book, cut by the south end of the needle. Again from B observe an object at C, with the north of the box to your eye, and set down the degree cut by the south point of the needle, so have you the bearings of the lines AB and BC; you may then set up your instrument at D, from whence take a back-sight to C, and a fore-sight to E: thus the bearings may be taken quite round, and the stationary distances being annexed to them, will complete the field-book.

But in this last method, care must be taken to see that the sights have not the least cast on either side; if they have, it will destroy all: and yet with the same sights you may take a survey by fore-sights, or by back-sights only, with as great truth as if the sights were ever so erect, provided the same cast continues without any alteration; but, upon the whole, back-sights only will be found the readiest method.

If your needle be pointed at each end, in taking fore-sights, you may turn the north part of the box to your eye, and count your degrees to the south part of the needle, as before; or you may turn the south of the box to your eye, and count your degrees to the north end of the needle.

But in back-sights you may turn the north of the box to your eye, and count your degrees to the north point of the needle; or you may turn the south of the box to your eye, and count your degrees to the south end of the needle.

The brass ring in the box is divided on the side into 360 degrees, thus; from the north to the east into 90, from the north to the west into 90, from the south to the east into 90, and from the south to the west into 90 degrees; so the degrees are numbered from the north to the east or west, and from the south to the east or west.

The manner of using this part of the instrument is this; having directed your sights to the object, whether fore or back, as before, observe the two cardinal points of your compass, the point of the needle lies between, (the north, south, east and west being called the four cardinal points, and are graved on the bottom of the box) putting down those points, together by their initial letters, and thereto annexing the number of degrees, counting from the north or south, as before, thus; if the point of your needle lies between the north and east, north and west, south and east, or south and west points in the bottom of the box, then put down NE, NW, SE, or SW, annexing thereto the number of degrees cut by the needle on the side of the ring, counting from the north or south as before.

158 THE CIRCUMFERENTOR.

But if the needle point exactly to the north, south, east, or west, you are then to write down N, S, E, or W, without annexing any degree.

This is the manner of taking field notes, whereby the content of ground may be universally determined by calculation; and they are said to be taken by the quartered compass, or by the four nineties.

To find the number of degrees contained in any given angle.

Set up your instrument at the angular point, and thence direct the sights along each leg of the angle, and note down their respective bearings, as before; the difference of these bearings, if less than 180, will be the quantity of degrees contained in the given angle; but if more, take it from 360, and the remainder will be the degrees contained in the given angle.

THE

THEODOLITE.

HIS instrument is a circle, commonly of brass, of ten or twelve inches in diameter, whose limb is divided into 360 degrees, and those again are subdivided into smaller parts, as the magnitude of it will admit; sometimes by equal divisions, and sometimes by diagonals, drawn from one concentric circle of the limb to another.

In the middle is fixed a circumferentor, with a needle; but this is of little or no use, except in finding a meridian line, or the proper situation of the land.

Over the brass circle is a pair of sights, fixed to a moveable index, which turns on the centre of the instrument, and upon which the circumferentor-box is placed.

This instrument will either give the angles of the field, or the bearing of every stationary distance line, from the meridian; as the circumferentor and quartered compass do.

To take the angles of the field.

PL. 6. fig. 6.

Lay the ends of your index to 360°, and 180°; turn the whole about with the 360 from you; direct

the sights from A to G, and screw the instrument fast; direct them from A, to cut the object at B; the degree then cut by that end of the index which is opposite you, will be the quantity of the angle GAB, to place in your field-book; to which annex the measure of the line AB, in chains and links; set up your instrument at B, unscrew it, and lay the ends of your index to 360 and 180; turn the whole about with the 360 from you, or 180 next you, till you cut the object at A; screw the instrument fast, and direct your sights to the object at C; and the degree then cut by that end of the index which is opposite to you, will be the quantity of the angle ABC. Thus proceed from station to station, still laying the index to 360, turning it from you, and observing the object at the foregoing station, screwing the instrument fast, and observing the object at the following station, and counting the degrees to the opposite end of the index, will give you the quantity of each respective angle.

LEMMA.

All the angles of any polygon, are equal to twice as many right angles as there are sides less by four. Thus, all the angles A, B, C, D, E, F, G, are equal to twice as many right angles as there are sides in the figure, less by four.

PL. 6. fig. 6.

Let the polygon be disposed into triangles, by lines drawn from any assigned point H within it, as by the lines HA, HB, HC, &c. It is evident then (by theo. 2. sect. 4. part 1.) that the three angles of each triangle are equal to two right; and consequently, that the angles in all the triangles are twice as many right ones as there are sides:

but all the angles about the point H, are equal to four right (by cor. 2. theo. 1. sect. 4.); therefore the remaining angles are equal to twice as many right ones as there are sides in the figure, abating four. Q. E. D.

SCHOLIUM.

Hence we may know if the angles of a survey be truly taken; for if their sum be equal to twice as many right angles, as there are stations, abating four right angles, you may conclude that the angles were truly taken, otherwise not.

If you take the bearing of any line with the circumferentor, that bearing will be the number of degrees the line is from the north; consequently the north must be a like number of degrees from the line, and thus the north, and of course the south, as well as the east and west, or the situation of the land, is obtained.

To take the bearing of each respective line from the meridian; or to perform the office of the circumferentor, or quartered compass by the theodolite.

Set your instrument at the first station, and lay the index to 360° and 180°, with the flower-de-luce of the box next 360; unscrew the instrument, and turn the whole about, till the north and south points of the needle cut the north and south points in the box; then screw it fast, and the instrument is north and south, if there be no variation in the needle; but if there be, and its quantity known, it may be easily allowed.

The circumferentor-box may then be taken off.

Direct the sights to the object at the second station, and the degree cut by the opposite end of the index will be the bearing of that line from the north, and the same that the circumferentor would give.

After having measured the stationary distance, set up your instrument at the second station; unscrew it, and set either end of the index to the degree of the last line, and turning the whole about with that degree towards you, direct your sights to an object at the foregoing station, and screw the instrument fast; it will then be parallel to its former situation, and consequently north and south; direct then your sights to an object at the following station, and the degree cut by the opposite end of the index, will be the bearing of that line.

In like manner you may proceed through the whole.

If the brass circle be divided into four nineties, from 360 and 180, and the letters N, S, E, W, be applied to them; the bearings may be obtained by putting down the letters the far or opposite end of the index lies between, and annexing thereto the degrees from the N or S; and this is the same as the quartered compass.

If you keep the compass box on, to see the mutual agreement of the two instruments; after having fixed the theodolite north and south, as before; turn the index about with the north end or flower-de-luce next your eye, and count the degree to the opposite, or south end of the index, and this will correspond with the degree cut by the south end of the needle.

At the second, or next station, unscrew the instrument, and set the south of the index to the degree of the last station; turn the whole about, with the south of the index to you, and cut the object at the foregoing station; screw the instrument fast, and with the north of the index to you, cut the object at the next following station, the degree then cut by the south of the index, will correspond with the degree cut by the south end of the needle, and so through the whole.

Some theodolites have a standing pair of sights fixed at 360 and 180, besides those on the moveable index; if you would use both, look through the standing sights, with the 180 next you, to an object at the foregoing station: screw the instrument fast, and direct the upper sights on the moveable index, to the object at the following station, and the degree cut by the opposite end of the index, will give you the quantity of the angle of the field.

Two pair of sights can be of no use in finding the angles from the meridian; and inasmuch as one pair is sufficient to find the angles of the field, the second can be of no use: besides, they obstruct the free motion of the moveable index, and therefore are rather an incumbrance than of any real use. Some will have it, that they are useful with the others, for setting off a right angle, in taking an off-set: and surely this is as easily performed by the one pair on the moveable index: thus, if you lay the index to 360 and 180, and cut the object either in the last or following station, screw the instrument fast, and turn the index to 90 and 270, and then it will be at right angles with the line. So that the small sights, at those of the circle, can be

of no additional use to the instrument, and therefore should be laid aside as useless.

This instrument may be used in windy and rainy weather, as well as in mountainous and hilly grounds; for it does not require an horizontal position to find the bearing, or angle, as the needle doth; and therefore is preferred to any instrument that is governed by the needle.

THE SEMICIRCLE.

HIS instrument, as its name imports, is a half circle, divided from its diameter into 180 degrees, and from thence again, that is, from 0, to 360 degrees: it is generally made of brass, and is from 8 to 18 inches diameter.

On the centre there is a moveable index with sights, on which is placed a circumferentor-box, as in the theodolite.

This instrument may be used as the theodolite in all respects; but with this difference, when you are to reckon the degree to that end of the index which is off the semicircle, you may find it at the other end, reckoning the degree from 180 forwards.

THE

PLANE TABLE.

A PLANE TABLE is an oblong of oak, or other wood, about 15 inches long, and 12 broad; they are generally composed of 3 boards, which are easily taken asunder, or put together, for the convenience of carriage.

There is a box frame, with 6 joints in it, to take off and put on as occasion serves; it keeps the table together, and is likewise of use to keep down a sheet of paper which is put thereon.

The outside of the frame is divided into inches and tenths, which serve for ruling parallels or squares on the paper, or for shifting it, when occasion serves.

The inside of the frame is divided into 360 degrees, which, though unequal on it, yet are the degrees of a circle produced from its centre, or centre of the table, where there is a small hole.

The degrees are subdivided as small as their distance will admit; at every tenth degree are two numbers, one the number of degrees, the other its complement to 360.

There is another centre hole about fof the table's breadth from one edge, and is in the mid-

dle between the two ends. To this centre hole on the other side of the frame, there are the divisions of a semicircle, or 180 degrees; and these again are subdivided into halves, or quarters, as the size of the instrument will admit.

That side of the frame on which the 360 degrees are, supplies the place of a theodolite, the other, that of a semicircle.

There is a circumferentor-box of wood, with a paper chart at the bottom, applied to one side of the table by a dove-tail joint, fastened by a screw. This box (besides its rendering the plane table capable of answering the end of a circumferentor) is very useful for placing the instrument in the same position every remove.

There is a brass ruler or index, of about two inches broad, with a sharp or fiducial edge, at each end of which is a sight; on the ruler are scales of equal parts, with and without diagonals, and a scale of chords; the whole is fixed on a ball and socket, and set on a three-legged staff.

To take the angles of a field by the table.

Having placed the instrument at the first station, turn it about till the north end of the needle be over the meridian, or flower-de-luce of the box, and there screw it fast. Assign any convenient point, to which apply the edge of the index, so as through the sights you may see the object in the last station, and by the edge of the index from the point draw a line. Again, turn about the index with its edge to the same point, and through the sights ob-

serve the object in the second station, and from the point, by the edge of the index, draw another line; so is the angle laid down; on that last line set off the distance to the second station, in chains and links; apply your instrument to the second station, taking the angle as before; and after the like manner proceed till the whole is finished.

This method may be used in good weather, if the needle be well touched and play freely; but if it be in windy weather, or the needle out of order, it is better, after having taken the first angle as before, and having removed your instrument to the second station, and placed the needle over the meridian line as before, to lay the index on the last drawn line, and look backward through the sights; if you then see the object in the first station, the table is fixed right, and the needle is true; if not, turn the table about, the index lying on the last line, till through the sights you see the object in the first station: and then screw it fast, and keeping the edge of the index to the second station, direct your sights to the next; draw a line by the edge of the index, and lay off the next line; and proceed through the whole without using the needle, as you do with the theodolite.

If the sheet of paper on the table be not large enough to contain the map of the ground you survey, you must put on a clean sheet, when the other is full; and this is called shifting of paper, and is thus performed.

PL. 6. fig. 8.

Let ABCD represent the sheet of paper on the plane table, upon which the plot E, F, G, H, I,

K, L, M, is to be drawn; let the first station be E; proceed as before from thence to F, and to G; then proceeding to H, you find there is not room on your paper for the line GH; however draw as much of the line GH, as the paper can hold, or draw it to the paper's edge. Move your instrument back to the first station E, and proceed the contrary way to M, and to L; but in going from thence to K, you again find your sheet will not hold it; however, draw as much of the line LK on the sheet as it can hold.

Take that sheet off the table, first observing the distance oo of the lines GH and LK, by the edge of the table; take off that sheet, and mark it with No. 1, to signify it to be the first taken off. Having then put on another sheet, lay that distance oo on the contrary end of the table, and so proceed as before, with the residue of the survey, from o to H, to K, and thence to o; so is your survey complete.

In the like manner you may proceed to take off, and put on, as many sheets as are convenient; and these may afterwards be joined together with mouth glue, or fine white wafer, very thin.

If the index be fixed to the first centre, using the 360 side, it will then serve as a theodolite, and when to the second centre, using the 180 side, it will serve as a semicircle; by either of which you may survey in rainy weather, when you cannot have paper on the table.

To measure Angles of Altitude by the Circumplementor, Theodolite, Semicircle, or Plane Table.

1. To take an angle of altitude, by the circumferentor.

LAET the glass lid be taken off, and let the instrument be turned on one side, with the stem of the ball into the notch of the socket, so that the circle may be perpendicular to the plane of the horizon; let the instrument be placed in this situation before the object, so that the top thereof may be seen through the sights; let a plummet be suspended from the centre pin, and the object being then observed, the complement of the number of degrees, comprehended between the thread of the plummet, and that part of the instrument which is next your eye, will give the angle of altitude required.

2. If an angle of altitude is to be taken by the theodolite, or semicircle, let a thread be run through a hole at the centre, and a plummet be suspended by it; turn the instrument on one side, by the help of the ball and notch in the socket for that purpose, so that the thread may cut 90, having 360 degrees next you; screw it fast in that position, and through the sights cut the top of the objects; and the degrees then cut by the end of the index next you, are the degrees of elevation required. An angle of depression is taken the contrary way.

170 OF ANGLES OF ELEVATION, &c.

3. By the plane table an angle of altitude is taken in the like manner, by suspending a plummet from the centre thereof, having turned the table on one side, and fixed the index to the centre by a screw, so as to move freely, let the thread cut 90, look through the sights as before, and you have the angle of elevation, and on the contrary that of depression.

THE

PROTRACTOR.

THE protractor is a semicircle annexed to a scale, and is made of brass, ivory, or horn; its diameter is generally about five or six inches.

The semicircle contains three concentric semicircles at such distances from each other, that the spaces between them may contain figures.

The outward circle is numbered from the right to the left hand, with 10, 20, 30, &c. to 180 degrees; the middlemost the same way, from 180 to 360 degrees; and the innermost from the upper edge of the scale both ways, from 10, 20, 30, &c. to 90 degrees.

It is easy to conceive that the protractor, though a semicircle, may be made to supply the place of a whole circle; for if a line be drawn, and the centre-hole of the protractor be laid on any point in that line, the upper edge of the scale corresponding with that line, the divisions on the edge of the semicircle will run from 0 to 180, from right to left: again, if it be turned the other way, or downwards, keeping the centre-hole thereof on the aforesaid point in the line, then the divisions will run from

180 to 360, and so completes an entire circle with the former semicircle.

The use of the protractor is to lay off angles, and to delineate or draw a map, or plan of any ground from the field notes; and is performed in the following manner.

To protract a field-book, when the angles are taken from the meridian.

PL 6. fig. 9.

On your paper rule lines parallel to each other, at an inch asunder (being most usual), or at any other convenient distance; on the left end of the parallels put N. for north, and on the right S. for south; put E. at the top for east, and W. at the bottom of your paper for west.

Then let the following field-book be that which is to be protracted, the bearings being taken from the meridian, whether by a circumferentor, theodolite, or semicircle, and measured with a two-pole chain.

No.	Bearing.	Ch. L.
1	283½	55.20
2	348‡	12.36
3	317	29.20
4	266	55.20
5	193	40.00
6	124	76.00
7	63‡	87.02
Close at the first station,		

Pitch upon any convenient point on your paper for your first station, as at 1, on which lay the centre-hole of your protractor, with a protracting pin; then if the degrees be less than 180, turn the arc of your protractor downwards, or towards the west; but if more than 180, upwards, or towards the east,

Or if the right hand be made the north, and the left the south, the west will be then up, and the east down.

In this case, if the degree be less than 180, turn the arc of your protractor upwards, or towards the west; and if more, downwards, or towards the east.

By the foregoing field-book, the first bearing is 283½, turn the arc of your protractor upwards, keeping the pin in the centre-hole, move the protractor so that the parallel lines may cut opposite divisions, either on the ends of the scale, or on the degrees, and then it is parallel. This must be always first done, before you lay off your degrees.

Then by the edge of the semicircle, keeping the protractor steady, with the pin prick the first bearing $283\frac{1}{2}$, and from the centre point, through that point or prick, draw a blank line with the pin, on which from a scale of equal parts, or from the scale's edge of the protractor, lay off the distance $55C.\ 20L.$ so is that station protracted.

At the end of the first station, or at 2, which is the beginning of the second, with the pin place the centre of the protractor, turning the arc up, because the bearing of the second station is more

than 180, viz. 3484. Place your protractor parallel as before, and by the edge of the semicircle, with the pin prick at that degree, through which and the end of the foregoing station, draw a blank line, and on it set the distance of that station.

In the like manner proceed through the whole, only observe to turn the arc of your protractor down, when the degrees are less than 180.

If you lay off the stationary distances by the edge of the protractor, it is necessary to observe, that if your map is to be laid down by a scale of 40 perches to an inch, every division on the protractor's edge will be one two-pole chain; a division will be 12½ links.

If your map is to be laid down by a scale of 20 perches to an inch, two divisions will be one two-pole chain; one division will be 25 links; a division 12½ links, and 5 of a division will be 6½ links.

In general, if 25 links be multiplied by the number of perches to an inch, the map is to be laid down by, and the product be divided by 20 (or which is the same thing, if you cut off one and take the half), you will have the value of one division on the protractor's edge, in links and parts.

Examples.

1. How many links in a division, if a map be laid down by a scale of 8 perches to an inch?

25

8

2|0)20|0

10 links. Answer.

2. How many links in a division, if a map be laid down by a scale of 10 perches to an inch?

25

10

20)250

12.5 or 121 links. Answer.

And so of any other.

To protract a field-book, taken by the angles of the field.

Note. We here suppose the land surveyed is kept on the right hand as you survey.

Draw a blank line with a ruler of a length greater than the diameter of the protractor; pitch upon any convenient point therein, to which apply the centre-hole of your protractor with your pin, turning the arc upwards if the angle be less than 180, and downwards if more; and observe to keep the upperedge of the scale, or 180 and 0 degrees upon the line: then prick off the number of degrees contained in the given angle, and draw a line from the first point through the point at the degrees; upon which lay the stationary distance. Let this line be lengthened forwards and backwards, keeping your first station to the right, and second to the left;

and lay the centre of your protractor over the second station, with your pin, turning the arc upwards, if the angle be less than 180, and downwards, if more; and keeping the 180 and 0 degrees on the line, prick off the number of degrees contained in the given angle, and through that point and the last station draw a line, on which lay the stationary distance; and in like manner proceed through the whole.

In all protractions, if the end of the last station falls exactly in the point you began at, the field-work and protraction are truly taken, and performed; if not, an error must have been committed in one of them: in such case make a second protraction; if this agrees with the former, and neither meet nor close, the fault is in the field-work, and not in the protraction; and then a re-survey must be taken.

REMARKS.

The accuracy of geometrical and trigonometrical mensuration, depends in a great degree on the exactness and perfection of the instruments made use of; if these are defective in construction, or difficult in use, the surveyor will either be subject to error, or embarrassed with continual obstacles. If the adjustments, by which they are to be rendered fit for observation, be troublesome and inconvenient, they will be taken upon trust, and the instrument will be used without examination, and thus subject the surveyor to errors, that he can neither account for, nor correct.

In the present state of science, it may be laid down as a maxim, that every instrument should be

so contrived, that the observer may easily examine and rectify the principal parts; for however careful the instrument-maker may be, however perfect the execution thereof, it is not possible that any instrument should long remain accurately fixed in the position in which it came out of the maker's hand, and therefore the principal parts should be moveable, to be rectified occasionally by the observer.

AN ENUMERATION OF INSTRUMENTS USEFUL TO A SURVEYOR:

Fewer or more of which will be wanted, according to the extent of his work, and the accuracy required.

A case of good pocket instruments.

A pair of beam compasses.

A set of feather-edged plotting scales.

Three or four parallel rules.

A pair of proportional compasses.

A pair of triangular ditto.

A pantagraph.

A cross staff.

A circumferentor.

An Hadley's sextant.

An artificial horizon.

A theodolite.

A surveying compass.

Measuring chains, and measuring tapes.

King's surveying quadrant.

A perambulator, or measuring wheel.

A spirit level with telescope.

Station staves, used with the level

A protracter, with or without a nonius.

To be added for county and marine surveying;

An astronomical quadrant, or circular instrument.

A a

A good refracting and reflecting telescope. A copying glass.

For marine surveying;

A station pointer. An azimuth compass. One or two boat compasses.

Besides these, a number of measuring rods, iron pins, or arrows, &c. will be found very convenient, and two or three offset staves, which are straight pieces of wood, six feet seven inches long, and about an inch and a quarter square; they should be accurately divided into ten equal parts, each of which will be equal to one link. These are used for measuring offsets, and to examine and adjust the chain.

Five or six staves of about five feet in length, and one inch and an half in diameter, the upper part painted white, the lower end shod with iron, to be struck into the ground as marks.

Twenty or more iron arrows, ten of which are always wanted to use with the chain, to count the number of links, and preserve the direction of the chain, so that the distance measured may be really in a straight line.

The pocket measuring tapes, in leather boxes, are often very convenient and useful. They are made to the different lengths of one, two, three, four poles, or sixty-six feet and 100 feet; divided, on one side, into feet and inches, and on the other into links of the chain. Instead of the latter, are sometimes placed the centesimals of a yard, or three feet into 100 equal parts.

SECTION IL

MENSURATION

OF HEIGHTS AND DISTANCES.

1st. Of Heights.

PL. 5. fig. 18.

HE instrument of least expence for taking heights, is a quadrant, divided into ninety equal parts or degrees; and those may be subdivided into halves, quarters, or eighths, according to the radius, or size of the instrument: its construction will be evident by the scheme thereof.

From the centre of the quadrant let a plummet be suspended by a horse hair: or a fine silk thread of such a length that it may vibrate freely, near the edge of its arc: by looking along the edge AC, to the top of the object whose height is required; and holding it perpendicular, so that the plummet may neither swing from it, nor lie on it; the degree then cut by the hair, or thread, will be the angle of altitude required.

If the quadrant be fixed upon a ball and socket on the three-legged staff, and if the stem from the ball be turned into the notch of the socket, so as to bring the instrument into a perpendicular position, the angle of altitude by this means, can be acquired with much greater certainty.

An angle of altitude may be also taken by any of the instruments used in surveying; as has been

particularly shown in treating of their description and uses.

Most quadrants have a pair of sights fixed on the edge AC, with small circular holes in them; which are useful in taking the sun's altitude, requisite to be known in many astronomical cases; this is effected by letting the sun's ray, which passes through the upper sight, fall upon the hole in the lower one; and the degree then cut by the thread, will be the angle of the sun's altitude; but those sights are useless for our present purpose, for looking along the quadrant's edge to the top of the object will be sufficient, as before.

PROB. I.

PL. 5. fg. 19.

To find the height of a perpendicular object at one station, which is on an horizontal plane.

A steeple.

Given, { The angle of altitude, 53 degrees. Distance from the observer to the foot of the steeple, or the base, 85 feet. Height of the instrument, or of the observer, 5 feet.

Required, the height of the steeple.

The figure is constructed and wrought, in all respects, as case 2. of right-angled trigonometry; only there must be a line drawn parallel to, and beneath AB of 5 feet for the observer's height, to represent the plane upon which the object stands;

to which the perpendicular must be continued, and that will be the height of the object.

Thus, AB is the base, A the angle of altitude, BC the height of the steeple from the instrument, or from the observer's eye, if he were at the foot of it; DC the height of the steeple above the borizontal surface.

Various statings for BC, as in case 2. of right-angled plane trigonometry.

To BC 112.8
Add DB 5. the height of the observer.

Their sum is 117. 8 or 118 feet, the height of the steeple required.

PROB. II.

PL. 5. fig. 20.

To find the height of a perpendicular object, on an horizontal plane; by having the length of the shadow given.

Provide a rod, or staff, whose length is given, let that be set perpendicular, by the help of a quadrant, thus; apply the side of the quadrant AC, to the rod, or staff; and when the thread cuts 90° it is then perpendicular; the same may be done by a carpenter's or mason's plumb.

Having thus set the rod or staff perpendicular; measure the length of its shadow, when the sun shines, as well as the length of the shadow of the object, whose height is required; and you have the proper requisites given. Thus,

ab, the length of the shadow of the staff, 15 feet.

bc, the length of the staff, 10 feet.

AB, the length of the shadow of the steeple, or object, 135 feet.

Required BC, the height of the object.

The triangles abc, ABC, are similar, thus; the angle b=B, being both right; the lines ac, AC are parallel, being rays, or a ray of the sun; whence the angle a=A (by part 3. theo. 3. sect. 4.) and consequently c=C. The triangles being therefore mutually equiangular, are similar (by theo. 16. sect. 4) it will be,

 $ab \cdot bc : AB : BC$.
15 10 135 90. the steeple's height, required.

The foregoing method is most to be depended on; however, this is mentioned for variety's sake.

PROB. III.

P1. 5. fig. 21.

To take the altitude of a perpendicular object, at the foot of a hill, from the hill's side.

Turn the centre A of the quadrant, next your eye, and look along the side AC, or 90 side, to the top and bottom of the object; and noting down the angles, measure the distance from the place of observation to the foot of the object. Thus,

Given, Angle to the foot of the object, 55% or 55°. 15'
Angle to the top of it, 31% or 31°. 15'
Distance to the foot of it, 250 feet.

Required, the height of the object.

By Construction.

Draw an indefinite blank line AD, at any point in which A make the angles EAB of 55°. 15′, and EAC of 31°. 15′; lay 250 from A to B; from B, draw the perpendicular BE (by prob. 7 of geometry (crossing AC in C; so will BC be the height of the object required.

In the triangle ABC there is given,

ABE the complement of EAB to 90°, which is 34°. 45'.

. CAB the difference of the given angle 24°.00'.

The side AB, 250. Required, BC.

This is performed as case 2. of oblique angular trigonometry. Thus,

180—the sum of ABE 34°. 45′, and CAB 24°. 00′ = ACB 121°. 15′. Then,

S. ACB: AB:; S. CAB: BC.
121°. 15' 250 24°. 00' 119, the height required.

PROB. IV.

PL. 5. fg. 22.

To take the altitude of a perpendicular object, on the top of a hill, at one station; when the top and bottom of it can be seen from the fost of the hill.

As in prob. 1. take an angle to the top, and another to the bottom of the object; and measure from the place of observation to the foot of the object, and you have all the given requisites. Thus,

A Tower on a hill.

Given, Angle to the bottom, 48°. 36'.

Angle to the top, 67°.00'.

Dist. to the foot of the object, 136 feet.

Required, the height of the object.

By Construction.

Make the angle $DAB=48^{\circ}$ 30', and lay 136 feet from A to B; from B, let fall the perpendicular BD; and that will be the height of the hill; produce BD upwards by a blank line: again, at A, make the angle $DAC=67^{\circ}$ 00' by a blank line, and from C where that crosses the perpendicular produced, draw the line CB, and that will be the height of the object required.

Let AC be drawn.

In the triangle ABC, there is given,

The angle ACD the complement of $DAC=23^{\circ}.00'$.

CAB the difference between the two given angles=18°. 30'.

And the side AB 136. To find BC.

SC: AB: S.CAB: BC. 23° 136 18°. 30′ 110½.

If BD were wanted, it is easily obtained, by the first case of right-angled plane trigonometry.

PROB. V.

PL. 5. fig. 23.

To take an inaccessible perpendicular altitude, on a horizontal plane.

This is done at two stations, thus:

Let DC be a tower which cannot be approached by means of a moat or ditch, nearer than B; at B, take an angle of altitude, to C: measure any convenient distance backward to A, which note down; at A, take another angle to C; so have you the given requisites, thus:

Given, { First angle, 55°. 00′. Stationary distance, 87 feet. Second angle, 37°. 00′.

The height of the tower CD, is required.

By Construction.

Upon an indefinite blank line, lay off the stationary distance 87, from A to B; from B, set off your first; and from A, your second angle; from C, the point of intersection of the lines which form these angles, let fall the perpendicular CD; and that will be the height of the object required.

The external angle CBD, of the triangle ABC; is equal to the two internal opposite ones, A, and ACB (by theo. 4. sect. 4.): wherefore if one of the internal opposite angles be taken from the external angle, the remainder will be the other internal opposite one, thus;

 $CBD 55^{\circ} - A 37^{\circ} = ACB 18^{\circ}$.

Therefore in the triangle ABC; we have the angles A, and AGB, with the side AB given to find BC.

S. ACB: AB:: S. A: BC. 18° 87 37° 169.4 Having found BC, we have in the triangle BCD the angle CBD 55°, consequently BCD 35°, and BC 169.4; to find DC.

This is performed by the first case of right-angled trigonometry, three several ways; thus:

1. R: BC:: S. CBD: DC. 90° 169.4 55° 138.8. The height required.

2. Sec. CBD: BC:: T. CBD: DC. 55° 169.4 55° 138.8.

The height required.

3. Sec. BCD: BC:: R: CD.
35° 169.4 90° 138.8.

The height required.

If BD, the breadth of the moat, were required; it may also be found, by three different statings, as in the first case of right-angled plane trigonometry.

PROB. VI.

P.L. 5. fig. 24.

Let BC, a may-pole, whose height is 100 feet, be broken at D; the upper part of which, DC, falls upon an horizontal plane, so that its extremity, C, is 34 feet from the bottom or foot of the pole.

Required, the segments BD and DC.

By Construction.

Lay 34 feet from A to B; on B erect the perpendicular BC of 100 feet; and draw AC; bisect

AC (by prob. 4. geom.) with the perpendicular line, EF; and from D, where it cuts the perpendicular BC, draw AD, which will be the upper segment; and DB will be the lower.

By cor. to lemma, preceding theo. 7. geom. AD=DC; and (by the lemma) the angle C=CAD.

In the triangle ABC, find C as in case 6, of rightangled trigonometry, thus;

1.
$$BC:R::AB:T.C=GAD.$$
100 90° 34 18° 47′

By theo. 4. geom. The external angle $ABD = 37^{\circ} 34'$, or to twice the angle C, i. e. to C and GAD.

Then in the triangle ABD, there is ABD 37° 34', therefore also its complement DAB 52° 26', and AB 34, given, to find AD and BD.

By the second case of right-angled trigonometry.

$$BC-DC=BD$$
.
100-55.77=44.23 required.

These may be had from other statings, as in the second case aforesaid.

PROB. VII.

PL. 5. fig. 25.

To take the altitude of a perpendicular object on a hill, from a plane beneath it.

This is done at two stations, thus;

Let the height DC, of a wind-mill on a hill be required.

From any part of the plane whence the foot of the object can be seen, let angles be taken to the foot and top; measure thence any convenient distance towards the object, and at the end thereof, take another angle to the top: and you have the proper requisites, thus;

First station. Angle to the foot DAB 21°00'.

Angle to the top CAB 35°00'.

Stationary distance AB 104 feet.

Second station.

Angle to the top 48° 30.

DC required.

By Construction.

On an indefinite blank line, lay the stationary distance AB 104 feet; from A, set off the second, and from B, the third given angle; and from the intersecting point C of the line formed by them, let fall the perpendicular CE; from A set off the first angle, and the line formed by it will determine the point D. Thus have we the height of the hill, as well as that of the wind-mill.

The angle CBE-A=ACB, as in the last prob. In the triangle ABC, find AC thus;

S. ACB: AB:: S. ACB (or sup. of CBE): AC 13°. 30′: 104:: 131°.30′: 333.6

The angle CAE - DAE = CAD.

The angle $ACD = AED \times EAD$, by theo. 4.

In the triangle CAD, find CD thus,

S. ADC: AC: S. CAD: DC 111.: 333.6:: 14:86.46 required.

CE, BE, or DE, may be found by other various statings, as set forth in the first and second cases of right-angled trigonometry.

PROB. VIII.

Pt. 5. fig. 26.

To find the length of an object, that stands obliquely on the top of a hill, from a plane beneath.

Let CD be a tree whose length is required.

This is done at two stations.

Make a station at B, from whence take an angle to the foot, and another to the top of the tree; measure any convenient distance backward to A, from whence also let an angle be taken to the foot, and another to the top; and you have the requisites given. Thus,

First station. Angle to the foot $EBD=36^{\circ}$. 30'. Angle to the top $EBC=44^{\circ}$. 30'. Stationary distance AB=104 feet.

Second station. Angle to the foot $EAD=24^{\circ}$. 30'. Angle to the top $EAC=32^{\circ}$. 00'.

Let DC and DE be required.

The geometrical constructions of this and the next problem are omitted; as what has been already said, and the figures, are looked upon as sufficient helps.

EBC-A=ACB, or 44°. 30′—32°.=12°. 30′. as before.

In the triangle ABC, find BC. Thus,

1. S. ACB : AB :: S. A : BC. 12°. 30′ 104 32° 254.7.

 $EBD-EAD=ADB_{1}$ or 36°. 30′-24°. 30′=12° 00′

In the triangle ADB, find DB, thus;

2. S. ADB : AB : : S. DAB : DB. 12°00′ 104 24°. 30′. 207.4

CBE - DBE = CBD, or 44°. 30′—36°. 30′ = 8°00′

In the triangle CBD there is given, CB 254.7, DB 207.4, and the angle CBD 8° 00′; to find DC.

This is performed as case 3. of oblique angled trigonometry, thus;

3. BC × BD · BC—BD :: T. of BDC+BCD / 462.1 47.3 86°. 00′. T. of BDC—BCD.

55°. 40′.

86°. 00' + 55°. 40' = 141°. 40' = BDC. 86°. 00' - 55°. 40' = 30°. 20' = BCD.

4. S. BCD: BD: S. CBD: DC. 30°. 20′ 207.4 8°. 00′ 57.15 length of the tree.

To find DE in the triangle DBE.

Say R.: BD:: S. DBE: DE, 90°. 207.4 36°. 30′ 123.4 height of the hill.

PROB. 1X.

To find the height of an inaccessible object CD, on a hill BC, from ground that is not horizontal.

PL. 6. fig. 1.

From any two points, as G and A, whose distance GA, is measured, and therefore given; let the angles HGD, BAD, BAC, and EAG, be taken; because GH is parallel to EA (by part 2. theo. 3. geom.) the angle HGA=EAG; therefore $EAG \times HGD=AGD$: and (by cor. 1. theo. 1. geom) 180—the sum of EAG and BAD=GAD; and, (by cor. 1. theo. 5. geom.(180—the sum of the angles AGD and GAD=GDA: thus we have the angles of the triangle AGD, and the side AG given; thence (by case 2. of obl. ang. trig.) AD may be easily found. The angle DAB-CAB = DAC, and $90^{\circ}-BAD=ADC$; and $180^{\circ}-$ the sum of DAC and ADC=ACD: so have we the

several angles of the triangle ACD given, and the side AD; whence (by case 2. of obl. trig.) CD may be easily found. We may also find AC, which with the angle BAC, will give CB the height of the hill.

The solutions of the several problems in heights and distances, by Gunter's scale, are omitted; because every particular stating has been already shewn by it, in trigonometry.

2d. OF DISTANCES.

THE principal instruments used in surveying, will give the angles or bearings of lines; which has been particularly shewn, when we treated of them.

PROB. I.

P1. 6. fig. 2.

Let A and B be two houses on one side of a river, whose distance asunder is 293 perches: there is a tower at C on the other side of the river, that makes an angle at A, with the line AB of 53° 20'; and another at B, with the line BA of 66° 20'; required the distance of the tower from each house, viz. AC and BC.

This is performed as case 2. of oblique angled trigonometry, thus;

1. S. C: AB:: S. A: BC. 60° 20′ 293 53° 20′ 270.5.

2. S. C : AB : : S. B : AC. 60° 20′ 293 66° 20′ 308.8.

PROB. II.

PL. 6. fig. 11.

Let B and C, be two houses whose direct distance as under, BC, is inaccessible: however it is

known that a house at A is 252 perches from B, and 230 from C; and that the angle BAC, is found to be 70°. What is the distance BC, between the two houses?

This is performed as case 3. of oblique angled trigonometry, thus;

55+3°. 44' = 58°. 44' = C. 55° — 3°. 44' = 51°, 16 = B.

2. S. C: AB:: S. A: BC. 58°. 44′ 252 70° 277.

PROB. 111.

PL. 6. fig. 3.

Suppose ABC a triangular piece of ground, which by an old survey we find to be thus; AB 260, AC 160, BC 150 perches, the mearing lines AC and BC, are destroyed or plowed down, and the line AB, only remaining. What angles must be set off at A and B, to run new mearings by exactly where the old ones were?

This is performed as in case 4. of oblique angled trigonometry, thus;

130 + 5.96 = 135.96 = AD. 130 - 5.96 = 124.04 = DB.

2. AD: R:: AC: Sec. A. 136 90 :: 160 312.47'.

3. BC: S. A:: AC: S. B. 150 31°. 47′ 160 34°. 10.

PROB. IV.

PL. 6. fig. 4.

Let D and C, be two trees in a bog, to which you can have no nearer access than at A and B; there is given, DAB 100°, CAB 36°. 30′, CBA 121°. DBA 49°, and the line AB 113 perches. Required, the distances of the trees DC.

180°—the sum of DBA and DAB=ADB=31°.
180°—the sum of CAB and CBA=ACB=22. 30.

In the triangle ABD, find DB, thus;

1. S. ADB: AB: S. DAB: DB. 31° 113:: 100° 216.

And in the triangle ABC, find BC, thus;

2. S. ACB : AB :: S. CAB : BC. 22° 30′ 113 36° 30′ 175.6.

In the triangle DBC, you have $DBC=ABC-ABD=72^{\circ}$; likewise the sides BD, BC, as before found, given to find DC.

3. BD+BC: BD—BC:: T.of \(\frac{1}{2}\) DCB+CDB: 391.6 40.4 54°

T. of $\frac{1}{2}$ DCB—CDB.

8° 05'.

 $54^{\circ} + 8^{\circ} 05' = 62^{\circ} 05' = DCB$, $54^{\circ} - 8^{\circ} 05' = 45^{\circ} 55' = CDB$.

4. S. CDB : BC : S. DBC : DC. 45° 55′ 175.6 72° 232.5.

LEMMA.

PL. 6. fig. 12.

If from a point C, of a triangle ABC, inscribed in a circle, there be a perpendicular CD, let fall upon the opposite side AB; that perpendicular is to one of the sides, including the angle, as the other side, including the angle, is to the diameter of the circle, i. e. DC: AC:; CB: CE.

Let the diameter CE be drawn, and join EB; it is plain the angle CEB = CAB (by cor. 2. theo. 7. geom.) and CBE is a right angle (by cor. 5. theo. 7. geom.) and =ADC: whence ECB = ACD. The triangles CEB, CAD, are therefore mutually equiangular, and (by theo. 16. geom.) DC:AC:CB:CE, or DC:CB:AC:CE. Q. E. D.

PROB. V.

Pl. 6. fig. 5.

Let three gentlemen's seats, A, B, C, be situate in a triangular form: there is given, AB 2.5 miles, AC 2.3, and BC 2. It is required to build a church at E, that shall be equi-distant from the seats A, B, C. What distance must it be from each seat, and by what angle may the place of it be found?

By Construction.

By prob. 15. geom. Find the centre of a circle that will pass through the points, A, B, C: and that will be the place of the church; the measure of which, to any of these points, is the answer for the distance: draw a line from any of the three points to the centre, and the angle it makes with either of the sides that contain the angle it was drawn to; that angle laid off by the direction of an instrument, on the ground, and the distance before found, being ranged thereon, will give the place of the church required.

By Calculation.

1.
$$AB : AC+BC :: AC-BC : AD-DB$$
.
2.5 4.3 .3 .516.

1.25 + .258 = 1.508 = AD.

By cor. 2. theo. 14. geom. The square root of the difference of the squares of the hypothenuse AC, and given leg AD, will give DC.

That is, 5.29 - 2.274064 = 3.015936.

Its square root is 1.736 = CD.

Then by the preceding lemma,

2. CD: AC: CB: the diameter. 1.736 2.3 2 2.65.

the half of which, viz. 1.325 is the semi-diameter, or distance of the church from each seat, that is, AE, CE, BE.

From the centre E, let fall a perpendicular upon any of the sides as EF, and it will bisect in E: (by theo. 8. geom.)

Wherefore $AF = CF = \frac{1}{2}AC = 1.15$.

In the right angled triangle AFE, you have AF 1.15, and AE the radius 1.325 given, to find FAE, thus;

3. AF : /R. : : AE : Sec. FAE.
1.15 90° 1.325 29° 47′.

Wherefore directing an instrument to make an angle of 29° 47′, with the line AC; and measuring 1.325 or that line of direction, will give the place of the church, or the centre of a circle that will pass through A, B, and C.

The above angle FAE, may be had without a secant, as before, thus;

AE : R :: AF : S. AEF.1.325 90° .115 60°. 13′.

Its complement 29°. 47', will give FAE, as before.

The questions that may be proposed on this head, being innumerable, we have chosen to give only a few of the most useful.

SECTION III.

Mensuration of Areas, or the various methods of calculating the superficial content of any field.

DEFINITION.

THE area or content of any plane surface, in perches, is the number of square perches which that surface contains.

PL. 7. fig. 1.

Let ABCD represent a rectangular parallelogram, or oblong: let the side AB, or DC, contain 8 equal parts; and the side AD, or BC, three of such parts; let the line AB be moved in the direction of AD, tillithas come to EF; where AE, or BF (the distance of it from its first situation) may be equal to one of the equal parts. Here it is evident, that the generated oblong ABEF, will contain as many squares as the side AB contains equal parts, which are 8; each square having for its side one of the equal parts, into which AB, or AD, is divided. Again, let AB move on till it comes to GH, so as GE, or HF, may be equal to AE, or BF; then it is plain that the oblong AGHB, will contain twice as many squares. as the side AB contains equal parts. After the same manner it will appear, that the oblong ADCB will contain three times as many squares as the side AB contains equal parts; and in general, that every rectangular parallelogram, whether square or oblong, contains as many squares as the product of the number of equal parts in the base, multiplied into the number of the same equal parts in the height, contains units, each square having for its side one of the equal parts.

Hence arises the solution of the following problems.

PROB. I.

To find the content of a square piece of ground.

1. Multiply the base in perches, into the perpendicular in perches, the product will be the content in perches; and because 160 perches make an acre, it must thence follow, that

Any area, or content in perches, being divided by 160, will give the content in acres; the remaining perches, if more than 40, being divided by 40, will give the roods, and the last remainder, if any, will be perches.

Or thus:

2. Square the side in four-pole chains and links, and the product will be square four-pole chains and links: divide this by 10, or cut off one more than the decimals, which are five in all, from the right towards the left: the figures on the left are acres; because 10 square four-pole chains make an acre, and the remaining figures on the right, are decimal parts of an acre. Multiply the five figures to the right by 4, cutting 5 figures from the product, and if any figure be to the left of them, it is a rood, or roods; multiply the last cut off figures by 40, cutting off five, or (which is the same thing) by 4, cutting off four; and the remaining figures to the left, if any, are perches.

1. The first part is plain, from considering that a piece of ground in a square form, whose side is a perch, must contain a perch of ground; and that 40 such perches make a rood, and four roods an

acre; or which is the same thing, that 160 square perches make an acre, as before.

2. A square four-pole chain (that is, a piece of ground four poles or perches every way) must contain 160 square perches; and 160 perches make an acre, therefore 10 times 16 perches, or 10 square four-pole chains, make an acre.

Note. The chains given, or required, in any of the following problems, are supposed to be twopole chains, that chain being most commonly used; but they must be reduced to four-pole chains or perches for calculation, because the links will not operate with them as decimals.

Examplés.

PL. 1. fig. 17.

Ch. L.

Let ABCD be a square field, whose side is 14 29, required the content in acres.

> 26244 5832

160)850.3056(5. 1. 10. content.

40)50(1 rood.

10 perches.

Or thus:

Ch. L.

Ch. L.

14. 29 are equal to 7. 29 of four-pole chains, by prob. 1. sect. 1. pt. 2. 7. 29

6561 1458

5103

A.R. P.

Acres 5|31441 cont. as before 5.1.10

4

Rood 1|25764

40

Perches 10|30560

It is required to lay down a map of this piece of ground, by a scale of twenty perches to an inch.

Take 29. 16 the perches of the given side, from the small diagonal on the common surveying scale, where 20 small, or two of the large divisions, are an inch: make a square whose side is that length (by prob. 9. geom.) and it is done.

PROB. II.

To find the side of a square, whose content is given.

Extract the square root of the given content in perches, and you have the side in perches, and consequently in chains.

EXAMPLE.

It is required to lay out a square piece of ground which shall contain 12A. 3R. 16P. Required the number of chains in each side of the square; and to lay down a map of it, by a scale of 40 perches to an inch.

A. R. P.

12. 3. 16.

$$\frac{4}{51}$$
 $\frac{51}{40}$
 $\frac{Ch. L.}{2056(45.34 + \text{perches} = 22. 33\frac{1}{2} \text{ by prob. 6.}}$

85)456 [sect. 1. pt. 2.

903)3100

9064)39100 &c.

To draw the map.

From a scale where 4 of the large, or 40 of the small divisions are an inch, take 45.34, the perches of the side, of which make a square.

PROB. III.

To find the content of an oblong friece of ground.

Multiply the length by the breadth, for the content.

EXAMPLE.

PL. 1. fig. 3.

Let ABCD be an oblong piece of ground, whose length AB is $14C.\ 25L.$ and breadth $8C.\ 37L.$ required the content in acres, and also to lay down a map of it, by a scale of 20 perches to an inch.

Ch. L. Perches. 14.25=29.008.37=17.48} By prob. 4. sect. 1. pt. 2.

> 15732 3496

—— A. R. P.

160)506.9200(3. 0. 27. content.

26 perches, or near 27.

Or thus:

4 pole ch.

Ch. L. Ch. L.

 $\begin{array}{c}
 14.25 = 7.25 \\
 8.37 = 4.37
 \end{array}$

By prob. 1. sect. 1. pt. 2.

5075 2175 2900

Acres 3|16825

4

Rood |67300

4

Perches 26|9200

To draw the map.

Make an oblong (by schol. to prob. 9. geom.) whose length, from a scale of 20 to an inch, may be 29 perches, and breadth, 17.48 perches.

PROB. IV.

The content of an oblong piece of ground, and one side given, to find the other.

Divide the content in perches, by the given side in perches, the quotient is the side required in perches; and thence it may be easily reduced to chains.

EXAMPLE.

There is a ditch 14 Ch. 25 L. long, by the side of which it is required to lay out an oblong piece of ground, which shall contain 3A. 0R. 37P: what breadth must be laid off at each end of the ditch to enclose the 3A. 0R. 37P?

8

The map is constructed like the last.

PROB. V.

To find the content of a piece of ground, in form of an oblique the gular parallelogram; or of a rhombus, or rhomboides.

Multiply the base into the perpendicular height. The reason is plain from theo. 13. geom.

Example.

PL. 7. fig. 2.

Let ABCD be a piece of ground in form of a rhombus, whose base AB is 22 chains, and perpendicular DE, or FC, 20 chains. Required the content.

$$Ch.$$
 $Ch.$ $22=11.0$ $20=10.0$ 4 pole chains. Acres 11|0

Or,

$$Ch.$$
 $22=44$
 $20=40$ perches.

 $160)1760(11 \text{ acres.}$
 160

The converse of this is done by prob. 4. and the map is drawn, by laying off the perpendicular on that part of the base from whence it was taken; joining the extremity thereof to that of the base by a right line, and thence completing the parallelogram.

PROB. VI.

To find the content of a triangular piece of ground.

Multiply the base by half the perpendicular, or the perpendicular by half the base; or take half the product of the base into the perpendicular.

The reason of this is plain, from cor. 2. theo. 12. geom.

EXAMPLE.

PL. 1. fig. 16.

Let ABC be a triangular piece of ground, whose longest side or base BC, is 24C. 38L. and perpendicular AD, let fall from the opposite angle, is 13 C. 28L. Required the content.

Ch. L. Ch. L. 1. Base 24. 38 = 12. 384 pole chains. $\frac{1}{2}$ perp. 3. 39 (

> 11142 3714 3714

Acres 4 19682

Rood | 78728

Perches 31 49120 A. R. P.

Content 4. 0. 31.

```
Ch. L. Ch. L.

Perp. 13.28 = 6.78 ) four-pole chains by properchains by properchains.

Perp. 6.39 = 3.39 ) prob. 1. sect. 1. pt. 2.

Or 2dly. Perp. 6.78 of four-pole chains.

Perp. 6.78

4068

4068

A. R. P.

4|19682 = 4. 0. 31.

Or 3dly. Base 12.38 four-pole chains.

Perp. 6.78

9904

8666

7428
```

 $\frac{83.9364}{A} = \frac{A \cdot R \cdot P}{4|19682} = 4 \cdot 0 \cdot 31.$

Or the base and perpendicular may be reduced to perches; and the content may be thence obtained, thus:

```
Ch. L. Perches.
Perp. 13.28 = 27.12
                      By prob. 4. sect. 1. pt. 2...
Half the perp. 13.56
       Perches. Ch. L.
1: Base 49.52 = 24.38
½ perp. 13.56
       29712
      24760
     14856
     4952
                   R. P.
 160)671.4912(4. 0. 31.
        31
         Perches.
2. Perp. 27.12
Half base 24.76
         16272
        18984
       10848
       5424
       671.4912 = 4. 0.
                           31.
```

But, square perches may be reduced to acres, &c. rather more commodiously, by dividing by 40 and 4, than by 160; thus,

4|0)67|1.

4)16. 31

A. 4. 0. 31

Perches.

3. Base 49.52
Perp. 27.12

9904
4952
34664

9904

 $\frac{1342.9824}{671.4912 = 4.} A. R. P.$

The map may be readily drawn, having the distance from either end of the base, to the perpendicular given; as may be evident from the figure.

PROB. VII.

The content of a triangular piece of ground, and the base given, to find the perpendicular.

Divide the content in perches, by half the base in perches; and the quotient will give you the perpendicular, in perches and so in chains.

EXAMPLES.

PL. 1. fig. 16.

Let BC be a ditch, whose length is 24C. 40L. by which it is required to lay out a triangular piece of ground, whose content shall be 4A. 1R. 10P. Required the perpendicular.

Ch. L. Perches. Base 24.40 = 49.6Half the base = 24.8

A. R. P.
4. 1. 10.
4

17
40
Perches.
24.8)690(27.28

1940

2040

560

64

Perches. Ch. L. Answer perp. 27. 28. = 13.45.

This perpendicular being laid on any part of the base, and lines run from its extremity to the ends of the base, will lay out the triangle (by cor. to theo. 13. geom.) so that the perpendicular may be set on that part of the base which is most convenient and agreeable to the parties concerned.

LEMMA.

PL. 8. fig. 9.

If from half the sum of the sides of any plane triangle ABC, each particular side be taken; and if the half sum, and the three remainders be multiplied continually into each other, the square roof of this product will be the area of the triangle.

Bisect any two of the angles, as A and B, with the lines AB, BD meeting in D; draw the perpendiculars DE, DF, DG.

In the same way if A and C were bisected, the same point D would be had; therefore a line from D to C will bisect C, and thus the triangles DFC, DGC will be also equal.

Produce CA to H, till AH=EB or GB; so will HC be equal to half the sum of the sides, vis. to $\frac{1}{2}AB$, $+\frac{1}{4}AC+\frac{1}{2}BC$; for FC, FA, EB, are severally equal to CG, AE, BG; and all these together are equal to the sum of the sides of the triangle; therefore FC + FA + EB or CH, are equal to half the sum of the sides.

FC=CH-AB, for AF=AE, and HA=EB; therefore HF=AB; and AF=CH-BC; for CF

=CG, and AH=GB; therefore BC=HA+FC, and AH=CH-AH.

Continue DC, till it meets a perpendicular drawn upon H in K; and from K draw the perpendicular KI, and join AK.

Because the angles AHK and AIK are two right ones, the angles HIA and K together, are equal to two right; since the angles of the two triangles contain four right: in the same way FDE + FAE = (2 right angles =) FAE + IAH; let FAE be taken from both, then FDE = IAH, and of course FAE = K; the quadrilateral figures AFDE, and KHAI, are therefore similar, and have the sides about the equal angles proportional; and it is plain the triangles CFD and CHK are also proportional: hence,

FD: HA:: FA: HK FD: FC:: HK: HC

Wherefore by multiplying the extreme, and means in both, it will be the square of $FD \times HK \times HC = FC \times FA \times HA \times HK$; let HK be taken from both, and multiply each side by CH; then the square of $CH \times$ by the square of $FD = FC \times FA \times HA \times CH$.

It is plain, by the foregoing problem, that $\frac{1}{2}AB \times DE$, $+\frac{1}{2}BC \times DG + \frac{1}{2}AC \times FD =$ the area of the triangle; or that half the sum of the sides, vis. $CH \times FD =$ the triangle; wherefore the square of $CH \times$ by the square of $FD = FC \times FA \times HA \times CH$, that is, the half sum multiplied continually into the differences between the half sum and each side, will be the square of the area of the triangle, and its root the area. Q. E. D.

Hence the following problem will be evident.

PROB. VIII.

The three sides of a plane triangle given to find the area.

RULE.

From half the sum of the three sides subtract each side severally; take the logarithms of half the sum and three remainders, and half their total will be the logarithm of the area: or, take the square root of the continued product of the half sum and three remainders for the area.

Examples.

Ps. 8. fig. 9.

1. In the triangle ABC, are

Given,
$$\begin{cases} AB=10.64 \\ AC=12.28 \\ CB=9.00 \end{cases}$$
 four-pole chains; required the area?

Sum 31.92

Half sum	15.96	Log.	1.203033
(5.32	_	0.725912
Remainders {	3.68	-	0.565848
(6.96		0.842609

2)3.337402

Answer, Sqr. Ch. 46.63 Log. 1.668701 or, 4.663 Acres.

Or, $15.96 \times 5.32 \times 3.68 \times 6.96 = 2174.71113216$;

To find the Content of Ground.

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the square root of which is 46.63, for the area as before.

2. What quantity of land is contained in a triangle, the 3 sides of which are, 80, 120 and 160 perches respectively? Answer, 29A. 7P.

PROB. IX.

Two sides of a plane-triangle and their included angle given, to find the area.

RULE

To the log. sine of the given angle (or of its supplement to 180°, if obtuse) add the logarithms of the containing sides; the sum, less radius, will be the logarithm of the double area.

EXAMPLES.

PL. 5. fig. 16.

Suppose two sides, AB, AC, of a triangular lot ABC, form an angle of 30 degrees, and measure one 64 perches, and the other 40.5, what must the content be?

· 1	160)648	(4A.	8P. answer.
5	2)1296.	log.	3.112605
Containing sides	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	log.	1.806180
Given angle			9.698970

- 2: Required the area of a triangle, two sides of which are 49.2 and 40.8 perches, and their contained angle 1444 degrees? Answer, 3A. 2R. 22P.
- 3. What quantity of ground is inclosed in an equilateral triangle, each side of which is 100 perches, either angle being 60 degrees? Answer, 27A. 10P.

Demonstration of this problem.

PL. 11. fig. 3.

Let AH be perpendicular to AB and equal to AC, and HE, FCG, parallel to AB; then making AH (= AC) radius, AF (= CD) will be the sine of CAD, and the parallelograms ABEH (the product of the given sides,) and ABGF the double area of the triangle) having the same base AB, are in proportion as their heights AH, AF; that is, as radius to the sine of the given angle; which proportion gives the operation as in the rule above.

PROB. X.

To find the area of a trapezoid, viz. a figure bounded by four right lines, two of which are parallel, but unequal.

Rule.

Multiply the sum of the parallel sides by their perpendicular distance, and take half the product for the area.

Note. On this 10th problem are founded most of the calculations of differences by latitude and departure, and those by offsets, following in this treatise.

Ff

EXAMPLES.

1. Required the area of a trapezoid, of which the parallel sides are, respectively, 30 and 49 perches, and their perpendicular distance 61.6?

$$30+49 = \frac{61.6}{79.}$$
 Multiply.

2)4866.4

Answer, 2433.2=15A. 33.2P.

P4. 2. Ag. 10.

2. In the trapezoid ABCD the parallel sides are, AD, 20 perches, BC, 32, and their perpendicular distance, AB, 26; required the content?

Answer, 4A. 36P.

PROB. XI.

To find the Content of a trapezium.

RULE.

Multiply the diagonal, or line joining the remotest opposite angles, by the sum of the two perpendiculars falling from the other angles to that diagonal, and half the product will be the area.

EXAMPLE.

PL. 7. fig. 3.

Let ABCD be a field in form of a trapezium, the diagonal AC 64.4 perches, the perpendicular Bb 13.6 and Dd 27.2, required the content?

Diagonal = 64.4 Multiply. 13.64+27.2 = 40.8

2)2627.52

160)131376(8A. 33‡P. Answer. 1280

33‡ perches.

Note. The method of multiplying together the half sums of the opposite sides of a trapezium for the content is erroneous, and the more so the more oblique its angles are.

To draw the map set off Ab 28 perches, and Ad 34.4, and there make the perpendiculars to their proper lengths, and join their extremities to those of the diagonal.

PROB. XII.

To find the area of a circle, or an ellipsis.

RULE.

Multiply the square of the circle's diameter, or the product of the longest and shortest diameters of the ellipsis by .7854 for the area. Or, subtract 0.104909 from the double logarithm of the circle's diameter, or from the sum of the logarithms of those elliptic diameters, and the remainder will be the logarithm of the area.

Note. In any circle, the Diam. multi. by 3.14159, produces the Cir. Circum. div. by 3.14159, quotes the diam.

EXAMPLES.

1. How many acres are in a circle of a mile diameter?

1 Mile=320 per. $\log. 2.505150$

2.505150

5.010300

0.104909

4|0)8042|5. log. 4

4.905391

4)2010.25

Answer, 502A. 2R. 25P.

2. A gentleman, knowing that the area of a circle is greater than that of any other figure of equal perimeter, walls in a circular deer park of 100 perches diameter, in which he makes an elliptical fish pond 10 perches long by 5 wide; required the length of his wall, content of his park, and area of his pond?

Answer, the wall 314.16 perches inclosing 49A. 14P. of which $39\frac{1}{4}$ perches, or $\frac{1}{4}$ of an acre nearly, is appropriated to the pond.

PROB. XIII.

The area of a circle given, to find its diameter.

Rule.

To the logarithm of the area add 0.104909, and half the sum will be the logarithm of the diameter. Or, divide the area by .7854, and the square-root of the quotient will be the diameter.

EXAMPLES.

A horse in the midst of a meadow suppose, Made fast to a stake by a line from his nose. How long must this line be, that feeding all round,

Permits him to graze just an acre of ground?

Area in perches 160 log. 2.204120 0.104909 2)2.309029

Diameter, 14.2733 .log. 1.154514

Answer, 7.13665 per. = 117F.9 In.

PROB. XIV.

Allowance for roads.

It is customary to deduct 6 acres out of 106 for roads; the land before the deduction is made may be termed the gross, and that remaining after such deduction, the neat.

RULE.

The gross div. } by 1.06, { quotes the neat. prod. the gross.

Examples.

1. How much land must I inclose to have 850A. 2R. 20P. neat?

202

40|20. 4| 2.5 —— Acres. A. R. P. 850.625×1.06=901.6625=901.2.26. the ans.

2. How much neat land is there in a tract of 901A. 2R. 26P. gross?

Note. These two operations prove each other.

PROB. XV.

To find the area of a piece of ground be it ever so irregular by dividing it into triangles and trapezia.

P'L. 7. fig. 4.

We here admit the survey to be taken and protracted; by having therefore the map, and knowing the scale by which it was laid down, the content may be thus obtained.

Dispose the given map into triangles, by fine pencilled lines, such as are here represented in the scheme, and number the triangles with 1, 2, 3, 4, &c. Your map being thus prepared, rule a table with four columns; the first of which is for the number of the triangle, the second for the base of it, the third for the perpendicular, and the fourth for the content in perches.

Then proceed to measure the base of number 1, from the scale of perches the map was laid down, and place that in the second column of the table, under the word base; and from the angle opposite to the base, open your compasses so, as when one foot is in the angular point, the other being moved backwards and forwards, may just touch the base line, and neither go the least above or beneath it; that distance in the compasses measured from the same scale, is the length of that perpendicular, which place in the third column, under the word perpendicular.

If the perpendiculars of two triangles fall on one and the same base, it is unnecessary to put down the base twice, but insert the second perpendicular opposite to the number of the triangles in the table, and join it with the other perpendicular by a brace, as No. 1 & 2, 4 & 5, 6 & 7, 9 & 10, &c.

Proceed after this manner, till you have measured all the triangles; and then by prob. 6. find the content in perches of each respective triangle, which severally place in the table opposite to the number of the triangle, in the fourth column, under the word content.

But where two perpendiculars are joined together in the table, by a brace having both one and the same base; find the content of each (being a trapezium) in perches, by prob. 11. which place opposite the middle of those perpendiculars, in the fourth column, under the word content.

Having thus obtained the content of each respective triangle and trapezium, which the map contains, add them all together, and their sum will

be the content of the map in perches; which being divided by 160, gives the content in acres. Thus, for

EXAMPLES.

ľ	No.	Ease.	Perpend:	Content.	
-	1	24.8	17.0	412.92	
I	2		16.3	412.52	
	3	28.2	16.0	225.6	
	4	39.8	19.6)	710.40	
	5		16.2	712.42	
	6	49.4	29.0	1006.0	
I	7		15.0	1086.8	
I	8	38.7	6.7	129.64	
	9	40.0	17.0)	600.	
Ì	10	-	13.0	000.	
	11	42.8	10.2)	4015	
ļ	12		12.3 \$	481.5	
	13	26.2	17.9	234.49	
	14	24.0	11.6)	259.2	
l	15		10.0	209.2	
	Content in perches 4142.57				

This being divided by 160, will give 25A. 3R. 22P. the content of the map.

Let your map be laid down by the largest scale your paper will admit, for then the bases and perpendiculars can be measured with greater accuracy than when laid down by a smaller scale, and if possible measure from scales divided diagonally.

If the bases and perpendiculars were measured by four-pole chains, the content of every triangle and trapezium, may be had as before, in problems 6. and 11. and consequently the whole content of the map.

If any part of your map has short or crooked bounds, as those represented in plate 7. fig. 5. then by the straight edge of a transparent horn, draw a fine pencilled line as AB to balance the parts taken and left out, as also another, BC: these parts when small, may be balanced very nearly by the eye, or they may be more accurately balanced by method the third. Join the points A and C by a line, so will the content of the triangle ABC, be equal to that contained between the line AC, and the crooked boundary from A to B, and to C: by this method the number of triangles will be greatly lessened, and the content become more certain; for the fewer operations you have, the less subject will you be to err: and if an error be committed, the sooner it may be discovered.

The lines of the map should be drawn small, and neat, as well as the bases; the compasses neatly pointed, and scale accurately divided; without all which you may err greatly. The multiplications should be run over twice at least, as also the addition of the column content.

From what has been said, it will be easy to survey a field, by reducing it into triangles, and measuring the bases and perpendiculars by the chain. To ascertain the content only, it is not material to know at what part of the base the perpendicular was taken: since it has been shewn (in cor. to theo. 13. geom.) that triangles on the same base, and between the same parallels, are equal; but if you would draw a map from the bases and perpen-

diculars, it is evident that you must know at what part of the base the perpendicular was taken, in order to set it off in its due position; and hence the map is easily constructed.

PROB. XVI.

To determine the area of a friece of ground, having the man given, by reducing it to one triangle equal thereto, and thence finding its content.

PL. 8. fig. 5.

Let A B C D E F G H be a map of ground, which you would reduce to one triangle equal thereto.

Produce any line of the map, as AH, both ways, lay the edge of a parallel ruler, from A to C, having B above it; hold the other side of the ruler, or that next you, fast; open till the same edge touches B, and by it, with a protracting pin, mark the point b, on the produced line, lay the edge of the ruler from b to D, having C above it, hold the other side fast, open till the same edge touches C, and by it mark the point c, on the produced line. A line drawn from c to D will take in as much as it leaves out of the map.

Again lay the edge of the ruler from H to F, having G above it, keep the other side fast, open till the same edge touches G, and by it mark the point g, on the produced line; lay the edge of the ruler from g to E, having F above it, keep the other side fast, open till the same edge touches F, and by it mark the point f, on the produced line. Lay the edge of the ruler from f to D, having E

above it, keep the other side fast, open till the same edge touches E, and by it mark the point e, on the produced line. A line drawn from D to e, will take in as much as it leaves out. Thus have you the triangle c D e, equal to the irregular polygon A B C D E F G H.

If when the ruler's edge be applied to the points A and C, the point B falls under the ruler, hold that side next the said points fast, and draw back the other to any convenient distance; then hold this last side fast, and draw back the former edge to B, and by it mark b, on the produced line; and thus a parallel may be drawn to any point under the ruler, as well as if it were above it. It is best to keep the point of your protracting pin in the last point in the extended line, till you lay the edge of the ruler from it to the next station, or you may mistake one point for another.

This may also be performed with a scale, or ruler, which has a thin sloped edge, called a fiducial edge; and a fine pointed pair of compasses. Thus,

Lay that edge on the points A and C, take the distance from the point B to the edge of the scale, so that it may only touch it, in the same manner as you take the perpendicular of a triangle; carry that distance down by the edge of the scale parallel to it, to b; and there describe an arc on the point b; and if it just touches the ruler's edge, the point b is in the true place of the extended line. Lay then the fiducial edge of the scale from b to D, and take a distance from C, that will just touch the edge of the scale; carry that distance along the edge, till the point which was in C, cuts the produced line in c; keep that foot in c, and

describe an arc, and if it just touches the ruler's edge, the point c is in the true place of the extended line. Draw a line from c to D, and it will take in and leave out equally: in like manner the other side of the figure may be balanced by the line c D.

Let the point of your compasses be kept to the last point of the extended line, till you lay your scale from it to the next station, to prevent mistakes from the number of points.

That the triangle c D c, is equal to the right-lined figure ABCDEFGH, will be evident from problems 18. 19. geom. for thereby, if a line were drawn from b to C, it will give and take equally, and then the figure b C D E F G H, will be equal to the map. Thus the figure is lessened by one side, and by the pext balance line will lessen it by two, and so on, and will give and take equally. In the same manner an equality will arise on the other side.

The area of the triangle is easily obtained, as before, and thus you have the area of the map.

It is best to extend one of the shortest lines of the polygon, because if a very long line be produced, the triangle will have one angle very obtuse, and consequently the other two very acute; in which case it will not be easy to determine exactly the length of the longest side, or the points where the balancing lines cut the extended one.

This method will be found very useful and ready in small enclosures, as well as very exact; it may be also used in large ones, but great care must be taken of the points on the extended line, which will be crowded, as well as of not missing a station.

PROB. XVII.

A map with its area being given, and its scale omitted to be either drawn or mentioned; to find the scale.

OAST up the map by any scale whatsoever, and it will be.

As the area found

Is to the square of the scale by which you cast up, :: The given area of the map

To the square of the scale by which it was laid down.

The square root of which will give the scale.

EXAMPLE.

A map whose area is 126Å. 3R. 16P. being given; and the scale omitted to be either drawn or mentioned; to find the scale.

Suppose this map was cast up by a scale of 20 perches to an inch, and the content thereby produced be 31A. 2R. 34P.

As the area found, 31A. 2R. 34P.=5074P.

Is to the square of the scale by which it was cast up, that is to $20 \times 20 = 400$,

:: The given area of the map 126A. 3R. 16P. = 20296P.

To the square of the scale by which it was laid down.

5074:400: 20296: 1600 the square of the required scale.

Root.

1600(40

16

8(00

Answer. The map was laid down by a scale of 40 perches to an inch.

PROB. XVIII.

How to find the true content of a survey, though it be taken by a chain that is too long or too short.

Let the map be constructed, and its area found as if the chain were of the true length. And it will be,

As the square of the true chain
Is to the content of the map,
: The square of the chain you surveyed by
To the true content of the map.

EXAMPLE.

If a survey be taken with a chain which is 3 inches too long; or with one whose length is 42 feet 3 inches, and the map thereof be found to contain 920A. 2R. 20P. Required the true content.

As the square of 42F. 0In.=the square of 504 inches=254016.

Is to the content of the map 920A. 1R. 20P. = 147260P.

: The square of 42F. 3In. = the square of 507 inches = 257049.

To the true content.

......

P. P. 250416: 147260:: 257049: 149019 A. R. P.

160(149019(931. 1. 19 Answer.

501

219

40)59(1R.

19P.

METHOD OF DETERMINING' THE AREAS OF RIGHT-LINED FIGURES UNIVERSALLY, OR BY CALCULATION.

DEFINITIONS.

PL. 8. fig. 7.

- 1. MERIDIANS are north and south lines, which are supposed to pass through every station of the survey.
- 2. The difference of latitude, or the northing or southing of any stationary line, is the distance that one end of the line is north or south from the other end; or it is the distance which is intercepted on the meridian, between the beginning of the stationary line and a perpendicular drawn from the other end to that meridian. Thus, if N. S. be a meridian line passing through the point A of the line AB, then is Ab the difference of latitude or southing of that line,
- 3. The departure of any stationary line, is the nearest distance from one end of the line to a meridian passing through the other end. Thus Bb is the departure or easting of the line AB: but if CB be a meridian, and the measure of the stationary distance be taken from B to A; then is BC the difference of latitude, or northing, and AC the departure or westing of the line BA.

63,₃

- 4. That meridian which passes through the first station, is sometimes called the first meridian; and sometimes it is a meridian passing on the east or west side of the map, at the distance of the breadth thereof, from east to west, set off from the first station.
- 5. The meridian distance of any station is the distance thereof from the first meridian, whether it be supposed to pass through the first station, or on the east or west side of the map.

THEO. I.

In every survey which is truly taken, the sum of the northings will be equal to that of the southings; and the sum of the eastings equal to that of the westings.

PL. 9. fig. 1.

Let a, b, c, e, f, g, h, represent a plot or parcel of land. Let a be the first station, b the second, c the third, &c. Let NS be a meridian line, then will all lines parallel thereto, which pass through the several stations, be meridians also; as ao, bs, cd, &c. and the lines bo, cs, de, &c. perpendicular to those, will be the east or west lines, or departures.

The northings, ei+go+hq=ao+bs+cd+fr the southings: for let the figure be completed; then it is plain that go+hq+rk=ao+bs+cd, and ei-rk=fr. If to the former part of this first equation ei-rk be added, and fr to the latter, then go+hq+ei=ao+bs+cd+fr; that is, the sum of the northings is equal to that of the southings.

Hh

The eastings cs+qa=ob+de+if+rg+oh, the westings. For aq+yo(az)=de+if+rg+oh, and bo=cs-yo. If to the former part of this first equation, cs-yo be added, and bo to the latter, then cs+aq=ob+de+if+rg+oh; that is, the sum of the eastings is equal to that of the westings. Q. E. D.

SCHOLIUM.

This theorem is of use to prove whether the field-work be truly taken, or not; for if the sum of the northings be equal to that of the southings, and the sum of the eastings to that of the westings, the field-work is right, otherwise not.

Since the proof and certainty of a survey depend on this truth, it will be necessary to shew how the difference of latitude and departure for any stationary line, whose course and distance are given, may be obtained by the table, usually called the Traverse Table.

To find the difference of Latitude and departure, by the Traverse Table.

This table is so contrived, that by finding therein the given course, and a distance not exceeding 120 miles, chains, perches, or feet, the difference of latitude and departure is had by inspection: the course is to be found at the top of the table when under 45 degrees; but at the bottom of the table when above 45 degrees. Each column signed with a course consists of two parts, one for the

difference of latitude, marked Lat. the other for the departure, marked Dep. which names are both at the top and bottom of these columns. The distance is to be found in the column marked Dist. next the left hand margin of the page.

Example.

In the use of this table, a few observations only are necessary.

- 1. If a station consist of any number of even chains or perches (which are almost the only measures used in surveying) the latitude and departure are found at sight under the bearing or course, if less than 45 degrees; or over it if more, and in a line with the distance.
- 2. If a station consist of any number of chains and perches, and decimals of a chain or perch, under the distance 10, the lat. and dep. will be found as above, either over or under the bearing; the decimal point or separatrix being removed one figure to the left, which leaves a figure to the right to spare.

If the distance be any number of chains or perches, and the decimals of a chain or perch, the lat and dep. must be taken out at two or more operations, by taking out the lat and dep. for the chains or perches in the first place; and then for the decimal parts.

To save the repeated trouble of additions, a judicious surveyor will always limit his stations to whole chains, or perches and lengths, which can commonly be done at every station, save the last.

1. In order to illustrate the foregoing observations, let us suppose a course or bearing, to be S. 35°. 15' E. and the distance 79 four-pole chains. Under 35°. 15', or 35½ degrees; and opposite 79, we find 64. 52 for the latitude, and 45. 59 the departure, which signify that the end of that station differ in latitude from the beginning 64. 52 chains, and in departure 45. 59 chains.

Note. We are to understand the same things if the distance is given in perches or any other measures, the method of proceeding being exactly the same in every case.

Again, let the bearing be 54[‡] degrees and distance as before; then over said degrees we find the same numbers, only with this difference, that the lat. before found, will now be the dep. and the dep. the lat. because 54[‡] is the complement of 35[‡] degrees to 90, vis. lat. 45. 59. dep. 64. 52.

2. Suppose the same course, but the distance 7 chains 90 links, or as many perches. Here we find the same numbers, but the decimal point must be removed one figure to the left.

Thus, under 35¹, and in a line with 79 or 7.9, are

Lat. 6. 45 Dep. 4. 56

the 5 in the dep. being increased by 1, because the 9 is rejected; but over 544 we get

Lat. 4. 56 Dep. 6. 45 3. Let the course be as before, but the distance 7.79, then opposite

Dep. 4. 43	Lat. 6. 29 7	7. 70 9
		
4. 49	6. 36	7. 79

Or opposite

7. 00 . 79	Lat. 5. 72 . 64	Dep. 4. 03 . 46
	**************************************	•
7. 79	6. 36	4. 49

THEO. II.

When the first meridian passes through the map.

If the east meridian distances in the middle of each line be multiplied into the particular southing, and the west meridian distances into the particular northing, the sum of these products will be the area of the map.

PL. 10. fig. 1.

Let the figure abkm be a map, the lines, ab bk to the southward, and km ma to the northward, NS the first meridian line passing through the first station a.

The meridian
$$\begin{cases} zd \times ao \\ tu \times ox(by) \end{cases} = Area \begin{cases} am \\ ow \end{cases}$$
The meridian $\begin{cases} ef \times gx \\ hh \times ga(my) \end{cases} = Area \begin{cases} xp \\ gl \end{cases}$

These four areas am+ow+xp+gl will be the area of the whole figure *cmsniprlc*, which is equal to the area of the map abkm. Complete the

figure.

The parallelograms am and ow, are made of the east meridian distances ds and tu, multiplied into the southings ao and ox. The parallelograms xp and gl are composed of the west meridian distances of and hh, multiplied into the northings xg and ga (my) but these four parallelograms are equal to the area of the map; for if from them be taken the four triangles marked Z, and in the place of those be substituted the four triangles marked O, which are equal to the former; then it is plain the area of the map will be equal to the four parallelograms. Q. E. D.

THEO. III.

If the meridian distance when east, be multiplied into the southings, and the meridian distance when west be multiplied into the northings, the sum of these less by the meridian distance when west, multiplied into the southings, is the area of the survey.

PL. 10. fig. 2.

Let ab c be the map.

The figure being completed, the rectangle af is made of the meridian distance eq when east, multiplied into the southing an; the rectangle yk is made of the meridian distance xw, multiplied into the northings cz or ya. These two rectangles, or parallelograms, af+yk, make the area of the figure dfnyikd, from which taking the rectangle oy, made of the meridian distance tu when west, into the southings oh or bm, the remainder is the area of the figure dfokikd, which is equal to the area of the map.

Let bou = Y, urih = L, ric = O, wrc = Z = akw = K, and efb = B, ade = A. I say, that Y+Z+B=K+L+A.

Y=L+O, add Z to both, then Y+Z=L+O+Z; but Z+O=K, put K instead of Z+O; then Y+Z=L+K, add to both sides the equal triangles B and A, then Y+Z+B=L+K+A. If therefore B+Y+Z be taken from abc, and in lieu thereof we put L+K+A, we shall have the figure dfohikd=abc, but that figure is made up of the meridian distance when east, multiplied into the southing, and the meridian distance, when west, multiplied into the northing less by the meridian distance, when west, multiplied into the southing. Q. E. D.

COROLLARY.

Since the meridian distance (when west) multiplied into the southing, is to be subtracted, by the same reasoning the meridian distance when east, multiplied into the northing, must be also subtracted.

SCHOLIUM.

From the two preceding theorems we learn how to find the area of the map, when the first meridian passes through it; that is, when one part of the map lies on the east and the other on the west side of that meridian. Thus,

RULE.

The merid. } east {multiplied {southings}}
Dist. when I west { into the {northings}}
their sum is the area of the map.

But,

The merid. {east } multiplied {northings}
Dist. when {west } into the {southings}
the sum of these products taken from the former
gives the area of the map.

These theorems are true, when the surveyor keeps the land he surveys, on his right hand, which we suppose through the whole to be done; but if he goes the contrary way, call the southings northings, and the northings southings, and the same rule will hold good.

General Rule for finding the Meridian distances.

- 1. The meridian distance and departure, both east, or both west, their sum is the meridian distance of the same name.
- 2. The meridian distance and departure of different names; that is, one east and the other west, their difference is the meridian distance of the same name with the greater.

Thus in the first method of finding the area, as in the following field-book.

The first departure is put opposite the northing or southing of the first station, and is the first meridian distance of the same name. Thus if the first departure be east, the first meridian distance will be the same as the departure, and east also; and if west, it will be the same way.

The first meridian distance The next departure	6.61 E. 6.61 E.
The second meridian distance The next departure	13.22 E. 1.80 E,
The third meridian distance	15.02 E.

At station 5, the meridian distance	5.78 E.
The next departure	7.76 W.
The next meridian distance	1,98 W.
At station 11, the meridian distance	0.12 W.
The next departure	5.84 E.
The next meridian distance	5.72 E.

PL. 10. fig. 3.

In the 5th and 11th stations, the meridian distance being less than the departures, and of a contrary name, the map will cross the first meridian, and will pass as in the 5th line, from the east to the west line of the meridian; and in the 11th line it will again cross from the east to the west side, which will evidently appear, if the field-work be protracted, and the meridian line passing through the first station, be drawn through the map.

The field-book cast up by the first method, will be evident from the two foregoing theorems, and therefore requires no further explanation; but to find the area, by the second method, take this

RULE

When the meridian distances are east, put the products of north and south areas in their proper columns; but when west, in their contrary columns; that is, in the column of south area, when the difference of latitude is north; and in north when south: the reason of which is plain, from the two last theorems. The difference of these two columns will be the area of the map.

,	·					
No St.	I PACHTINUM	C.L.	Lat. and half Dep	_	Area.	Deduct.
1	NE 75	13.70	N 3.54 E 6.61	6.61 E 13.22 E		23.3994
2	NE 201	10.30	1	15.02 F 16.82 E		144.9430
3	East	16.20		2 4.92 E 33.02 E	T.	
4	SW 333	35.30	S 29.44 W 9.74	23.28 E :3.54 E	68 <i>5</i> .3632	
5	SW 76	16.00	S 3.87 W 7.76		I TO VEUE	
6	North	9.00	N 9.00 0.00	1.98 W 1.98 W	1 17 99AA	•
7	SW 84	11.60	S 1.21 W 5.77	7.75 W 13.52 W		9.3775
8	NW 53į	11.60		18.16 W 22.80 W	1198 N9N4 I	
9	NE 364			1.06 W	262.3828	
10	NE 223	14.00	N 12.93 E 2.68	8.64 W 5.96 W	111.7152	
11	SE 763	12.00	S 2.75 E 5.84	0.12 W 572 E		0.3300
12	SW 15	111 X & 1	S 10.48 W 1.40	4.32 E 2.92 E	45.2736	
13	SW 164		S 9.69 W 1.46	1.46 E 0.00	14.1474	
1285.1012 178.0499						78.0499
	Content in Chains, 1107.0513					

The foregoing Field-Book, Method II. 243

As is needless here to insert the columns of bearing or distances, in chains, they being the same as before.

No.	Lat	and	Merid.	N. Area.	S. Area
St.	half	Dep.	Dist.	IV. AICA.	o. Area,
1	N E	o.54 6.61	6.61 E 13.22 E	4 4 4 4 4 4	
2	N E	1	15.02 E 16.82 E	1144.9430	
3	E		24.92 E 33.02 E	3	
4	S W		23.28 E 13.54 E		685.3532
5	S W	3.87 7.76	5.78 E 1.98W		22.3686
6	N	9.00 0. 0 0			17.8200
7	S W	1.21 5.77	7.75 W 13.52 W	9.3775	
•	N W		18.16W 22.80W		126.0303
9	N E	1	17.06W 11.32W		262.3828
10	E	2.93 2.6 8	8.64W 5.96W		111.7152
. 11	S E S	2.75 5.84	0.12W 5.72 E	0.3300	
12	W	0.48	4.32 E 2.92 E		45.2736
	S W	9.69 1.46	1.46 E 0,00		14.1474
				178.0499	284.1012
					178 0499
Aı	rea in	chair	s, as befo	ore,	1107.0513

Construction of the Map from either the 1st or the 2d Table?

PL. 10. Ag. 3.

Draw the line NS for a north and south line, which call the first meridian; in this, line assume any point, as 1, for the first station. Set the northing of that stationary line, which is 3.54, from 1 to 2, on the said meridian line. Upon the point 2 raise a perpendicular to the eastward, the meridian distance being easterly, and upon it set 13.22, the second number in the column of meridian distance from 2 to 2, and draw the line 1 2, for the first distance line: from 2 upon the first meridian, set the northing of the second stationary line, that is, 9.65 to 3, and on the point 3 erect a perpendicular eastward, upon which let the meridian distance of the second station 16.82, from 3 to 3, and draw the line 2 3, for the distance line of the se-And since the third station has neicond station. ther northing nor southing, set the meridian distance of it 33.02, from 3 to 4, for the distance line of the third station. To the fourth station there is 29.44, southing, which set from 3 to 5; upon the point 5, erect the perpendicular 5 5; on which lay 13,54, and draw the line 4 to 5.

In the like manner proceed to set the northings and southings on the first meridian, and the meridian distances upon the perpendiculars raised to the east or west; the extremities of which connected by right lines, will complete the map.

A Specimen of the Pennsylvania Method of CALCULATION; which, for its Simplicity and Ease, in finding the Meridian Distances, is supposed to be preferable in Practice to any Thing here to fore published on the Subject.

IND in the first place, by the Traverse Table, the lat. and dep. for the several courses and distances, as already taught; and if the survey be

truly taken, the sums of the northings and southings will be equal, and also those of the eastings and westings. Then, in the next place, find the meridian distances, by choosing such a place in the column of eastings or westings, as will admit of a continual addition of one, and subtraction of the other; by which means we avoid the inconvenience of changing the denomination of either of the departures.

The learner must not expect that in real practice the columns of lat. and those of dep. will exactly balance when they are at first added up, for little inaccuracies will arise, both from the observations taken in the field, and in chaining; which to adjust, previous to finding the meridian distances, we may observe, That if, in small surveys, the difference amount to two-tenths of a perch for every station, there must have been some error committed in the field; and the best way in this case, will be to rectify it on the ground by a re-survey, or at least as much as will discover the error. But when the differences are within those limits, the columns of northing, southing, easting, and westing, may be corrected as follows:

Add all the distances into one sum, and say, as that sum is to each particular distance, so is the difference between the sums of the columns of northing and southing to the correction of northing or southing belonging to that distance: the corrections thus found are respectively additive, when they belong to the column of northing or southing, which is the less of the two, and subtractive when they belong to the greater; if the course be due east or west, the correction is always additive to the less of the two columns of northing or southing. The corrections of easting and westing are found exactly in the same manner.

This rule was investigated two different ways, by N. Bowditch, Author of the Practical Navigator, and R. Adrain, Prof. Math. and N. Phil. Columbia Col. N. York, as may be seen in the Analyst No. IV. published in 1808.

The following example will sufficiently illustrate the manner of applying the rule.

In this example the sum of the distances is 791, and the difference between the columns of northing and southing, is .4, also the first distance is 70; say then,

which fourth proportional .04 is the first correction belonging to the southing 53.6, from which the correction .04 should be subtracted.

In this manner the several corrections of the southings

But as only two of these corrections amount to half a tenth, we must use .1 for each of the corrections .09 and .07, and neglect the correction ,04; thus the correct southings become

In like manner from the remaining distances we obtain to

the northings
$$101.1$$
 the additive corrections .06 54.0 00.0 the additive corrections .06 00.0

And consequently, by neglecting .04, and .03, and using .1 for each of the two .06 and .07, the northings

when corrected are 101.2 54.0 60.1

In obtaining these corrections, it is commonly unnecessary to use all the significant figures of the distances: thus, for the ratio of 791 to 70, we may say, as 80 to 7.

			, —	-Diff.		11.4	Diff.			
					257.0	0.812				
257.1		218.2 1257.1	218.2	257.0	257.2	218.4	218.0			
130.0			00.1	130.0				130	West.	7
19.2		1356		19.1		1357		187	S. 8 W.	6
	183.6	29.0		·	183.7	29.1.		- 186	S. 81 E.	5
			54.0				54.0	2	North.	4
·	73.5		101.2		73.5		101.1	125	N. 36 E.	ده
62.9			62.9	62.9			62.9	89	N. 45 W.	22
•5.0		53.6		45.0		53.6		70	S. 40° W.	-
.	ដែ	ŝ	Z	₩.	়	ŵ	Z.	Per.	No. Courses.	o.
	cted.	Corrected		Ş	From the Tables.	om the	F.	3.	Field-Notes.	

EXAMPLE OF CORRECTING A SURVEY

The latitudes and departures being thus balance ed, proceed to insert the meridian distances by the above method, where we still make use of the same field notes, only changing chains and links into perches and tenths of a perch. Then by looking along the column of departure, it is easy to observe, that in the columns of easting, opposite station 9, all the eastings may be added, and the westings subtracted, without altering the denomination of either. Therefore by placing 46.0, the east departure belonging to this station in the column of meridian distances, and proceeding to add the eastings and subtract the westings, according to the rule already mentioned, we shall find that at station 8, these distances will end in 0, 0, or a cypher, if the additions and subtractions be rightly made. Then multiplying the upper meridian distance of each station by its respective northing or southing, the product will give the north or south area, as in the examples already insisted on, and which is fully exemplified in the annexed specimen. When these products are all made out, and placed in their respective columns, their difference will give double the area of the plot, or twice the number of acres contained in the survey. Divide this remainder by 2, and the quotient thence arising by 160 (the number of perches in an acre), then will this last quotient exhibit the number of acres and perches contained in the whole survey; which in this example may be called 110 acres, 103 perches, or 110 acres, 2 quarters, 23 perches.

FIELD-NOTES, of the two foregoing Methods, as Practised in Pennsylvania.

Cast up by perches and tenths of a perch.

N.	. Courses.	Dist	N.	5.	E.	W.	MD.	N. Area.	S. Areas.
1	N 75.00 E	54.8	14.2		52.9		285.3 288.2	5341.26	
2	N 20.90 E	41.2	38.6		14.4		302.6 317.0	11680.36	400 400 400
3	East.	64.8			64.8		381.8 446.6		
4	S 33.30 W	141.2		117.7		77.9	\$68.7 290.8		43395.99
5	8 76.00 W	64.0		15.5		62.1	228.7 166.0		3544.85
6	North.	36.0	36.0				166.6 166.6	5977.60	
7	S 84.00 W	46.4		4.9		46.1	120.5 74.4		590.45
8	N 58.15 W	46.4	27.8			37.2	97.2 00.0	1034.16	
9	N 36.45 E	76.8	61.5		46.0		46 .0 92.0	2829.00	
19	N 22.30 E	56.0	51.7		21.4		113.4 154.8	5862.78	-
11	8 76.45 E	48.0		11.0	46.7		181.5 928.2		1996.50
12	8 15,00 W	43.4		41.9		11.2	217.0 205.8		9092.30
13	S 16.45 T	40.5		88.8		11.7	194.1		7531.08
	•		229.8	229.8	246.2	46.2		30745.16	36151.17 74 5.16
								2	5406.01
							Area	in perches.	1 7703 (6 05
									-

SECTION IV.

OF OFF-SETS.

In taking surveys it is unnecessary and unusual to make a station at every angular point, because the field-work can be taken with much greater expedition, by using off-sets and intersections, and with equal certainty; especially where creeks, &c. bound the survey.

Off-sets are perpendicular lines drawn or measured from the angular points of the land, that lie on the right or left hand to the stationary distance, thus,

PL. 11. fig. 2.

Let the black lines represent the boundaries of a farm or township: and let 1 be the first station; then if you have a good view to 2, omit the angular points between 1 and 2, and take the bearing and length of the stationary line 1, 2, and insert them in your field-book: but in chaining from 1 to 2, stop at d opposite the angular point a, and in your field-book insert the distance from 1 to d, which admit to be 4 C. 25L. as well as the measure of the off-set ad, which admit to be 1C. 12L. thus: by the side of your field-book in a line with the first station, say at 4C. 25L. L. 1C. 12L. that is, at 4C. 25L. there is an off-set to the left hand of 1C. 12L.

This done, proceed on your distance line to e opposite to the angle b, and measure eb, supposing then 1 e to be 7C. 40L. and eb 3C. 40L. say (still in a line with the first station in your field-book) "at 7C. 40L. L. 3C. 40L." That is, at 7C. 40L. there is an off-set to the left of 3C. 40L. proceed then with your distance line to f opposite to the angle e, and measure fe; suppose then 1 f to be 13C. and fe 1C. 25L. say in the same line as before, at 13C. L. 1C. 25L. Then proceed from f to 2, ar 1 you will have the measure of the entire stationary line 1, 2, which insert in its proper column by the bearing.

In taking off-sets, it is necessary to have a perch chain, or a staff of half a perch, divided into links for measuring them; for by these means the chain in the stationary line is undisturbed, and the number of chains and links in that line from whence, or to which, the off-sets are taken, may be readily

known.

Having arrived at the second station, if you find your view will carry you to 3, take the bearing from 2 to 3, and in measuring the distance line, stop at l opposite g; admit 2l to be 4C. 10L. and the off-set lg 1C. 20L. then in a line with the second station in your field-book, say at 4C. 10L. R. 1C. 20L. that is, the off-set is a right hand one of 1C. 20L. Again at m, which suppose to be 10C. 25L. from 2; take the off-set mh of 1C. 15L. and in a line with the second station, say at 10C. 25L. R. 1C. 15L. In the same line when you come to the boundary at i, insert the distance 2i, 13C. 10L. thus, at 13C. 10L. 0; that is, at 13C. 10L. there is no off-set. At n, which is 15C. from 2, take the off-set nk 45L. and still opposite to the second station say at 15C. L. 45. L.

Let the line, 3, 6, represent the boundary, which by means of water, briers, or any other impediment, cannot be measured. In this case make one or more stations within or without the land, where the distances may be measured, and draw a line from the beginning of the first to the end of the last distance, thus; make stations at 3, 4, and 5, taking the bearings, and measuring the distances as usual, which insert in your field-book, and draw a mark like one side of a parenthesis, from the third to the fifth station, to shew that a line drawn from the third station to the farthest end of the fifth stationary line will express the boundary. Thus,

No. Sta.	Deg.	Ch. L.
(3	$172\frac{1}{2}$	5.45
4	200	13.25
4	250	3.36

Suppose the point p of the boundary to be inaccessible, by means of the lines 6p or p7, being overflowed, or that of a quarry, furze, &c. might prevent your taking their lengths: in this case take the bearing of the line 6, 7, which insert op-. posite to the sixth station in your field-book with the other bearing; then direct the index to the point p, and insert its bearings on the left side of the field-book, opposite to the sixth station, annexing thereto the words Int. for boundary; and having measured and inserted the distance 6, 7, set the index in the direction of the line 7p, and insert its bearing on the left of the seventh station of the field-book, annexing thereto the words Int. for boundary: the crossing or intersection of these two bearings will determine the point p, and of course the boundary 6p7 is also determined.

If your view will then reach in the first station,

take its bearing, stationary line, and off-sets, as before, and you have the field-book completed. Thus,

The Field-Book.

Remarks and intersect.	N. St.	Deg.	C. L.	OFF-SETS.
318 Int. to a tower	1	358	22.12	At 4 C. 25 L. L. 1C. 12L. at 7C. 40L. L. 3C. 40L. at 13C. L. 1C. 25L.
231 Int. to ditto	2	2973	22.12	At 4C. 10L. R. 1C. 20L. at 10C. 25L. R. 1C. 51L. at 13C. 10L. 0. at 15C. L. 45L.
1554 Int. for bound. 274 Int. for ditto.	5	200 250 125	13.25 3.36 15.15	At 1C. 20L. L. 2C.

Close at the first station.

If you would lay down a tower, house, or any other remarkable object in its proper place; from any two stations take bearings to the object, and their intersection will determine the place where you are to insert it, in the manner that the tower is set out in the figure, from the intersection taken at the first and second stations of the above field-book.

A protraction of this will render all plain, on which lay off all your off-sets and intersections, and proceed to find the content by any of the methods in section the 4th.

The foregoing field-book may be otherwise kept, thus,

Remarks and intersection.	No St.	Deg.	L. han. Off-set Ch. L.	Dist. Ch. L.	R. han. Off-set Ch. L.
318 Int. to a tower	1	358	1.12 3.40 1.25	4.25 7.40 13.00 22.12	
232 Int. for ditto.	2	2971	0.45	4.10 10.25 13.10 15.00 21.21	1.20
155 ¹ Int. for bound.	3 4 5 6	172½ 200 250 125	1	5.45 13.25 3.36 15.15	
274 In. for boundary.	7	105	2.20 2.32	1.20 7.45 11.25 12.25 15.10	0.36

How to east up off-sets by the pen.

PL. 11. fig. 2.

$$1, 2-1f=2f-1e=fe, 1e-1d=ed.$$

Then $1d \times \frac{1}{2}da = 1da$, by prob. 6, page 183, and $\frac{1}{2}cd \times da + fc = bcfc$, and $2f \times \frac{1}{2}fc = cf9$; the sum

of all which will be 1abc21; the area contained between the stationary line 1, 2, and the boundary, 1 abc 2.

In the same manner you may find the area of 2ihg2, of ik3i, as well as what is without and withinside of the stationary line 7, 1.

If therefore the left hand off-sets exceed the right hand ones, it is plain, the excess must be added to the area within the stationary lines, but if the right hand off-sets exceed the left hand ones, the difference must be deducted from the said area; if the ground be kept on the right hand, as we have all along supposed; or in words, thus;

To find the contents of off-sets.

- 1. From the distance line, take the distance to the preceding off-set, and from that the distance of the one preceding it, &c. in four-pole chains; so will you have the respective distances from off-set to off-set, but in a retrograde order.
- 2. Multiply the last of these remainders by the first off-set, the next by the sum of the first and second, the next by half the sum of the second and third, the next by half the sum of the third and fourth, &c. The sum of these will be the area produced by the off-sets.

Thus, in the foregoing field-book, the first stationary line is 22C. 12L. or 11C. 12L. of four-pole chains. See the figure.

•	Ch. L.	Ch. L.	Ch. L
From	11.12 = 1,2	6.50 = 1f	3.90 = 1e
Take	6.50 = 1f	3.90 = 1e	2.25 = 1d
	4.62=2f	2.60 = ef	1.65 = ed
ed=1.6 $ef=2.60$ $2f=4.6$ Conten	5×1C. 26L.±0 0×1C. 32L.± 2×37L. half	the sum of 2d the last off-set ets on the first	st and 2d 2.0790 and 3d=3.4320 = 1.7094
The sur	n of the left	e rest are perfo hand off-sets v right hand one	vill be 14.0856
Excess	of left hand o	ff-sets in squ. 4	pole C. 10.4031 Acres 1.04031
•			.16124
•	•		

Excess of left hand off-sets above the right hand ones, 1A. 0R. 6P. to be added to the area within the stationary lines.

6.4496

Perches

SECTION V.

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To find the area of a friece of Ground by intersections only, when all the angles of the field can be seen from any two Stations on the outside of the ground.

PL. 12. fig. 1.

LAET ABCDEFG be a field, H and I two places on the outside of it, from whence an object at every angle of the field may be seen.

Take the bearing and distance between H and I, set that at the head of your field-book, as in the annexed one. Fix your instrument at H, from whence take the bearings of the several angular points A, B, C, D, &c. as they are here represented by the lines HA, HB, HC, HD, &c. fix your instrument at I, and take bearings to the same angular points, represented by the lines IA, IB; IC, ID, &c. and let the first bearings be entered in the second column, and the second bearings in the third column, of your field-book; then it is plain that the points of intersection, made from the bearings in the second and third columns of every line, will be the angular points of the field, or the points A, B, C, D, &c. which points being joined by right lines, will give the plan ABCDEFGHA required.

Bear. 180 Dis	s. 2	8C. of	the S	ta. H and I.
11	Vo.	Bear.	Bear.	
			3311	
	1		317	
31			307출	
	\mathbf{D}	2384	289	
	E	$215\frac{1}{2}$	2622	
		$208\frac{1}{2}$		
	G	220	300	

The same may be done from any two stations within-side of the land, from whence all the angles of the field can be seen.

This method will be found useful in case the stationary distances from any cause prove inaccessible, or should it be required to be done by one party, when the other in whose possession it is, refuses to admit you to go on the land.

To find the content of a field by calculation, which was taken by intersection.

In the triangle AIH, the angles AHI, AIH, and the base HI being known, the perpendicular Aa, and the segments of the base Ha, AI may be obtained by trigonometry: and in the same manner all the other perpendiculars Bb, Cc, Dd, Ee, Ff, Gg, and the several segments at b, c, d, e, f, and g: if therefore the several perpendiculars be supposed to be drawn into the scheme (which are here omitted to prevent confusion arising from a multiplicity of lines) it is plain that if from bBCDEeb, there be taken bBAGFeb, the remainder will be the map ABCDEFGA.

As before half the sum of Bb, and Cc multiplied by bc, will be the area of the trapezium bBCc; after the same manner, half the sum of Cc, and Dd, multiplied by cd, will give the area of the trapezium cCDd; and again, half the sum of Dd, and Ee multiplied by de, gives the area of the trapezium dDEe; and the sum of these three trapezia will be the area of the figure bBCDeb.

Again, in the same manner, half the sum of Bb and Aa multiplied by ah, will give the area of the trapezium BbAa; and half the sum of aA, and gG, by ag, gives the trapezium aAGg; to these add the trapezia gGF, and fFEe, which are found in the like manner; and you will have the figure bBAGFEeb, and this taken from bBCDeb, will leave the map ABCDEFGA. Q. E. F.

It will be sufficient to protract this kind of work, and from the map to determine the area as well as in plate 10. fig. 3. to find the areas of the pieces, 3, 4, 5, 6, 3, and 6, 7, 7, 6, from geometrical constructions.

How to determine the station where a fault has been committed in a field book, without the trouble of going round the whole ground a second time.

From every fourth or fifth station, if they be not very long ones, or oftener if they are, let an intersection be taken to any object, as to any particular part of a castle, house, or cock of hay, &c. or if all these be wanting, to a long staff with a white sheet or napkin set thereon, to render the object more conspicuous, and let this be placed on the summit of the land, and let the respective intersections so

taken be inserted on the left hand side of the fieldbook, opposite to the stations from whence they were respectively taken.

In your protraction as you proceed, let every intersection be laid off from the respective stations from whence they were taken, and let these lines be continued; if they all converge or meet in one point, we thence conclude all is right, or so far as they do converge; but if we find a line of intersection to diverge or fly off from the rest, we may be sure that either a mistake has happened between the station the foregoing intersection was taken at, and the station from whence the intersection line diverges, or there must be an error in the intersection; but to be assured in which of these the fault is, protract on to the next intersection, and having set it off, if it converges with the rest, though the foregoing one did not, we may conclude the fault was committed in taking the last intersection but one, and none in any station, and that so far is true as is protracted; but if this as well as the foregoing intersection diverge or fly from the point of concourse or converging point of the rest, the error must have its rise from some station or stations, at or after that, from whence the last converging intersection line was taken: so that by going to that station on the ground, and proceeding on to that where the next, or from whence the following diverging intersection was taken, we can readily and with little trouble set all to rights.

But in most tracts of land, one object cannot be seen from every station, or from perhaps one fourth of them; in this case we are under the necessity to move the pole after we begin to lose sight of it, to some other part of the land, where

it may be seen from as many more stations as possible; which is easily done by viewing the boundary before it be surveyed: the pole then being fixed in an advantageous place, the first intersection to it is best to be made from the same station from whence the last one was taken, and then as often as may be thought convenient, as before; in like manner the whole may be done by the removal of the pole.

When we here speak of stations, we do not mean such as are usually taken at every particular angle of the field: for it is to be apprehended, that every skilful surveyor, particularly such who use calculation, will take the longest distances possible, not only to lessen the number of stations, for the ease of either protraction or calculation, but with greater certainty to account for the land passed by, on the right hand or on the left, which is taken by off-sets: and surely it will be allowed that any measure taken on the ground, and the content thence arithmetically computed, will be much more accurate than that which is obtained from any geometrical projection.

From what has been said it is plain, that from this method any fault committed in a survey can be readily determined, and therefore must be much preferable to the present method of taking diagonals, or the bearings and lengths of lines across land, to accomplish that end; which last method is too frequently used by surveyors to approximate or arrive near the content, which will ever remain uncertain, let these diagonals be ever so many, till the station or stations wherein the error or errors were committed, be found; and the fault or faults be corrected.

Where one diagonal is taken, it may perhaps close or meet with one part of the survey and not with the other; in this case, if the surveyor would discover his error, he must survey that part of the land which did not close, and this may be half or more, of the whole. And should the diagonal close with neither part, but be too long, or too short, or should it fall on either side of the assigned point it was to close with, he ought to go over the whole, and make a new survey of it in order to discover his error.

A number of diagonals are frequently taken, the sum of the lengths of which very often exceeds the circuit of the ground, and after all they are but approximations, and the content remains uncertain as before; therefore he who returns a map, made up by the assistance of diagonals, where there remains a misclosure in any one part, runs the risque of being detected in an error, and must suffer uneasiness in his mind, as he cannot be certain of the return he makes.

The frequent misclosures which are botched up by diagonals, occasion the many and frequent scandalous broils and animosities between surveyors, which tend to the loss of character of the one or the other, and indeed often to the disrepute of both, as well as to that of the science they profess.

But these may be easily remedied by intersections, and the bearing or line to be adjusted where the fault was committed, and till this be found, nothing can be certain.

SECTION VI.

To enlarge or diminish maps.

To enlarge or diminish a map, or to reduce a map from one scale to another; also the manner of uniting separate maps of lands which join each other, into one Map of any assigned size.

LAY the map you would enlarge, over the paper on which you would enlarge it, and with a fine protracting pin, prick through every angular point of your map, join these points on your paper (laying the map you copy before you) by pencilled or popped lines, and you have the copy of the map you are to enlarge: in this manner any protraction may be copied on paper, vellum, or parchment, for a fair map.

If you would enlarge a map to a scale which is double, or treble, or quadruple to that of the map to be enlarged, the paper you must provide for its enlargement must be two, or three, or four times as long and broad as the map; for which purpose in large things you will find it necessary to join several sheets of paper, and to cement them with white wafer or paste, but the former is best,

Then pitch upon any point in your copied map for a centre; from whence if distances be taken to its extreme points, and thence if those distances be set in a right line with (but from) the centre, and these last points fall within your paper, the map may be increased on it to a scale as large again as its own; and if the like distances be again set outwards in right lines from the centre, and if these last points fall within your paper, it will contain a map increased to a scale three times as large as its own, &c.

PL. 12. fig. 2.

Let the pricked or popped lines represent the copy of a down or old survey, laid down by a scale of 80 perches to an inch, and let it be required to enlarge it to one laid down by 40 to an inch.

Pitch upon your centre as Θ , from whence thro' a lay the fiducial edge of a thin ruler, with a fine pointed pair of compasses, take the distance from a to the centre Θ , and lay it by the ruler's edge from a to A: in the like manner take the distance from the next station b to the centre Θ , and lay it over in a right line from b to B, and join the points A and B by the right line AB; in the like manner set over the distance from every station to the centre, from that station outwards, and you will have every point to enlarge to; the joining of these constantly as you go on by right lines, will give you the enlarged map required.

In taking the distance from every station to the centre, set one foot of the compasses in the station, and the other very lightly over the centre-point, so lightly as scarcely to touch it, otherwise the centre-point will become so wide, that it may occasion several errors in the enlarged map: for

if you err from the exact centre but a little, that error will become double, or treble, or quadruple, as you enlarge to a scale that is double, or treble, or quadruple of the given one; therefore great accuracy is required in enlarging a map.

When you have done with a station, give a dash with a pen or pencil to it, such as at the station a and b; by this means you cannot be disappointed in missing a station, or in laying your ruler over one station twice.

From what has been said it is plain, that if a map is to be enlarged to one whose scale is double the given one, that the distances from the respective stations to the centre, being set over by the ruler's edge, will give the points for the enlarged one. And thus may a map be enlarged from a scale of 160 to one of 80, from one of 80 to one of 40, from one of 20 to one of 10 perches to an inch, &c. For to enlarge to a scale that is double, the number of perches to an inch for the enlarged map must be half of those to an inch for that to be enlarged: to enlarge to a scale that is treble the given one, the number of perches to an inch for the enlarged map, will be one third of those for the other; if to a scale that is quadruple the given one, the number of perches to an inch for the enlarged map, will be one fourth of those for the other, &c. therefore if you would enlarge a map which is laid down by a scale of 120 perches to an inch, to one of 40 perches to an inch, the distance from the several stations to the centre, being set twice beyond the said stations, will mark out the several points required, for these points will be three times further from the centre than the stationary points of the map are.

Mm

In the same manner, if you would enlarge a map from a scale of 160, to one of 40 perches to an inch, the distance from the several stations to the centre, being set three times beyond said stations, will lay out the points for your enlarged map, for these points will be four times further from the centre than are the stations of the map.

When a map is enlarged to another, whose scale is double, or treble, or quadruple, &c. of the given one, every line, as well as the length and breadth of the enlarged map, will be double, or treble, or quadruple, &c. those of the given one, for it must be easy to conceive that those maps are like: but the area, if the scale be double, will be four times; if treble, nine times; if quadruple, sixteen times that of the given figure; that is, it will contain four, nine, or sixteen times as many square inches as the given one (for it has been shewn that like polygons are in a duplicate proportion with the homologous sides). Yet these figures being cast up by their respective scales will produce the same content.

Thus much is sufficient for enlarging maps, and from hence, diminishing of them will be obvious; for one fourth, one third, or half the distances from the several stations to the centre, will mark out points, which if joined, will compose a map similar to the given one, whose scale will be four times, three times, or twice as small as the given one.

Thus, if we would reduce a map from 40 to 80, from 20 to 40, from 10 to 20 perches to an inch, &c. half the distance of the stations from the centre will give the points requisite for drawing the

map; if we would reduce from 40 to 120, from 20 to 60, from 10 to 30 perches to an inch, &c. one third of the distances to the centre, will give the points for the map; and if we would reduce from 40 to 160, from 20 to 80, from 10 to 40 perches to an inch, &c. one fourth of the distances to the centre, will give the points for the map.

By the methods here laid down I have reduced a map from a scale of 40 to one of 20 perches to an inch, which contained upwards of 1200 acres, and consisted of 224 separate divisions, without the least confusion from the lines; for none can arise if the methods here laid down be strictly observed.

I have also from the same methods reduced a large book of maps, each of which was an entire skin of parchment, and the whole contained upwards of 46000 acres, to a pocket volume; and afterwards connected all these maps into one map, which was contained in one skin of parchment: therefore upon the whole I do recommend these methods for reducing maps to be much more accurate than any of the methods commonly used, such as squaring of paper, using a parallelogram, proportionable compasses, or any other method I ever met with, though the figures to be reduced were ever so numerous, irregular, or complicated.

To unite separate maps of lands which join each other, into one map of any assigned size.

If there be several large maps contained in a book, each of which suppose to take up a skin

of parchment, or a sheet of the largest paper; which maps of lands join each other; and it be required to reduce them to so small a scale, that all of them when joined together may be contained in one skin, half a skin, or any assigned sized piece of parchment, or paper.

Having pricked off and copied the several maps on any kind of paper, unite them by cutting with scissors along the edge of one boundary which is adjoining the other, but not cutting by the edge of both, and throw aside the parts cut off; then lay these together on a large table, or on the floor, and where the boundaries agree, they will fit in with each other as indentures do; and after this manner they are easily connected: measure then the length and breadth of the entire connected maps, and the length and breadth of the parchment or paper you are confined to; if the former be three, four, or five times greater (that is, longer and broader) than the latter, reduce each copied map severally to a scale that is three, or four, or five times less, as before; and the same parts of the boundaries you cut by in the large maps, by the same you must, also cut in small ones, and unite the small as the large ones were united; cementing them together with white wafer: thus will your map be reduced to the assigned size, which copy over fair, on the parchment, or paper you were confined to.

But it is not always that a person is confined to a given area of parchment, or paper; in such cases, if there are many large maps to be united into one, reduce each of them severally to a scale of 160 perches to an inch, and unite those by the contiguity or boundaries, as before: or if you have a few, it will be sufficient to reduce them to a scale of 120, &c. But having the maps given, and the scale by which they are laid down, your reason will be sufficient to direct you to know what scale they should be reduced to

Directions concerning surveys in general.

If you have a large quantity of ground to survey, which consists of many fields or holdings, and that it be required to map and give the respective contents of the same, it is best to make a survey of the whole first, and to be satisfied that it is truly taken, as well as to find its content; and as you go round the land, to make a note on the side of your field-book at every station where the boundary of any particular field or holding intersects or meets the surround; then proceed from any one of those stations, and in your field-book say, "proceed from such a station," and when you have gone round that field or division, insert the station you close at, and so through the whole: a little practice can only render this sufficiently familiar, and the method of protraction must be evident from the field-notes. When the whole is protracted, and you are satisfied of the closes of the particular divisions, cast up each severally, and if the sum of their contents be equal to the content of the whole first found, you may safely conclude that all is right.

The protraction being thus finished and cast up, transfer it on clean paper, vellum, or parchment, as before; be careful to draw your lines with a fine pen, write on it the names of the circumjacent lands, and set No. 1, 2, 3, 4, &c. in every parti-

cular field or division; let every tenant's particular holding be distinguished by a different coloured paint being run finely along the boundaries; let all the roads, rivulets, rivers, bridges, bogs, ponds, houses, casfles, churches, beacons (or whatever else may be remarkable on the ground) be distinguished on the map. Write the title of the map in a neat compartment either drawn, or done from a good copper-plate graving, with the gen-tleman's arms. Prick off one of your parallels with the map, and on it make a mariner's compass, and draw a flower-de-luce to the north, and this will represent the magnetical north; after which set off the variation, which express in figures, and through the centre of the compass, let a true meridian line be drawn of about 3 inches long, by which write True Meridian. Let a scale be drawn, or it is sufficient to express the number of perches to an inch, the map was laid down by. Draw a reference table of three, or, if occasion be, of four or more columns; in the first insert the number of the field or holding: in the next its name, and by whom occupied: in the third the quantity of acres, roods, and perches it contains: if you have unprofitable land, as bog or mountain, let the quantity be inserted in the fourth column; and, if it be required, you may make another column for statute measure, and then the map is completed.

SECTION VIL

THE METHOD OF DIVIDING LAND, OR OF TAKING OFF OR INCLOSING ANY GIVEN QUANTITY.

Example 1.

PL. 12. fig. 1.

Let ABCD, &c. be a map of ground, containing 11 acres, it is required to cut off a piece as **DEFGID**, that shall contain 5 acres.

Join any two opposite stations as D and G, with the line DG, (which you may nearly judge to be the partition line) and find the area of the part DEFG, which suppose may want 3R. 20P. of the quantity you would cut off: measure the line DG, which suppose to be 70 perches. Divide 3R. 20P. or 140P. by 25, the \$ of DG, and the quotient 4 will be a perpendicular for a triangle whose base is 70, and the area 140P. Let HI be drawn parallel to DG, at the distance of the perpendicular 4, and from I, where it cuts the boundary, draw a line to D, and that line DI, will be the division line; or a line from G to H will have the same effect; all which must be evident from what has been already said.

But if hills, trees &c. obstruct the view of the points D and I from each other, it will be necessary in order to run a partition line, to know its bearing; and it may be proper on some occasions, to have its length; both these may be easily calculated from the common field-notes only, as in the following example, without the trouble of any other measurement on the ground, or any depen-

dance on the map and scale.

EXAMPLE II.

PL. 12. fig. 3.

Let ABCDEFGHIA be a tract of land, to be divided into two equal parts, by a right line from the corner I to the opposite boundary CD; required the bearing and length of the partition line IN, by calculation, from the following field-notes, viz.

Fi	eld-	Notes	and A	rea.
Boun.		Bearin	ıg.	Perch.
AB	N.	190.	o'E.	108.
BC	S.	77.	o E.	91.
CD	S.	27.	o E.	115.
DE	S.	52.	oW.	58.
EF	S.	15.	30E.	76.
FG		Wes	t.	70.9
GH	N.	36.	ow.	47.
HI		Nort	h.	64.3
IA	N.	62.	15W.	59.
	152	١.	1R.	25.9P.

Operation.

1	IABCI	•	Per.	N.	. S.	E.	W.	Z
IA	N. 62°±	w.	59	27.5			52.2	3.
AB	N. 19	E.	188	102.1		35.2		d d
BC	S. 77	E.	91		20.5	88.7		2
CI					109.1	,	71.7	œ
Are	a,8722.3	per	ches	129.6	129.6	123.9	1123.9	CC.

152A. 1R. 25.9P.=24385.9 perch. half, to be divided off,=12192.9 the part IABCI = 8722.3 subt.

Triangle ICNI = 3470.6 perches.

	ICDI.	Per.	N.	S.	E.	W.	M
	N.—E. S. 27. E.				52.2	123.9	rid. dist.
Arc	ca, 6522.1	per.	109.1	109.1	122.9	123.9	9xc

Then, $\{ICDI:CD:ICNI:CN\}$ Th. 18 as $\{6522.1:115::3470.6:61.19\}$ Sec. 1 which determines the point N in CD.

	ICNI.	Per.	N.	S.	E.	W.
IC CN NI	as before S. 27 E.	61.2	109.1	54.6	17.7 27.8	
				54.6		99.5

As dif. lat.	54.6	As S.	Bear	61•15/
: Radius	S. 90 deg.	: Depa		99.5
:: Depart.	99.5	$:: \mathbf{Rad}$	ius S.	90 deg.
: Tang. Bea	er. 61°15′	: Dista	nce	113.49

Answer, { IN runs N. 61 • 15 E. } 113.5 per.

In the part IABCI, the difference between the northings and the southings of the three lines, IA, AB and BC (109.1) is the difference of latitude, and that of their eastings and westings (71.7) the departure of the line CI, which is placed thereto, so as to balance the columns; see theo. 1. sect. 5. hence the content is obtained, as already taught, without the bearing or length of the line CI.

For the triangle ICDI, the diff. lat. and dep. of IC are taken from the preceding table, which in going from I to C will be northing and easting: those of CD are found by the bearing and distance, and of DI by balancing the columns, as before for CI.

The difference of latitude (54.6) and departure (99.5) of the line NI, in the third table, are found by balancing those of IC and CN; and as they are the base and perpendicular of a right angled triangle, of which the line NI is the hypothemuse, and the angle opposite to the departure, the bearing, we have the answer by two trigonometrical statings, as above; and thus may any tract be accurately divided, or any proposed quantity readily cut off or inclosed.

Now the student or practitioner may calculate the content of the part ABCNIA (the bearing and distance, or the diff. lat. and dep. of CN and of NI being known) and if it be found equal to the intended quantity, it proves the truth of the operation.

Example III.

P. 12. fig. 3.

It is proposed to cut off 38A. 16P_‡. to the south end of this tract, by a line running from E due West 40 perches to a well at O, and from thence a right line to a point M in the boundary HI; the place of M, and the bearing and length of the line OM are required; the field-notes being as in example 2d.

Answer, { M from H, north, 43.23 } perchest OM, N. 78°7 W. 39.03 } perchest

In this example we find,

The area of	OEFGHO	===	5270.5
Consequently of	HOMH		826.0
Dif. lat. of the line	HO=HV	==	35.2
Departure of ditto	=QV	==	38.2

As HI happens to be a meridian, the area of HOMH divided by half OV (19.1) quotes HM (43.23) without finding the area of HOIH, as we did of ICDI in example 2d. and HM-HV=VM=8.03= dif. lat. of OM, which with its dep. VO=38.2. gives the bearing and distance as before.

EXAMPLE IV.

PL. 12. fig. 4.

A trapezoidal field ABCD, bounded as under specified, is to be divided into two equal parts by a right line EF parallel to AB or CD; required AF or BF?

Bou.	Bearing.	Per.	
AB	South.	30.	
BC	N. 80 W.	60.	
CD	N. 391 W.	45.5	
DA		89.4	
13A. 3R. 7P.			

In the triangle CBG are given BC and all the angles (known by the bearings) to find BG, and thence the area by prob. 9. sect. 4. which that the area of ABCD = area of EFG; then as the area of CBG to that of EFG, so is the square of BG to the square of FG, and FG—BG=BF.

Operation at large.

Angle G 39° 30′, log. S. Co. A Side BC 60 per. log.	1.77815 add
Angle C 40° 30′, sine	9.81254
Side BG 61'. 26 per. Side BC 60 per. Angle B 100° 0', sine	1.78718 1.77815 9.99335
2)3619.8, log.	3.55868
As $CBG = 1809.9$ Co. Ar. 1103.5 = BCEF	6.74235
To $EFG = 2913.4$, log.	3.46440 >add
So sqr. BG 61. 26, log. {	1.78718 1.78718
To sqr. FG 77.72	(2)3.78111
Ans. $BF = 16.46$ per.	1.89055

By the application of this method a tract of land may be divided accurately, in any proportion, by a line running in any assigned direction.

Note. When the practitioner would wish to be very accurate, it will be much better to work by four-pole chains and links than by perches and tenths; one tenth of a perch square being equal to 62 square links.

Example v.

The following Field-Notes (from A. Burns) are of a piece of land, which is proposed, as an example, to be divided into three equal parts by two right-lines running from the sixth and seventh stations; and proved, by calculating the content of the middle part.

St.	Bear	ng.	P.C.
1.	N.E.	56°4	21.60
2	N.E.	261	13.44
3	S.E.	714	18.96
4	S.E.	263	13.44
5	s.w.	714	18.96
6	S.E.	45	8.47
7	S.E.	63 }	13.44
8	N.E.	45	8.47
9	S.E.	26	13.44
.10	s.w.	45	8.47
11	s.w.	63 إ	13.44
12	N.W.	76	24.73
1:	N.W.		30.00
A	A. rea 167		P. 24.

EXAMPLE VI.

PL. 8. fig. 5.

The plot ABCDEFGHA is proposed to be divided, geometrically, in the proportion of 2 to 3, by a right line from a given point in any boundary or angle thereof, suppose the point D.

Reduce the plot to the triangle cDe, as already taught; divide the base ce in the point N, so that cN be to Nc in the ratio of two or three, by prob. 14. page 53; draw DN, and it is done.

EXAMPLE VII.

PL. 12. fig. 3.

Example 2d may likewise be performed geometrically.

Produce CD both ways for a base, and reduce the whole to a triangle, making I the vertical point; then bisect the base in N, and draw IN. But,

Notwithstanding this geometrical method is demonstrably true in theory, it is not as safe, on practical occasions requiring accuracy, as the calculation, even when performed with the greatest care; for which reason we will not enlarge on it here.

Example viii.

Suppose 864 acres to be laid out in form of a right-angled parallelogram, of which the sides shall be in proportion as 5 to 3; required their dimensions?

For the greater side, multiply the area by the greater number of the given proportion, and divide

by the less, or, for the less side, multiply by the less number, and divide by the greater; the square root of the quotient will be the side required: thus,

864 A. = 138240P	1.38240
. . . .	3
	
3)691200	5)414720
Answ.	√ 82944=288,

EXAMPLE IX.

If it be required to lay out any quantity of ground, suppose 47A. 2R. 16P. in form of a parallelogram, of which the length is to exceed the breadth by a given difference, for instance 80 perches, then add the square of half this difference to the area; and take the square-root of the sum; to which add half the difference for the greater side, and subtract it therefrom for the less; thus,

2)80		17A. 2	2R. 1	6P.=	=7616 perches. 1600
40	1			4	9216=96
1690	half	diff.	add	and	subt.—40
	٠.	Ans.	{ the	e leng e bre	gth = 136 $adth = 56$

Any proposed quantity of ground may be laid out or inclosed in the form

of a Square - by prob. 2d. Parallelogram, I side giv. by pro. 4th. Triangle of a given base, by pro. 7th. Circle - by prob. 13th.

It is sometimes most convenient, when land is to be laid out adjacent to a creek, river, or other crooked boundary, to measure off-sets to the angles or bending thereof, from a right line or lines taken near such boundary, and to deduct the area of these off-sets from the given quantity, and then to lay off the remainder from the right-line or lines, in the desired form.

In laying out new lands, attention must be paid to the allowance for roads, as exemplified in prob. 14th.

Example x.

It is required to divide off 30 acres, to the south east end of the tract, of which the field-notes are given in example 4th, by a right-line to run N. 20° E. See example 4th.

SECTION VIII.

OF SURVEYING HARBOURS, SHOALS, SANDS, &C.

PL. 13. fig. 1.

HERE are three methods whereby this may be performed; for the observations may be made either on the water or on the land. Those made on the water are of two kinds, one by the log-line and compass (as in plane sailing measuring) the course and distance round the sand; and then to be plotted as a large wood, or any inclosure taken by the circumferentor.

This method I omit for two reasons; first, because it is to be deduced from the writers of navigation: and, secondly, because the distances thus measured are liable to the errors of currents, which generally attend shoals or sands near the shore.

The second method, where there are no distances to be measured on the water, though still there is one inconvenience, common also to the former, because the bearings or observations are to be taken on that unstable element (an error scarce mentioned by practical artists) I shall briefly hint at; and so rather choose a third, which is liable to neither of these imperfections.

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Let a hoat be manned out with a signal flag, a log and line, lead and line, and to observe the bearings of any land mark, a compass with sights.

Take two or more objects or places, as A, B, C, on the shore, from whence the boat may be seen on the several parts of this shoal, and determine their relative position by bearing and distances either before or after the other necessary observations are made.

One of the boat's crew is to sound till he finds himself on the edge of the sand, by the depth of water, and then to come to an anchor; which he is to signify to two persons on the shore, at B and C, by his signal. And then from those known land-marks, B and C, the observers are to take the bearings of the boat, and to register their observations; which, when done, they are to signify to the crew by waving a flag, or by some other signal.

And in the mean time, to prevent mistakes, let the crew take the bearings of each of these landmarks: then weigh anchor, which suppose at D.

Then by sounding, proceed to E, and make like observations. And so at E, F, G, &c. till you have surrounded your sand.

And if in this process, you are about to lose the sight of one of your land-marks, suppose C, let your assistant at C, or B, who at that time will also be about to lose the sight of the boat, by signals (before agreed on) remove to some other object before-hand agreed on, suppose to H, or K; and then to proceed as before.

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Lastly, if the sand runs so far out at sea, that the object cannot be seen by the boat, nor the boat by the observer on shore; there may be rockets fired by the boat's crew, and also by the observers on the shore in the night, whereby those bearings may be taken almost at as great a distance as the light can be seen. For supposing they rise but a quarter of a mile above the apparent horizon, its stay will be about 9 seconds, and its distance for this quarter of a mile will be visible about 44 miles.

But rockets rise much higher, and then the distances are much greater, whereby they are visible.

Or two boats may lay at anchor instead of the land marks, and then you may work as before.

Now, since the land-marks B and C are fixed, their position may be laid down in the draught, as in common surveying, by plotting the distance between B and C. And then by plotting the line BD, and the line DC, according to their position, their common intersection will give the point D. And in like manner E, F, G, &c. may be plotted; and so the shoals completed. And this from the bearings taken at B and C.

If this be a standing lake, environed by hogs, or other impediments, the observations at D, E, F, &c. by taking their opposites, may suffice to plot the same from the land-mark, A, B, C, &c. as well as those taken on the land: or, indeed, by the course and distance, as in navigation, if the water be smooth and without a current.

In sea shoals, it is convenient to note at each observation the depth of the water found by the lead, and the drift and setting of the current by the logand compass, while the heat is at anchor, which may be done with ease and expedition enough. For, while the boat rides at an anchor, her stern points out the setting of the current, and the logand glass will measure its drift.

And these ought to be noted on the draught, which may be thus:

The currents may be shewn, by drawing a dart pointing out its setting, and its drift by the Roman capital letters, the depth of the water by the small figures, and rocks by little crosses, &c.

SECTION IX.

LEVELLING.

PL. 13. fg. 2.

LEVELLING is the art of ascertaining the perpendicular ascent or descent of one place (or more) above or below the horizontal level of another, for various intentions; and of marking out courses for conveyance of water, &c.

The true level is a curve conforming to the surface of the earth; as ABG.

The apparent level is a tangent to that curve; as ADE.

The correction, or allowance for the earth's curvature, is the difference between the apparent level and the true, as BD. The quantity of this correction may be known by having, in the right-angled triangle CAB, the two legs, AC=the semidiameter of the earth (=1267500 perches) and AD=the distance of the object, to find the hypothenuse CD, from which taking CB: (=CA) the remainder will be the correction BD; but it may be obtained more practically thus;

Square the distance in

(four-pole chains, and divide by \$00,)

or in perches, and divide by 12800,

or in miles, and multiply by

for the correction in inches.

EXAMPLE.

Required the correction for 20 four-pole chains =80 perches=1 mile.

 $800)20 \times 20 = 400(.5)$ $12800)80 \times 80 = 6400(.5)$ 1=.25, and $.25 \times 25 \times 8 = .5$

that is, .5, or 1 inch, the correction required.

But, to save the trouble of calculation, we insert the following table of corrections.

A Table of Corrections:

The distances in four-pole chains.

	Distan	Correc.	Distar.	Corre-	
	Chains	loches	Chains.	nches	
}	1	,0012	27	U,9 1	
4	2	ນ ,Q05	28	0,98	
}	.3 4	0,01125	29	1,05	1
}		J ,02	3 0	1,12	
1	5	0,03	31	',19	
	6	0.04	32	1,27	
	7	90,د	33	1,35	
1	8	.,08	34	1,44	
ł	9).10	3 5	1,53	,
	10	2,12	36	1,62	
į	1 t	J ₁ 15	37	:.71	
I	12	0,18	-38	1,80	
I	13	0,21	39	1,91	
ł	14	0.24	40	2,00	
	15	→.28	45 -	2,28	
ł	16	J,32	50	3,12	211.0
ı	17	0,36	55	8,78	
ı	18	J ,40	. 60	4,50	
	19	0,45	65	5,31	
	20	∴.50	70	6,12	
I	21	1),55	75	7,03	
I	22	0,60	80	8,00	
	23	1.67	85	9,03	,
	24	0.72	90	10,12	* * * *
Ī	25	J.78	95	11,28	and the second
	26),84	100	12,50	, •

The first thing necessary in levelling, is the adjusting of the level, which may be performed several ways; The following is very easy and practical.

Choose some ground which is not above 4 or 5 feet out of the level, for the distance of 8 or 10 chains length, and suppose it be AB (fig. 3.) and find the middle between A and B, which suppose to be C; plant the instrument at C: direct the tube to a station-staff, held up at A, and elevate or

depress the tube, till the bubble is exactly in the middle of the divisions; then by signals direct your assistant at A, to rise or depress the vane, which glass cuts the middle of that vane: then see how many feet, inches, and parts, are cut by the upper part of the vane, which suppose to be 3 feet 4 inches and 6 tenths.

In like manner direct to the other staff at B, and suppose the upper edge of that vane to cut at the height of 6 feet, 5 inches and two tenths, then will these two vanes be on a level.

From 6 feet 5.2 inches subtract 3 feet 4.6 inches, and reserve the remainder 3 feet 0.6 inches.

Now, remove the instrument as close to the higher station-staff as you can; so that the middle of the telescope may almost touch it. Then bring the telescope as near to a level as the judgment of the eye will direct.

Measure from the ground, the height of the top of the telescope; and also of the bottom, in feet, inches, and parts; suppose them to be 4 feet, 10.5 inches, and 5 feet 0.3 inches; then half the sum of the heights 4 feet 11.4 inches is the height of the centre of the glass; and to this add half the breadth of the vane, which suppose to be 1 inch and 5 tenths, and to the sum 5 feet 0.9 inches, add the preceding remainder 3 feet 0.6 inches; then let the person at B move his vane, till the upper edge cut 8 feet 1.5 inches, the sum of the preceding numbers.

Now, so elevate or depress the bair or the bulkble, till the hair cut the middle of the vane at the and at the same time the bubble stands at the middle of the divisions; and then will the instrument be duly adjusted.

If you have a mind to be more accurate, repeat the operation; but when you place the instrument at C, turn the tube at right angles to the line AB, and there set it level; then proceed with a repetition of the work. Only observe to cross-level it in this adjustment, and in all future uses whatsoever.

Or the level may be adjusted thus: As before, first plant the instrument in the middle between A and B (fig. 4.) and observe the heights on the station-staves, which suppose to be as above; and consequently their difference, as before, is 3 feet 0.6 inches. New measure from C towards the highest ground A, some distance that comes almost to A; suppose 4 chains to D, and DR will be Chains, and DA one chain: Then plant the instrument at D, direct the telescope to A, and setting the bubble to the middle of the division. direct your assistant to move the wane, till the hair cuts the middle of it; and note down the feet, inches, and parts cut by the upper edge of the vane; which suppose to be 3 feet 8.4 inches: To this add the difference 3 feet 0.6 inches, and the sum 6 feet 9 inches reserve.

Now direct the telescope to the staff at B, level it, and direct your assistant to move the vane, till the hair cuts the middle thereof; and then, if the upper edge of the vane cuts the foregoing sum 6 feet 9 inches, the hair and bubble are truly adjust-

difference between the numbers cut by the upperetigs of the vane, and the number 6 feet 9 inches;
so is the distance AD to a number, which added
to that cut by the vane, when less than 6 feet 9,
and subtracted from the number cut by the vane,
when it is greater than 6 feet 9, will give a number to which let the assistant fix the vane; then so
elevate or depress the hair or the bubble, till the
hair cuts the middle of the vane at B, and the bubble stands in the middle of the divisions; for then
the level will be adjusted. The operation may
be again repeated, and at every station cross levelled, which will confirm the former adjustment.

Or it will be still better to set the station staves equally distant from the instrument (suppose about 16 or 20 perches each) at an angle of about 60°, or so as to form nearly an equilateral triangle therewith, and level the 2 vanes (A and B fig. 5.) as before, which will be then both in the same horizontal level; whether the instrument be right adjusted or not, because one will be as much above or below the true level of the instrument, as the other, being in the same distance from it; then remove the instrument as near as may be to one of them, suppose A, and raise or lower the vane A to the exact level of the visual ray in the instrument, noting precisely how much it is moved, and have the other vane B move just as much, in order to bring them again to a level, allowing for the correction of the apparent level if it be a sensible quantity; then adjust the instrument to the level of the vane at B.

To adjust the rafter level (plate 13. fig. 6.) which may be 10, 12, or 14 feet in the span AB; set it on a plank or hard ground nearly level, and mark

where the plumb line cuts the beam mn, suppose at c, then invert the position by setting the foot A, in the place of B, and B in that of A, marking where the line now cuts, as at c; the middle point, between c and c will be the true levelling mark.

To continue a level course with this instrument, set the foot A to the starting place, and move B upward or downward toward D or E, till the point B be determined and marked for a level, with A, then carry the instrument forward in the direction of C till the foot A rests at B, whence the point C is levelled as before, &c. Sights may be placed at r and s, and the instrument adjusted to them, as before, by reversing them in the direction of some distant object.

After the instrument is duly adjusted, you may proceed to use it. Let the example be this annexed (fig. 7.) where A every where represents the level, and B the station staves; and suppose the route be made from a to e; first plant the instrument between the staves a and b: at A direct the level to aB, bring the bubble to the middle of the divisions, and instruct your assistant so to place the vane, that the hair in the telescope cuts the middle of the vane, then in a book divide into two columns, the one entitled Back sights, the other Fore sights, enter the feet, inches, and parts cut by the upper edge of the vane at aB, in the column entitled Back sights.

Then look toward the other staff b B, bring the bubble to the middle of the divisions, and direct your assistant to place the vane so, that the hair cuts the middle of the vane; then enter the feet, inches, and parts cut by the upper edge of the vane, in the column of Fere sights.

Now, plant the instrument at A^3 , still keeping the staff Bb exactly in the same place, and carry the staff aB forwards to the place cB; now look back to the staff bB, and enter the numbers cut by the vane there under the title Back sights; then look forwards to cB, and enter the observation under the title Fore sights. Do the like when the instrument is planted at A^3 , A^4 , &c. always taking care to keep the staff in the same place when you looked at it for a Fore sight, till you have also taken with it a Back sight,

Having finished your level, add up the column of Back sights into one sum, and the column of Fore sights also into one sum; and the difference between these sums is the ascent or descent required. And if the sum of the Fore sights be greater than the sum of the Back sights, then e is lower than a; but if the sum of the Fore sights be less than the sum of the Back sights, e is higher than a. For example, let the numbers be as in the following table.

•	Back sights.					Fore sights.					
-	Feet.	7	inch.	-	Tenths	Feet.		Inch.	-	Tenths.	
	3	•	7	•	5	6	•	4	,	5	
1	4	•	6	,	. 8	8	•	3	,	2 1	
	6 .	· • ·	, O	,	2 .	5	•	4	,	. 7.	
	9	•	: 5	3.	0	8	•	7	1	. 8	
	1	•	0	,	7	9	•	4	,	8	
•	24	•	8	,	2	38	•	1	• •	0	
,						24	•	8	,	2	
• '		•			:	13	•	4	,	8	
	Hence	u	e de	300	nt is	13	٠.	4	•	8	

Observations.

- 1. And if the distances thus taken are short, the curvature of the earth may be rejected. For, if the distance from the instrument be every where about 100 yards, all the curvatures in a mile's work will be less than half an inch.
- 2. If the distance from the instrument to the hindermost staff, be every where equal to the distance from the instrument to the corresponding staff; the curvature of the earth, and the minute errors of the instrument, will both be destroyed. Hence it will be much best to set the instrument as equally distant from both staves as may be.
- 3. If the distances of the instrument from the staves, be very unequal and very long, the curvatures must be accounted for, and the distances in order thereto, must be measured.
- 4. Therefore it appears, that the best method to take a level is to measure the several distances from the instrument to the back and forward station staves; and enter them in the field-book, according to the titles of their several columns, as in the following example; and correct the heights from the table of allowances, which may be done at home when you are about to sum up the heights.

-	Backwa	rds.		Forward	ds.	
Distan.	Reight	Corrected.	Distan.	Height	Corrected.	
Links.	Inches.	Inches.	Links.	Inches.	Inches.	•
370	3,25	3,24	418	4,86	4,34	-
480	6,10	6,08	328	7,18	7,17	
760	5,38	5,31	289	6,75	6.67	'
584	7,25	7,21	530	9,53	9,50	•
326	8,15	8,14	485	11,25	11,22	
658	10,25	10,20	376	8,65	8,63.	
· 58 0	6,32	6,29	720	10,34	10,28	•
3658	h i	46,47	31,46		57,81	
3146					46,47	
48,04					11,34	

So that the fall in 68 chains is about 11 inchestand to fan inch.

Lastly, Though hitherto we have considered the level with one telescope only, the same observations may be applied to a level with a double telescope; and I would advise those who use the double telescope, at every station to turn that end of the telescope forward, which before was the contrary way.

· A more general method of leveling, adapted to the surveying of roads and hilly ground, is exhibited in the following example, in which the measures are given in links.

EXAMPLES.

PL. 13. fig. 8.

Required the bearing and distance of the place B from A, and its perpendicular ascent or descent, above or below the horizontal level of A.

Stat.	Course or Bearing	Elev. or Depres.	Obl. Dist.		Perpen. Ascent or desc.	Dil. Lat.	De- part.
2 3 4	NE79°15 NE75 O NE50 30 SE85 15 SE70 O	D 21 45 E 14 00 D 11 30	738 684 976 930 620	635 947 911	253.4 236.1 185.4	,	613
			3948	3783	217.6 Desc.	622 N.	349 2 E.

As Dif. Lat. 622
Is to radius S. 20°,
So is Dep. 3492
To T. Bear. 79° 54′.

As S. Bear. 79° 45′ Is to Dep. 3492, So is radius S. 90° To Dist. 3547.

As 100 links: 66 feet: 217.6 links: 143.6 feet, the descent B below the level of A.

Hence, B bears N. 79° 54′ E. from A
Nearest horiz. dist. 3547 links.
Sum of obl. dist. 3948 links.
Sum of horiz. dist. 3783 links.
Perp. desc. 217.6L. = 143.6.F.

With the angular elevation or depression in the third column, and the oblique distance in the fourth (as course and distance) are found the horizontal distance in the fifth, and the perpendicular ascent or descent on the sixth, for each station (as difference of latitude and departure:) then, with the bearing and horizontal distance we get the difference of latitude and departure in the two last columns.

The ascents and descents in the sixth column are distinguished by the letters E and D in the third, signifying elevation or depression; and being added separately, the difference of their sums

is set at the bottom of the column with the name of the greater, and shews the perpendicular descent of B below the horizontal level of A.

In like manner the northings and southings in the seventh column are distinguished by the letters N and S in the second, &c.

PROMISCUOUS QUESTIONS.

The perambulator, or surveying wheel, is so contrived as to turn just twice in the length of a pole or 161 feet; what then is the diameter? Answ. 2.626 feet.

2. Two sides of a triangle are respectively 20 and 40 perches; required the third, so that the content may be just an acre?

Answ. either 23.099 or 58.876 perches

3. I want the length of a line by which my gardener may strike out a round orangery that shall contain just half an acre of ground.

Answ. 27% yards:

4. What proportion does the arpent of France, which contains 100 square poles of 18 feet each, bear to the American acre, containing 160 square poles of 16.5 feet each, considering that the length of the French foot is to the American as 16 to 15?

Answ. as 512 to 605.

5. The ellipse in Grosvener square measures 840 links the longest way, and 612 the shortest, within the rails: now the wall being 14 inches thick, it is required to find what quantity of ground it incloses, and how much it stands upon.

Answ. it incloses 4A. 6P. and stands on 1760#

square feet.

6. Required the dimensions of an elliptical acre with the greatest and least diameters in the proportion of 3 to 2?

Answ. 17.479 by 11.653 perches..

7. The paving of a triangular court at 18d. per foot, came to 100l. The longest of the three sides was 88 feet: what then was the sum of the other two equal sides?

Answ. 106.85 feet.

8. In 110 acres of statute measure, in which the pole is 16½ feet, how many Cheshire acres, where the customary pole is 6 yards, and how many of Ireland, where the pole in use is 7 yards?

Answ. 92A. 1R. 28P. Cheshire; 67P. 3R. 25P.

Trish.

9. The three sides of a triangle containing 6A. 1R. 12P. are in the ratio of the three numbers, 9, 8, 6, respectively; required the sides?

Answ. 59.029, 52.47, and 39.353.

10. In a pentangular field, beginning with the south side, and measuring round towards the east, the first or south side is 2735 links, the second 3115, the third 2370, the fourth 2925, and the fifth 2220; also the diagonal from the first angle to the third is 3800 links, and that from the third to the fifth 4010; required the area of the field?

Answ. 117A. 2R. 28 P.

11. Required the dimensions of an oblong garden containing three acres, and bounded by 104 perches of pale fence?

Answ. 40 perches by 12.

12. How many acres are contained in a square meadow, the diagonal of which is 20 perches more than either of its sides?

Answ. 4A. 2R. 11P.

13. If a man six feet high travel round the earth, much greater will be the circumference described by the top of his head than by his feet?

Answ. 37.69 feet.

- N. B. The required difference is equal to the circumference of a circle 6 feet radius, let the magnitude of the earth be what it may.
- 14. Required the dimensions of a parallelogram containing 200 acres, which is 40 perches longer than wide?

Answ. 200 perches by 160.

15. What difference is there between a lot 28 perches long by 20 broad, and two others, each of half the dimensions?

Answ. 1A. 3R.

PART III.

containing the Astronomical methods of finding the Latitude, Variation of the compass, &c. with a description of the instruments used in these operations.

SECTION I.

INTRODUCTORY PRINCIPLES.

AY and night arise from the circumstation of the Earth. That imaginary line about which the rotation is performed, is called the Axis, and its extremeties are called Poles. That towards the most remote parts of Europe is called the North Pole, and its opposite the South Pole. The Earth's Axis being produced will point out the Celestial Poles.

The Equator is a great circle on the Earth, every point of which is equally distant from the Poles; it divides the Earth into two equal parts, called Hemispheres: that having the North Pole in its centre is called the Northern Hemisphere—and the other, the Southern Hemisphere. The plane of this circle being produced to the fixed stars, will point out the celestial Equator or Equinoctial. The Equator, as well as all other great circles of the sphere, is divided into 360 equal parts, called degrees; each degree is divided into 60 equal parts, called minutes; and the sexagesimal division is continued.

Note. The ancients having no instruments by which they could make observations with any tolerable degree of accuracy, supposed the length of the year, or annual motion of the earth, to be completed in 360 days: and hence arose the division of the circumference of a circle into the same number of equal parts, which they called degrees.

The Meridian of any place, is a semi-circle passing through that place, and terminating at the Poles of the Equator. The other half of this circle is called the opposite Meridian.

The Latitude of any place, is that portion of the Meridian of that place, which is contained between the Equator and the given place; and is either North or South, according as the given place is in Northern or Southern Hemisphere, and therefore cannot exceed 90°.

The Parallel of Latitude of any place, is a circle passing through that place, parallel to the Equator.

The Difference of Latitude between any two places, is an arch of a meridian intercepted between the corresponding parallels of latitude of those places. Hence, if the places lie between the Equator and the same Pole, their difference of latitude is found by subtracting the less latitude from the greater: but if they are on opposite sides of the Equator, the difference of latitude is equal to the sum of the latitudes of both places.

The First Meridian is an imaginary semicircle, passing through any remarkable place, and is therefore arbitrary. Thus, the British esteem that

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to be the First Meridian which passes through the . Royal Observatory at Greenwich; and the French reckon for their First Meridian, that which passes through the Royal Observatory at Paris.—Formerly many French geographers reckoned the meridian of the island of Ferro to be their First Meridian; and others, that which was exactly 20 degrees to the west of the Paris Observatory. The Germans, again, considered the meridian of the Peak of Teneriffe to be the First Meridian. this mode of reckoning, Europe, Asia, and Africa, are in east longitude; and North and South America, in west longitude. At present, the first meridian of any country is generally esteemed to be that which passes through the principal Observatory, or chief city of that country.

The Longitude of any place is that portion of the Equator which is contained between the first meridian, and the meridian of that place: and is usually reckoned either east or mest, according as the given place is on the east or west side of the first meridian; and, therefore, cannot exceed 180°.

The Difference of Longitude between any two places is the intercepted arch of the Equator between the meridians of those places, and cannot exceed 180°.

There are three different Horizons, the apparent, the sensible, and the true. The apparent or visible Horizon is the utmost apparent view of the sea or land. The sensible is a plane passing through the eye of an observer, perpendicular to a plumbline harging freely; And the true or rational Horizon is a plane passing through the centre of the Earth, parallel to the sensible Horizon.

Altitudes observed at sea, are measured from the visible Horizon. At land, when an astronomical quadrant is used, or when observations are taken with a Hadley's quadrant by the method of reflection, the altitude is measured from the sensible Horizon; and in either case, the altitude must be reduced to the true Horizon.

The Zenith of any given place is the point immediately above that place, and is, therefore, the elevated pole of the Horizon: The Nadir is the other pole, or point diametrically opposite.

A Vertical is a great circle passing through the Zenith and Nadir; and, therefore, intersecting the Horizon at right angles.

The Altitude of any celestial body in that portion of a Vertical, which is contained between its centre and the true Horizon. The Meridian Altitude is the distance of the object from the true Horizon, when on the Meridian of the place of observation. When the observed Altitude is corrected for the depression of the Horizon, and the errors arising from the instrument, it is called the apparent Altitude; and when reduced to the true Horizon, by applying the parallax in Altitude, it is called the true Altitude. Altitudes are expressed in degrees, and parts of a degree.

The Zenith Distance of any object is its distance from the Zenith, or the complement of its Altitude.

The Declination of any object is that portion of its meridian which is contained between the equinoctial and the centre of the object; and is either north or south, according as the star is between the equinoctial and the north or south pole.

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The Ecliptic is that great circle, in which the annual revolution of the Earth round the Sun is performed. It is so named, because Eclipses cannot happen but when the moon is in or near that circle. The inclination of the Ecliptic and Equinoctial is at present about 23° 28'; and by comparing ancient with modern observations, the obliquity of the Ecliptic is found to be diminishing—which diminution, in the present century, is about half a second yearly.

The Ecliptic, like all other great circles of the sphere, is divided into 360°; and is further divided into twelve equal parts, called Signs: each Sign, therefore, contains 30°. The names and characters of these Signs are as follows:

Aries, & Cancer, Libra, Capricornus, & Taurus, & Leo, Scorpio, Maquarius, Cemini, U Virgo, Asagittarius, Pisces,

Since the Ecliptic and Equinoctial are great circles, they, therefore, bisect each other in two points, which are called the Equinoctial Points. The Sun is in one of these points in March, and in the other in September; hence, the first is called the Vernal, and the other the Autumnal Equinox—and that sign which begins at the Vernal Equinox is called Aries. Those points of the Ecliptic, which are equidistant from the equinoctial points, are called the Solstitial Points; the first the summer, and the second the winter solstice. That great circle which passes through the equinoctial points and the poles of the earth, is called. the Equinoctial Colure: and the great circle which passes through the solstitial points and the poles of the earth, is called the Solstitial Colures - " - - - -

When the Sun enters Aries, it is in the Equinoctial; and, therefore, has no declination. From thence it moves forward in the Ecliptic, according to the order of the signs, and advances towards the north pole, by a kind of retarded motion, till it enters Cancer, and is then most distant from the Equinoctial; and moving forward in the Ecliptic. the Sun apparently recedes from the north pole with an accelerated motion till it enters Libra, and being again in the Equinoctial, has no declination; the Sun moving through the signs Libra, Scorpio, and Sagittarius, enters Capricorn; and then its south declination is greatest, and is, therefore, most distant from the north pole; and moving forward through the signs Capricorn, Aquarius, and Pisces, again enters Aries: Hence, a period of the seasons is completed, and this period is called a Solar Year.

The signs Aries, Taurus, Gemini, Cancer, Leo, and Virgo, are called Northern Signs, because they are contained in that part of the Ecliptic which is between the Equinoctial and North Pole; and, therefore, while the Sun is in these signs, its. declination is north: the other six signs are called Southern Signs. The signs in the first and fourth quarters of the Ecliptic are called Ascending Signs: because, while the Sun is in these signs, it approaches the north pole—and, therefore, in the northern, temperate, and frigid zones, the Sun's meridian altitude daily increases; or, which is the same, the Sun ascends to a greater height above the horizon every day. The signs in the second. and third:quarters of the Ecliptic are called Descending Signs,

The Tropics are circles parallel to the Equinectial, whose distance therefrom, is equal to the

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obliquity of the Ecliptic. The Northern Tropic touches the Ecliptic at the beginning of Cancer, and is, therefore, called the *Tropic of Cancer*; and the Southern Tropic touches the Ecliptic at the beginning of Capricorn, and is hence called the *Tropic of Capricorn*.

Circles about the poles of the Equinoctial, and passing through the poles of the Ecliptic, are called Polar Circles; the distance, therefore, of each Polar Circle from its respective Pole, is equal to the inclination of the Ecliptic and Equinoctial. That Circle which circumscribes the North Pole is called the Artic, or North Polar Circle; and that towards the South Pole, the Antartic, or South Polar Circle.

That semicircle which passes through a star, or any given point of the heavens, and the Poles of. the Ecliptic, is called a Circle of Latitude.

The Reduced Place of a Star is that point of the Ecliptic, which is intersected by the circle of latitude passing through that star.

The Latitude of a Star is that portion of the circle of latitude contained between the Star and its reduced place—and is either north or south, according as the Star is between the Ecliptic and the north or south pole thereof.

The Longitude of a Star is that portion of the Ecliptic, contained between the Vernal Equipox and the reduced place of the Star.

SECTION II.

Description of the Instruments requisite in Astronomical Observations.

THE QUADRANT.

T is generally allowed that we are indebted to John Hadley, Esq. for the invention, or at least for the first public account of that admirable instrument, commonly called Hadley's Quadrant, who in the year 1731, first communicated its principles to the Royal Society, which were by them published soon after in their Philosophical Trans. actions; before this period, the Cross Staff and, Davis's Quadrant were the only instruments used for measuring altitudes at sea, both very imperfect, and liable to considerable error in rough weather; the superior excellence however of Hadley's Quadrant, soon obtained its general use among seamen, and the many improvements this instrument has received from ingenious men at warious times, has rendered it so correct, that it is now applied, with the greatest success, to the important purposes of ascertaining both the latitude and longitude at sea, or land.

The Octant or Frame, is generally made of ebony, or other hard wood, and consists of an arch firmly attached to two radii, or bars, which are strengthened and bound by the two braces, in order to prevent it from warping.

 \mathbf{R} $\dot{\mathbf{r}}$

The Arch, or Limb, although only the eighth part of a circle, is on account of the double reflection, divided into 90 degrees, numbered 0, 10, 20, 30, &c. from the right towards the left; these are subdivided into 3 parts, containing each 20 minutes, which are again subdivided into single minutes, by means of a scale at the end of the Index. The arch extending from 0 towards the right hand is called the arch of excess.

The Index is a flat brass bar, that turns on the centre of the instrument; at the lower end of the Index there is an oblong opening: to one side of this opening a Nonius scale is fixed to subdivide the divisions of the arch; at the bottom or end of the index, there is a piece of brass which bends under the arch, carrying a spring to make the Nonius scale lie close to the divisions; it is also furnished with a screw to fix the Index in any desired position.

Some instruments have an adjusting or tangentscrew, fitted to the Index, that it may be moved more slowly, and with greater regularity and accuracy than by the hand; it is proper, however, to observe, that the Index must be previously fixed near its right position by the above mentioned screw, before the adjusting screw is put in motion.

The Nonius is a scale fixed to the end of the Index for the purpose, as before observed, of dividing the subdivisions on the Arch into Minutes; it sometimes contains a space of 7 degrees, or 21 subdivisions of the limb, and is divided into 20 equal parts; hence each division on the Nonius will be one-twentieth part greater, that is, one minute longer than the divisions on the Arch; con-

sequently, if the first division of the Nonius marked 0, be set precisely opposite to any degree, the relative position of the Nonius and the Arch must be altered one minute before the next division on the Nonius will coincide with the next division on the Arch, the second division will require a change of 2 minutes, the third of 3 minutes, and so on, till the 20th stroke on the Nonius arrives at the next 20 minutes on the Arch; the 0 on the Nonius will then have moved exactly 20 minutes from the division whence it set out, and the intermediate divisions of each minute, have been regularly pointed out by the divisions of the Nonius.

The divisions of the Nonius scale are in the above case reckoned from the middle towards the right, and from the left towards the middle; therefore the first 10 minutes are contained on the right of the 0, and the other 10 on the left. But this method of reckoning the divisions being found inconvenient, they are more generally counted, beginning from the right-hand towards the left; and then 20 divisions on the Nonius are equal to 19 on the limb, consequently one division on the Arch will exceed one on the Nonius by one-twentieth part, that is, one minute.

The 0 on the Nonius, points out the entire degrees and odd twenty minutes subtended by the objects observed; and if it coincides with a division on the Arch, points out the required angle: thus, suppose the 0 on the Nonius stands at 25 degrees, then 25 degrees will be the measure of the angles observed; if it coincides with the next division on the left hand, 25 degrees 20 minutes is the angle; if with the second division beyond 25

degrees, then the angle will be 25 degrees 40 minutes; and so on in every instance where the 0 on the Nonius coincides with a division on the Arch; but if it does not coincide, then look for a division on the Nonius that stands directly opposite. to one on the Arch, and that division on the Nonius gives the odd minutes to be added to that on the Arch nearest the right-hand of the 0 on the Nonius; for example, suppose the Index division does not coincide with 25 degrees, but that the next division to it on the Nonius is the first coincident division, then is the required Angle 25 degrees 1 minute; if it had been the second division, the Angle would have been 25 degrees 2 minutes,. and so on to 20 minutes, when the 0 on the Nonius would coincide with the first 20 minutes on the Arch from 25 degrees. Again, let us suppose the 0 on the Nonius to stand between 50 degrees and 50 degrees 20 minutes, and that the 15th division on the Nonius coincides with a division on the Arch, then is the angle 50 degrees 15 minutes. Further, let the 0 on the Nonius stand between. 45 degrees 20 minutes and 45 degrees 40 minutes, and at the same time the 14th division on the No-: nius stands directly opposite to a division on the Arch, then will the Angle be 45 degrees 34 minutes.

The Index Glass is a plane speculum, or mirror of glass quicksilvered, set in a brass frame, and so placed that the face of it is perpendicular to the plane of the instrument, and immediately over the centre of motion of the Index. This mirror being fixed to the Index moves along with it, and has its direction changed by the motion thereof.

This glass is designed to reflect the image of the Sun, or any other object, upon either of the two horizon glasses, from whence it is reflected to the

eye of the observer. The brass frame, with the glass, is fixed to the Index by the screw; the other screw serves to place it in a perpendicular position, if by any accident it has been put out of order.

The Horizon Glasses are two small speculums on the radius of the Octant; the surface of the upper one is parallel to the Index glass when the O on the Nonius is at 0 on the Arch; these mirrors receive the rays of the object reflected from the Index glass, and transmit them to the observer. The fore Horizon glass is only silvered on its lower half, the upper half being transparent, in order that the direct object may be seen through it. back Horizon glass is silvered at both ends; in the middle there is a transparent slit, through which the Horizon may be seen. Each of these glasses is set in a brass frame, to which there is an axis; this axis passes through the wood work, and is fitted to a lever on the under side of the quadrant, by which the glass may be turned a few degrees on its axis, in order to set it parallel to the Index glass.

To set the glasses perpendicular to the plane of the quadrant, there are two sunk screws, one before and one behind each glass: these screws pass through the plate on which the frame is fixed into another plate, so that by loosening one and tightening the other of these screws, the direction of the frame, with its mirror, may be altered, and thus be set perpendicular to the plane of the instrument.

The Dark Glasses, or Shades, are used to prevent the bright rays of the Sun, or the glare of the Moon, from hurting the eye at the time of observation; there are generally three of them, two red, and one green. They are each set in a brass frame

which turn on a centre, so that they may be used separately or together, as the brightness of the object may require. The green glass may be used also alone, if the Sun be very faint; it is likewise used in taking observations of the Moon; when these glasses are used for the fore observation, they are set immediately before the fore Horizon glass, but in front of the other Horizon glass, when a back observation is made.

The Sight Vanes are pieces of brass, standing perpendicular to the plane of the instrument: that one which is opposite the fore horizon, is called the fore Sight Vane, the other the back Sight Vane. There are two holes in the fore Sight Vane, the lower of which, and the upper edge of the silvered part of the fore Horizon glass, are equidistant from the plane of the instrument, and the other is opposite to the middle of the transparent part of that glass; the back Sight Vane has only one hole, which is exactly opposite to the middle of the transparent slit in the Horizon glass to which it belongs: but as the back observations are liable to many inconveniences and errors, we shall not give any directions for their practice.

ADJUSTMENTS.

The several parts of the Quadrant being liable to be out of order from a variety of accidental circumstances, it is necessary to examine and adjust them, so that the instrument may be put into a proper state, previous to taking observations.

An instrument properly adjusted, must have the Index glass and Horizon glasses perpendicular to the plane of the Quadrant; the plane of the fore Horizon glass parallel, and that of the back Hori-

zon glass perpendicular to the plane of the Index glass, when the 0 on the Nonius is at 0 on the Arch; hence the Quadrant requires five adjustments, the first three of which being once made, are not so liable as the last two to be out of order; however they should all be occasionally examined in case of an accident.

I. To set the Plane of the Index Glass perpendicular to that of the Instrument.

Place the Index near to the middle of the Arch, and holding the Quadrant in a horizontal position, with the Index glass close to the eye, look obliquely down the glass, in such a manner that you may see the Arch of the Quadrant by direct view, and by reflection at the same time; if they join in one direct line, and the Arch seen by reflection forms an exact plane, or strait line, with the Arch seen by direct view, the glass is perpendicular to the plane of the Quadrant; if not, it must be restored to its right position by loosening the screw, or tightening it, or vice versa, by a contrary operation.

II. To set the Fore Horizon Glass parallel to the Index Glass, the Index being at 0.

Set the 0 on the Nonius exactly against 0 on the Arch, and fix it there by the screw at the under side. Then, holding the Quadrant vertically, with the Arch lowermost, look through the Sight Vane, at the edge of the sea, or any other well defined and distant object. Now, if the Horizon in the silvered part exactly meets, and forms one continued line with that seen through the unsilvered part, the Horizon glass is parallel to the Index glass. But if the Horizons do not coincide.

then loosen the button-screw in the middle of the lever, on the under side of the Quadrant, and move the Horizon glass on its axis, by turning the nut at the end of the adjusting lever, till you have made them perfectly coincide; then fix the lever firmly in this situation by tightening the buttonscrew. This adjustment ought to be repeated before and after every observation. Some observers adopt the following method, which is called finding the Index error. Let the Horizon glass remain fixed, and move the Index till the image and object coincide; then observe whether 0 on the Nonius agrees with 0 on the Arch, if it does not, the number of minutes by which they differ is to be added to the observed altitude or angle, if the 0 on the Nonius be to the right of the 0 on the Arch, but if to the left of the 0 on the limb, it is to be subtracted.

It has already been observed, that that part of the Arch beyond 0, towards the right hand, is called the Arch of excess: the Nonius, when the 'O on it is at that part, must be read the contrary way, or which is the same thing, you may read off the minutes in the usual way, and then their complement to 20 minutes will be the real number, to be added to the degrees and minutes pointed out by the 0 on the Nonius,

III. To set the Fore Horizon Glass perpendicular to the Plane of the Quadrant.

Having previously made the above adjustment, incline the Quadrant on one side as much as possible, provided the Horizon continues to be seen in both parts of the glass; if when the instrument is thus inclined, the edge of the sea seen through the lower hole of the Sight Vane continues to form

fectly adjusted; but if the reflected Horizon be separated from that seen by direct vision, the speculum is not perpendicular to the plane of the Quadrant: then if the limb of the Quadrant is inclined towards the Horizon, with the face of the instrument upwards, and the reflected sea appears higher than the real sea, you must slacken the screw before the Horizon glass, and tighten that which is behind it; but if the reflected sea appears lower, the contrary must be performed. Care must be always taken in this adjustment to loosen one screw before the other is screwed up, and to leave the adjusting screws tight, or so as to draw with a moderate force against each other.

This adjustment may be also made by the Sun, Moon, or a Star; in this case the Quadrant is to be held in a vertical position; if the image seen by reflection appears to the right or left of the object seen directly, then the glass must be adjusted as before by the two screws.

It will be necessary, after having made this adjustment, to examine if the Horizon glass still continues to be parallel to the Index glass, as sometimes by turning the sunk screws the plane of the Horizon glass will have its position altered.

USE OF HADLEY'S QUADRANT.

The use of the Quadrant is to ascertain the Angle subtended by two distant objects at the eye of the observer; but principally to observe the altitude of a celestial object above the Horizon: this is pointed out by the Index when one of the

SS

objects seen by reflection is made to coincide with the other, seen through the transparent part of the Horizon glass.

To take an Altitude of the Sun, Moon, or a Star, by a Fore Observation.

Having previously adjusted the instrument, place the 0 on the Nonius opposite to 0 on the Arch, and turn down one or more of the screens, according to the brightness of the Sun; then apply the eye to the upper hole in the fore Sight Vane, if the Sun's image be very bright, otherwise to the lower, and holding the Quadrant vertically, look directly towards the Sun so as to let it be behind the silvered part of the Horizon glass, then the coloured Sun's image will appear on the speculum; move the Index forward till the Sun's image, which will appear to descend, just touches the Horizon with its lower or upper limb; if the upper hole be looked through, the Sun's image must be made to appear in the middle of the transparent part of the Horizon, but if it be the lower hole, hold the Quadrant so that the Sun's image may be bisected by the line joining the silvered and transparent parts of the Horizon glass.

The Sun's limb ought to touch that part of the Horizon immediately under the Sun, but as this point cannot be exactly ascertained, it will be therefore necessary for the observer to give the Quadrant a slow motion from side to side, turning at the same time upon his heel, by which motion the Sun will appear to sweep the Horizon, and must be made just to touch it at the lowest part of the Arch; the degrees and minutes then pointed out by the Index on the Limb of the Quadrant will be the observed altitude of that limb which is brought in contact with the Horizon.

When the meridian or greatest altitude is required, the observation should be commenced a short time before the object comes to the meridian; being brought down to the Horizon, it will appear for a few minutes to rise slowly; when it is again to be made to coincide with the Horizon by moving the Index forward; this must be repeated until the object begins to descend, when the Index is to be secured, and the observation to be read off.

From this description of the Quadrant and its use, the manner of adjusting and using the Sextant will be readily apprehended. Our limits will not allow a particular description of this excellent instrument.

The Artificial Horizon.

In many cases it happens that altitudes are to be taken on land by the Quadrant or Sextant; which, for want of a natural horizon, can only be obtained by an artificial one. There have been a variety of these sorts of instruments made, but the kind now described is allowed to be the only one that can be depended upon. It consists of a wood or metal framed roof, containing two true parallel glasses of about 5 by 21 inches, fixed not too tight in the frames of the roof. This serves to shelter from the air a wooden trough filled with quicksilver. In making an observation by it with the Quadrant, or Sextant, the reflected image of the sun, moon, or other object, is brought to coincide with the same object reflected from the glasses of the Quadrant or Sextant: half the angle shown upon the limb is the altitude above the horizon or level required. It is necessary in a set of observations that the roof be always placed the same way. When done with, the roof folds up flatways, and, with the quicksilver in a bottle. &c. is packed into a portable flat case,

SECTION III.

To find the Latitude by the Meridian Altitude of the Sun.

The Latitude of a place is its distance from the equator, either North or South; and is measured by an arch of a Meridian contained between the Zenith and the equinoctial. Hence, if the distance of any heavenly body from the Zenith, when on the Meridian, and its declination, or the number of degrees and minutes it is to the Northward, or Southward of the equinoctial, be given, the Latitude may thence be tound.

The Altitude of the Sun, observed by a Quadrant, or Sextant, requires four corrections in order to obtain the true altitude; these are:

the Semidiameter, Dip, Refraction, and Parallax.

By the Semidiameter of the Sun is meant the angle subtended by the distance from its centre to its apparent circumference. The quartity of this angle is given for every sixth day in the year in table 10.

The Dip of the Horizon is a vertical angle contained between a Horizontal plane passing through the eye of an observer, and a line drawn from his eye to the visible Horizon. This Dip is found in Table 8, when the visible horizon is formed by the apparent junction of the water and sky; but in Table 9, when land intervenes. In this case, the line that separates the land and water is used as the Horizon, and its distance from the observer must be duly estimated.

The Refraction of any celestial body is the difference between its apparent place, and that wherein it would be seen, if the space between the observer and object, was either a void, or of a uniform

density. Table 6 contains this Refraction.

That part of the heavens, in which an object appears, when viewed from the surface of the earth, is called its apparent place; and the point, wherein it would be seen, at the same instant, if viewed from the centre of the earth, is called its true place; the difference between the true and apparent places, is called the Parallax. The Sun's Parallax in Altitude is found in Table 7.

RULE

For finding the Latitude from the Sun's Meridian Altitude.

Having observed with the Quadrant, or Sextant, the altitude of the Sun's lower limb above the visible horizon,—or the line of separation of the land from the water, when that horizon is obstructed by land—add thereto the semidiameter, taken from table 10 at the given day of the month, or the one nearest to it, and from this sum subtract the

Dip, from table 8 or 9, corresponding to the height of the observer's eye above the surface of the water; and this result will be the apparent altitude of the Sun's centre. Then take the refraction from table 6, and the parallax from table 7, corresponding to this altitude, and the difference of these quantities, called the correction, being subtracted from the apparent altitude, the remainder will be the Sun's true altitude; the complement of which will be its zenith distance, north or south, according as the Sun bears south or north, at the time of observation.

When the observation has been made by bringing the Sun's image in the Quadrant, or Sextant, to a just coincidence with its image in an artificial horizon, half the angle shown on the instrument is the Sun's apparent altitude, which must be corrected by the corresponding refraction and parallax only, in order to obtain the true altitude.

Take the Sun's declination from table 13, answering to the given year, month, and day, observing whether it be north or south, and reduce it, as there directed, by the help of table 14, to the longitude of the place of observation. Then the sum, or difference of the zenith distance, and declination, according as they are of the same, or of a contrary denomination, will be the latitude of the place of observation, of the same name with the greater of those two quantities.

Latitude.

EXAMPLES.

1st. March 10th, 1811, in length 2d, May 10th, 1811, in long, 20 tude 70. Withe Mer Alt 11 of L. Wint men, the negative distributions I, was absented to be 1890 50 between the Decarring a physical bearing south-height of the our its reflected at ign in the artificial pers, i's eye 12 feet, required the live on was had a with a seatant to be 589 30' 10 triggmed the late-Mer Alt () L. L = 49° 50 00 S. tude 980 50' 40' +2=49' 15 20" Sem dameter O Ap Ait. Dux—table 8 -01 19 Correction Ap. Alt. = 50 0. 49 -42 Correction True Alt. - 49 11 7 56 02 67 True Alt Zenith Dist. Reduced Dec. - 17 Zenith Dist. = 39 57 13N Reduced Dec. 4 15 1965. Latitude. = 38 15 37 N

55 42 24N.

3d. July 24th, 1811, in burg 62° Ith. October 11th, 1812, in long. 39' W, the Mer. Alt of O L. L. 91" W the Meridian Mutude of above the breder of a like was (2) L. L. acove the vision because observed, by a person on the ap-was observed to be 47. 13 twerpoint al. re. to be \$67.52 bear mig 5, the height of the eve living
ing 5—the doctors of that boy 25 feet, required the latitude
der of the lake beneath the sun Mon Alt. © L. L. = 679. 15. 00° 5,
being 3 miles from the observer, beindismeter == 4. 16. 04
and the height the water, 8 feet;
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The sarrace of the water, 8 feet; Ap. Alt required he latitude.
Mor. Alt. ...) L. L. =560 32' 90' S. Correction Semoliameter True Ait Dip from table 9 = = 56 45 14 Ap. Alt. Correction Zenith Dist. =41 Reduced Dec-**= 55 44 39** True Alt. Latitude Zennih Dist = 33 15 21 N thoda of finding the lautude by Reduced Dec. = 19 59 46 N observat, a the strict of establishment by the books professed of practical a method of observing the lautuale by the aim do not be north that the real test and the lautuale by the aim do not be north. star, in the explanation of table 12, movemed to this treatise

SECTION IV.

VARIATION OF THE COMPASS.

The variation of the compass is the deviation of the points of the mariner's compass from the corresponding points of the horizon, and is termed east or west variation, according as the magnetic needle, or north point of the compass, is inclined to the eastward or westward of the true north point of the horizon.

The true amplitude of any celestial object is an arch of the horizon contained between the true east or west points thereof, and the centre of the object at the time of its rising or setting; or it is the degrees and minutes, the object rises or sets to the northward or southward of the true east or west points of the horizon.

The magnetic amplitude, is an arch contained between the east or west points of the compass and the centre of the object at rising or setting; or it is the bearing of the object, by compass, when in

the horizon.

The true azimuth of an object is an arch of the horizon contained between the true meridian and the azimuth circle passing through

the centre of the object.

The magnetic azimuth, is an arch contained between the magnetic meridian and the azimuth circle passing through the centre of the object; or it is the bearing of the object, by compass, at any time when it is above the horizon-

The true amplitude, or azimuth, is found by calculation, and the

magnetic amplitude, or azimuth, by an azimuth compass.

THE AZIMUTH COMPASS.

From the accounts of the compasses, heretofore given in the description of surveying instruments, it is presumed that the nature and properties of the azimuth compass will be readily conceived by a contemplative inspection; the directions for its uses are as follow:

To observe the Sun's amplitude.

Turn the compass-box until the vane containing the magnifying glass is directed towards the sun: and when the bright speck, or rays of the sun collected by the magnifying glass, falls upon the slit in the other vane, stop the card by means of the nonius, and read off the amplitude.

Without using the magnifying-glass, the sight may be directed through the dark glass towards the sun; and in this case, the card is to be stopped when the sun is bisected by the thread in the other

wane.

The observation should be made when the sun's lower limb appears somewhat more than his semidiameter above the horizon, because his centre is really then in the horizon, although it is ap-

parently elevated on account of the refraction of the atmosphere: this is particularly to be noticed in high latitudes.

To observe the Sun's Azimuth.

Raise the magnifying-glass to the upper part of the vane, and move the box, as before directed, until the bright speck fall on the other vane, or on the line in the horizontal bar; the card is then to be stopped, and the divisions being read off, will be the sun's magnetic azimuth.

If the card vibrate considerably at the time of observation, it will be better to observe the extreme vibrations, and take their mean as the magnetic azimuth. When the magnetic azimuth is observed, the altitude of the object must be taken, in order to obtain the true azimuth.

It will conduce much to accuracy if several azimuths be observed, with the corresponding altitudes, and the mean of the whole taken for the observation-

To find the variation of the Compass by an amplitude.

RULE—1. To the log. secant of the latitude, rejecting the index, add the log. sine of the sun's declination, corrected for the time and place of observation; their sum will be the log. sine of the true amplitude, to be reckoned from the east in the morning, or the west in the afternoon, towards the north or south, according to the declination.

2. Then if the true and magnetic amplitudes, be both north or both south, their difference is the variation; but if one be north and the other south, their sum is the variation; and to know whether it be easterly or westerly, suppose the observer looking towards that point of the compass representing the magnetic amplitude: then if the true amplitude be to the right hand of the magnetic amplitude, the variation is east, but if to the left hand, it is west.

EXAMPLE I.

July 3, 1812, in latitude 90 86' S. the Sun was observed to rise E 320 42' N: required the variation of the compass.

Latitude 9° 36′ S. - Secant 0.00613 Declination 22 59 N. - Sine 9.59158

True amplitude F. 23 20 N. - Sine 9.59771 Mag. amplitude E. 12 42 N.

Variation - 10 38 west, because the true amplitude is to the left of the magnetic.

EXAMPLE II.

September 24, 1812, in latitude 26 32' N. and longitude 78 W. the Sun's centre was observed to set W. 60 15' S. about 6h. P. M. required the variation of the compass.

0º 30' S. Sun's declination Corr. for long. 78° W. 5 Corr. for time 6h. P. M. 0 41 Reduced declination Sine 8.07650 Latitude 26 32 Secant 0.04834 Sine W. 0 46 S. True amplitude 81.2484 W. 6 158 Mag. amplitude

Variation 5 29 east, because the true amplitude is to the right hand of the magnetic.

To find the Variation of the Compass by an Azimuth

RULE. 1.—Reduce the Sun's declination to the time and place of observation, and compute the true altitude of the Sun's centre.

2. Subtract the Sun's declination from 90°, when the latitude and declination are of the same name, or add it to 90°, when they are of contrary names; and the sum, or remainder, will be the Sun's polar distance.

3. Add together the Sun's polar distance, the latitude of the place, and the altitude of the Sun; take the difference between half their sum and the

polar distance, and note the remainder.

4. Then add together

the log. secant of the altitude \rejecting their the log. secant of the latitude \rightarrow indices.

the log. co. sine of the half sum, and the log. co. sine of the remainder.

- 5. Half the sum of these four logarithms will be the sine of an arch, which doubled, will be the Sun's true azimuth; to be reckoned from the south in north latitude, and from the north in south latitude: towards the east in the morning, and towards the west in the afternoon.
- 6. Then if the true and observed azimuths be both on the east, or both on the west side of the meridian, their difference is the variation: but if one, be on the east, and the other on the west side of the meridian, their sum is the variation; and to know if it be east or west, suppose the observer looking towards that point of the compass representing the magnetic azimuth; then if the true azimuth be to the right of the magnetic, the variation is east, but if the true be to the left of the magnetic, the variation is west.

November 2, 1812, in latitude 25° 32′ N. and longitude 75° W. the altitude of the Sun's lower limb was observed to be 15° 36′, about 4h. 10m. P. M. his magnetic azimuth at that time being S. 58° 32′ W. and the height of the eye 18 feet; required the variation of the compass.

Sun's de. Nov. 2, at n. 140 48' S. Obs. alt. Sun's lower limb 150 68' Cerr. for long. 75° W. + Semidiameter Co. for ti. 4h. 10m. af. n. + Reduced declination 15 48 14 55 Refraction 90 00 True altitude 15 45 Polar distance 104 55 Altitude Secant 0-01662 **15 45** Latitude Secant 0.04463 25 32 **146** 12 Half Co. sine 9.46845 **73** 6 Remainder Co. sine 9.92929 31 49 32 14 19.45399

True azimuth S. 64 28 W, Mag. azimuth S. 58 32 W.

Variation - 5 56 east, because the true azimuth is to the right of the magnetic.

9.72699

Sine

To draw a true meridian line to a map, having the variation and magnetical meridian given.

On any magnetical meridian or parallel, upon which the map is protracted, set off an angle from the north towardathe east, equal to the degrees or quantity of variation, if it be westerly, or from the north towards the west, if it be easterly, and the line which constitutes such an angle with the magnetical meridian, will be a true

meridian line.

For if the variation be westerly, the magnetical meridian will be the quantity of variation of the west side of the true meridian, but if easterly, on the east side; therefore the true meridian must be a like quantity on the east side of the magnetical one, when the variation is westerly, and on the west side when it is easterly.

To lay out a true meridian line by the circumferentor.

If the variation be westerly, turn the box about till the north of the needle points as many degrees from the flower-de-luce towards the east of the box, or till the south of the needle points the like number of degrees from the south towards the west, as are the number of degrees contained in the variation, and the index will be then due north and south: therefore if a line be struck out in the direction thereof, it will be a true meridian line.

If the variation was easterly, let the north of the needle point as many degrees from the flower-de-luce towards the west of the box. or let the south of the needle point as many degrees towards the east, as are the number of degrees contained in the variation, and then the north and south of the box will coincide with the north and south points of the horizon, and consequently a line being laid out by

the direction of the index, will be a true meridian line.

This will be found to be very useful in setting an horizontal dial, for if you lay the edge of the index by the base of the stile of the dial, and keep the angular point of the stile toward the south of the box, and allow the variation as before, the dial will then be due north and south, and in its proper situation, provided the plane upon which it is fixed be duly horizontal, and the sun be south at noon; but in places where it is north at noon, the angular point of the index must be turned to the north.

How maps may be traced by the help of a true meridian line.

If all maps had a true meridian line laid out upon them, it would be easy by producing it, and drawing parallels, to make out fieldnotes; and by knowing the variation, and allowing it upon every bearing, and having the distances, you would have notes sufficient for a trace. But a true meridian line is seldom to be met with, therefore we are obliged to have recourse to the foregoing method. It is therefore advised to lay out a true meridian line upon every map.

To find the difference between the present variation, and that at a time when a tract was formerly surveyed, in order to trace or run out the original lines.

If the old variation be specified in the map or writings, and the present be known, by calculation or otherwise, then the difference is immediately seen by inspection; but as it more frequently happens, that neither is certainly known, and as the variation of different instruments is not always alike at the same time, the following prac-

tical method will be found to answer every purpose.

Go to any part of the premises where any two adjacent corners are known; and, if one can be seen from the other, take their bearing; which, compared with that of the same line in the former survey, shows the difference. But if trees, hills, &c obstruct the view of the object, run the line according to the given bearing, and observe the nearest distance between the line so run and the corner, then,

As the length of the whole line
Is to 57.3 degrees,*
So is the said distance
To the difference of variation required.

EXAMPLE.

Suppose it be required to run a line which some years ago bore NE 45°, distance 80 perches, and in running this line by the given bearing, the corner is found 20 links to the left hand; what allowance must be made on each bearing to trace the old lines, and what is the present bearing of this particular line by the compass?

Answer, 34 minutes; or a little better than half a degree to the left hand, is the allowance required, and the line in question bears N. 440 26. E.

Note. The different variations do not affect the area in the calculation, as they are similar in every part of the survey.

* 57.3 Is the radius of a circle (nearly) in such parts as the circumference contains 360.

TABLE L

LOGARITHMS OF NUMBERS.

EXPLANATION.

OGARITHMS are a series of numbers so contrived, that the sum of the Logarithms of any two numbers, is the logarithm of the product of these numbers. Hence it is inferred, that if a rank, or series of numbers in arithmetical progression, be adapted to a series of numbers in geometrical progression, any term in the arithmetical progression will be the logarithm of the corresponding term in the geometrical progression.

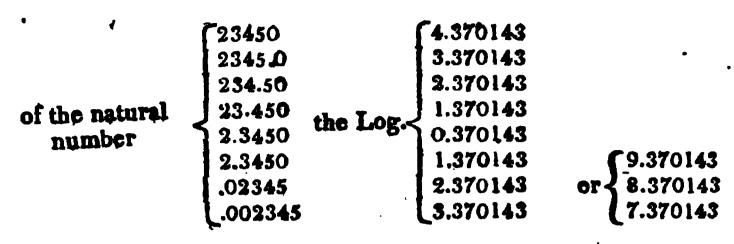
This table contains the common logarithms of all the natural numbers from 0 to 10000, calculated to six decimal places; such, on account of their superior accuracy, being preferable to those, that are

computed only to five places of decimals.

In this form, the logarithm of 1 is 0, of 10, 1; of 100, 2; of 1000, 3 &c. Whence the logarithm of any term between 1 and 10, being greater than 0, but less than 1, is a proper fraction, and is expressed decimally. The logarithm of each term between 10 and 100, is 1, with a decimal fraction annexed; the logarithm of each term between 100 and 1000 is 2, with a decimal annexed, and so on. The integral part of the logarithm is called the Index, and the other the decimal part.—Except in the first hundred logarithms of this Table, the Indexes are not printed, being so readily supplied by the operator from this general rule; the Index of a Logarithm is always one less than the number of figures contained in its corresponding natural number—exclusive of fractions, when there are any in that number.

The Index of the logarithm of a number, consisting in whole, or in parts, of integers, is affirmative; but when the value of a number is less than unity, or 1, the index is negative, and is usually marked by the sign, —, placed either before, or above the index. If the first significant figure of the decimal fraction be adjacent to the decimal point, the index is 1,— or its arithmetical complement 9; if there is one cipher between the decimal point and the first significant figure in the decimal, the index is — 2, or its arith. comp. 8; if two ciphers, the index is — 3, or 7, and so on; but the arithmetical complements, 9, 8, 7 &c. are rather more conveniently used in trigonometrical calculations.

The decimal parts of the logarithms of numbers, consisting of the same figures, are the same, whether the number be integral, fractional, or mixed: thus,



N. B. The arithmetical complement of the logarithm of any number, is found by subtracting the given logarithm from that of the radius, or by subtracting each of its figures from 9, except the last, or right-hand figure, which is to be taken from 10. The arithmetical complement of an index is found by subtracting it from 10.

PROBLEM I.

To find the logarithm of any given number.

RULES.

1. If the number is under 100, its logarithm is found in the first page of the table, immediately opposite thereto.

Thus the Log. of 53, is 1.724276.

2. If the number consists of three figures, find it in the first column of the following part of the table, opposite to which, and under 0, is its logarithm.

Thus the Log, of 384 is 2.584331—prefixing the index 2, because

the natural number contains 3 figures.

Again the log. of 65.7 is 1.817565—prefixing the index 1, because there are two figures only in the integral part of the given number.

3. If the given number contains four figures, the three first are to be found, as before, in the side column, and under the fourth at the top of

the table is the logarithm required.

Thus the log. of 8735 is 3.941263—for against 873, the three first figures found in the left side column, and under 5, the fourth figure found at the top, stands the decimal part of the logarithm, viz .941263, to which prefixing the index, 3, because there are four figures in the natural number, the proper logarithm is obtained.

Again the logarithm of 37.68 is 1.576111—Here the decimal part of the logarithm is found, as before, for the four figures; but the index is 1, because there are two integral places only in the natural number.

4. If the given number exceeds four figures, find the difference between the logarithms answering to the first four figures of the given number, and the next following logarithm; multiply this difference by the remaining figures in the given number, point off as many figures to the right-hand as there are in the multiplier, and the remainder, add-

et to the logarithm, answering to the first four figures, will be the required logarithm, nearly.

Thus; to find the logarithm of 738582;
the log. of the first four figures, viz. 7385 .868350
the next greater logarithm = 868409

to be multiplied by the remaining figures = 82

118
472

then to .868350 add 48

the sum 5.868398, with the proper index prefixed, is the required logarithm.

5. The logarithm of a vulgar-fraction is found by subtracting the logarithm of the denominator from that of the numerator; and that of a mixed quantity is found by reducing it to an improper fraction, and proceeding as before.

Thus to find the Logarithm of 7; from the log. of 7 = 0.845098 subtract the log. of 8 = 0.903090

Remainder = 9.942008 = the required log.

PROBLEM II.

To find the number answering to any given logarithm.

RULES.

1. Find the next less logarithm to that given in the column marked o at the top, and continue the sight along that horizontal line, and a logarithm the same as that given, or very near it, will be found; then the three first figures of the corresponding natural number will be found opposite thereto in the side column, and the fourth figure immediately above it, at the top of the page. If the index of the given logarithm is 3, the four figures thus found are integers; if the index is 2, the three first figures are integers, and the fourth is a decimal, and so on.

2. If the given logarithm cannot be exactly found in the table, and if more than four figures be wanted in the corresponding natural number; then find the difference between the given and the next less loga-

rithms, to which annex as many ciphers as there are figures required above four in the natural number; which—divide by the difference between the next less, and next greater logarithms, and the quotient annexed to the four figures formerly found, will give the required natural number.

Thus to find the natural number of the log. 4.828991; the next less log. is .828982 which gives 6735; the next greater log. is 829046

Dif. = 60
next less log. = 828982
given log. = 828991

Dif. with one e annexed = 90 then 64) 90 (1.4

260 256

therefore 1.4 being annexed to 6735, the required natural number, 67351.4, is now obtained.

TABLE I.

LOGARITHMS OF NUMBERS.

i	No.	Log.	No.	Log.	No.	Log.	No.	Log.	No.	Lo
	1	0.000000	21	1.322219	.41	1.612784	61	1.785350	81	1.908485
	2	0.301030	22	1.342423	42	1.623249	62	1.792392	82	1.913814
	3	0.477121	23	1.361728	43	1.633468	63	1.799341	83	1.919078
ı	4	0.602060	24	1.380211	44	1.643453	64	1.806180	84	· 1.924279
٠	_ 5_	0.698970	25	1.397940	45	1.653213	65	1.8,12913	85	1.929419
ı	6	0.778151.	26	1.414973	46	1.662758	66	1.819544	86	I.934498
ı	7	0.845098.	27	1.431364	47	1-672098	67	1.826075	87	1.939519
ı	8	0.903090	28	1-447158	48	1.681241	68	1.832509	88	1.944483
1	9	0.954243	29	1.462398	49	1.690196	69	1.838849	89	1.949390
ı	10	1.000000	30	1.477121	50	1.698970	70	1.845098	90	1.954243
I	11	1.041393	31	1.491362	51	1.707570	71	1.851258	10'	1.959041
ı	12	1.079181	32	1.505150	52	1.716003	72	1.857332	92	1.963788
I	13	1.113943	33	1.518514	53	1.724276	73	1.863323	93	1.968483
ł	14	1.146128	34	1.531479	54	1.732394	74	1.869232	94	1.973128
ı	15	1.176091	35	1.544068	55	1.740363	75	1.875061	95	1.977724
	16	1.204120	36	1.556302	.56	1.748188	76	1.880814	96.	1.982271
ł	17	1.230449	37	1.568202	57	1.755875	77	1.886491	97	1.986772
ı	18	1.255273	38	1.579784	. 58	1.763428	78	1.892095	98	1.991226
Į	19	1.278754	39	1.591065	59	1.770852	79	1.897627	99	1-995635
Į	20	1.303030	40	1.602060	60	1.778151	1 80	1.903090	100	2.000000

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101	004321	004751	005180	005609	006038	006466	006894	007321	007748	008174
103	008600	009200	009451	009876	010300	010724	011147	1011570	011993	01241
103	012037	.013259 .017461	868210	018284	014520	014940	015300	015779	016197 020361	010013
•	021189	021603	022016	022428	022841	021252	023664	024075	024486	024896
106	025306	025715	026124	026533	026942	027350	027757	028164	028571	028978
107	029384	029789	030195	030600	031004	031408	031812	032216	032619	033021
108	033424	033826	034227	034628	035029	035430	035830	036229	036629	037028
109						-			040602	
111	041393	041787	042182	042575	042009	043362	043755	044148	044540	044931
	045343	040606	040003	040495	040005	047275	047004	051034	048442	040030
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114									059942	
	060698	061075	061452	061829	062206	062582	062958	063333	063709	064083
116	064458	064832	065206	065580	065953	066326	066699	067071	067443	067814
117									071145	
119									074816	
120									082067	
121									085647	
122									089198	
123									092721	
124	093422	093772	094122	094471	094820	095169	095518	095866	096215	096562
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133									126456	
134									129690	
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137									139249	
138	139879	140194	140508	140822	141136	141450	141763	142076	142389	142702
139	149015	143327	143639	143951	144263	144574	144885	145196	145507	145818
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145									163757	
146	164353	164650	164947	165244	165541	165838	166134	166430	166726	167022
147	167317	167613	167908	168203	168497	168792	169086	169380	169674	169961
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153									186956	
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940						973359				
941						973820 974281				
942 943	07451	974558	974604	974650	974696	974742	974788	974834	97488C	97492
944	974972	975018	975064	975110	975156	975202	975248	975294	975340	97538
945	975432	975478	975524	975570	975616	975661	975707	975753	975799	97584
946 947						976121 97 6 579				
948	976808	976854	97 690 0	976946	976991	977037	977083	977129	977175	97722
949	977266	977312	977358	977403	977449	977495	977541	977586	977632	97767
950	977724	977769	977815	977861	977906	977952	977998	978043	978089	97813
951	078627	978220	970272	974317	978810	978409 978865	9/0454	978956	970540	97004
953	979093	979138	479184	979230	979275	979321	979366	979412	979457	97950
954	979548	979594	979639	979685	979730	979776	979821	979867	979912	97495
955	980003	980049	980094	980140	080640	980231 980685	980270	980322	980307	98081
956	980450	9800503	981003	981048	981003	981139	981184	981220	951275	98132
958	1081365	981411	981456	981501	981547	981592	981637	981683	981728	98177
959	981819	981864	981909	981954	982000	982045	982090	982135	982181	98222
960	981271	982316	982362	982407	982452	982497	982543	982588	982633	98267
961 962	082176	082220	982266	982210	982366	982949 983401	983446	9834G1	983536	98358
963	983626	983671	983716	983762	983807	983852	983897	983942	983987	y8403:
964	084077	984122	984167	984212	984257	984302	984347	984392	984437	98448
	984527	984572	984017	984662	984707	984752 98 52 02	984797	984842	985237	08518
966 967	985426	985022	985516	985561	985606	985651	985696	985743	985786	985831
968	985875	985920	985965	986010	986055	986100	986144	986189	986234	98627
969						986548				
970	986772	986816	986861	986906	986951	986995 987443	987040	987085	087577	08762
971	087666	087711	987756	987800	987845	987890	987934	987979	988024	98806
973	988113	088157	988202	988247	988291	988336	988381	988425	988470	988511
974	988559	988603	988648	988693	908737	988782	988826	988871	988915	98896
975	989005	989049	080 5 20	080484	080628	989227 98 9672	989717	080761	989806	989850
977	080895	989939	989983	990028	990072	990117	990161	990206	990250	990291
978	990339	990383	990428	990472	990516	990561	990605	990650	990094	990731
979						991004				
980	991226	991270	991315	991359	991403	991448 ₁ 991890:	991492	991530	991500	99102
981	002111	002156	992200	992244	992288	992333	992377	992421	992405	992509
983	002553	992598	992642	992686	992730	992774	992818	992863	992907	99295
984	992995	993039	993083	993127	993172	993 2 16 993657	993200	993304	993348	99339
985	003877	003021	993965	994009	994053	994097!	994141	994185	994229	99427:
987	1994317	994361	994405	994449	994493	994537	994581	994025	994069	9 94 71.
988	1994757	994801	994845	994889	994933	99 49 77	995021	995004	945100	772.2
989						995416				
991	1995035	995079	995723	9957 9 7	995011	995854 996293	996336	337342	996424	99646
992	1006612	aabeee	96599	1996643	996687	996730	990774	996818	996862	199090
993	1006040	999993	997037	1997080	997124	997108	997212	9972551	1997299	1 9 973 4 .
994	997386	997430	997474	997517	997501	997605 998041	997048	997092	997730	99///!
995	1008250	008 101	498346	1008300	998434	1998477	998521	1998504	1999000	199005:
997	1008604	008770	998782	1998826	1998869	998913	998950	1999000	999043	199909
998	1999130	999174	999218	999 201	999305	99 93 48 999783	999392 994826	999435	999478	99952 000051
3.30		999009	999052	3	4	5	999020	7	8	4
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TABLE 2.

Logarithmic Sines, Tangents, and Secants.

This table contains the logarithmic, or, as they are sometimes called, the artificial sines, tangents, and secants, to each degree and minute of the quadrant, with their complements or co-sines, co-tangents, and co-secants, to six places of figures besides the index.

To find the Logarithmic Sine, Co-Sine, &c. of any Number of Degrees and Minutes.

If the given degrees be under 45, they are to be taken from the top, and the minutes f om the left side column, opposite to which in that column with the name of the logarithm at the top, will be found the required logarithm. But if the degrees be more than 45, they will be found at the bottom of the page, and the minutes in the right side column; likewise the name of the logarithm is to be taken from the bottom of the page.

When the given degrees exceed 90, they are to be subtracted from 180 degrees, and the logarithm of the remainder taken out as before. Or the logarithmic sine, tangent, &c. of degrees more than 90, is the logarithmic co-sine, co-tangent, &c. of their excess above 90 degrees.

BXAMPLES.

			•	•		logarithm:
Require	ed the	log. sine of	36	32	-	9.774729
•	•	co-sine of	61	18	•	9.681443
•	-	tangent of	54	17	•	10 143263
-	-	co-tang. of	42	50	•	10.03287 7
-	-	secant of	19	27	•	10.025519
•	-	co-secant of	70	33	•	10.025519
•	4	sine of	108	36		•
-	or	sine of	71	24	•	9.976702
•	Or	co-sine of	18	36		·

To find the Degrees and Minutes nearest corresponding to a gives Logas rithmic Sine, Co-sine, &c.

Look in the column marked at the top or bottom with the name of the given logarithm, and when the nearest to it is found, the corresponding degrees and minutes will be those required. observing that when the name is at the top of the column, the degrees are to be taken from the top and the minutes from the left side column, but if the name is at the bottom, the corresponding degrees will be there likemes, and the minutes in the right side column.

EXAMPLES.

The degrees and minutes corresponding to the

log. sine	9.265390	are	100	37'
co-sine				
tangent	9.70156		26	
O 1	10.25413		5 6	· 9

The logarithmic sines, &c. taken out to degrees and minutes only are in general sufficiently accurate, but in some of the more rigid astronomical calculations, it is frequently necessary to take them out to the nearest second; when this is the case they are to be found in the following manner:

To find the sine, tangent, &c. of an arch expressed in degrees, minutes and seconds.

RULE.

Find the sine, tangent, &c. answering to the given degree and minute, and also that answering to the next greater minute; multiply the difference between them by the given number of seconds, and divide the product by 60; then, the quotient added to the sine, tangent, &c. of the given degree and minute, or subtracted from the co-sine, co-tangent, &c. will give the quantity required, nearly.

If the arch be less than three degrees, it will be necessary to use the

following rule ---

To the arithmetical complement of the given degrees and minutes reduced to seconds, add the logarithm of the given degrees, minutes, and seconds, reduced to seconds, and the log.-sine, tangent, &c. of the given degrees and minutes, the sum, rejecting 10 from the index, will be the log.-sine, tangent, &c. of the proposed number of degrees, minutes, and seconds.

To find the degrees, minutes, and seconds, answering to a given logarithmic sine, tangent, &c.

RULE.

Find the degrees minutes and seconds answering to the next less logazithmic sine, tangent, &c. which subtract from that given; multiply the remainder by 60, and divide the product by the difference between the next less and next greater logarithms, and the quotient will be the seconds to be annexed to the degrees and minutes before found.

If the given logarithm is that of the sine or tangent of a small arch—then, to the arithmetical complement of the next less logarithm in the tables, add the given logarithm, and the logarithm of the degrees and minutes, in seconds, answering to the next less logarithm, the sum, rejecting radius, will be the logarithm of the number of seconds in the required arch.

Sine 0 Degree.

-		<u> </u>	مسندره والبراج والتراكيات	Degree.			
M	1 0"	10"	20"	30"	40"	50"	
0	-	5.685575	5.986605	6.162696	6.287635	6.384545	
1 1	6.463726	6.530673	6.488665	6.639817	6.685575	6.726967	59
	6.764756	6.799518	6.831703	6.861666	6.889695	6.916024	58
-	6.940847	6.964328	6.986605	7.007794	7.027997	7.047303	57
3	7.065786	7.083515	7.100548	7.116938	7.132733	,	_
4	7.162696	7.176936	7.190725	7.204089	7.217054	7.147973 7.229643	55
5	7.102090		7.265358	7.276639	7.287635	7.298358	54
2	7.308824	7.253776	7.329027	7.338787	7.348332	1	53
7 8	7.366816	7.319043	7.384544	•	7.401578	7.357672	52
•	7.417968	7-375770	7.433762	7-393145 7-441449	7.449002	7-456426	51
9		7.425937				The second lives and the second	50
10	7.463725	7.470904	7.477966	7.484915	7.491754	7.498487	49
11	7.505118	7.511649	7.518083	7.524423	7.530672	7.536832	48
12	7.542906	7.548897	7.554806	7.560635	7.566387	7.572065	47
13	7.577668	7.583201	7.5886 64	7.594059	7.599388	7.604652	46
14	7.609853	7.614993	7.620072	7.625093	7.630056	7.634963	45
16	7.639816	7.644615	7.649361	7.654056	7.658701	7.663297	44
15	7.667844	7.672345	. 7.676799	7.681208	7.685573	7.689894	43
17	7.694173	7.698410	7.702606	7.706762	7.710879	7.714957	43
18	7.718997	7.722999	7.726965	7.730896	7.734791	7.738651	41
19	7.743477	7.746270	7.750031	7-753758	7-757454	7.761119	40
20	7-764754	7.768358	7-771932	7-775477	7.778994	7.782482	39
21	7.785943	7.789376	7.792782	7.796162	7.799515	7.802843	38
22	7.806146	7.809423	7.812677	7.815905	7.819111	7.822292	37
23	7.825451	7.828586	7.831700	7.834791	7.837860	7.840907	36
24	7-843934	7.846939	7.849924	7.852888	7.855833	7.858757	35
25	7.861662	7.864548	7.867414	7.870262	7.873092	7.875902	34
26	7.878695	7.881470	7.884228	7.886968	7.889690	7.892396	33
27	7.895085	7.897758	7.900414	7.903054	7.905678	6.908287	32
28	7.910879	7.913457	7.916019	7.918566	7.921098	7.923616	31
29	7 926119	7 928608	7.931082	7-933543	7.935989	7.938422	30
30	7.940842	7.943248	7.945641	7.948020	7.950387		-
31	7.955082	7.943.40	7.959727	7.962031	7.964322	7.952741 7.966602	29 28
32	7.968870	7.971126	7.973370	7.975603	7.977824	7.980034	•
33	7.982233	7.984421	7.986598	7.988764	7.990919	7.993064	27 26
34	7.995198	7.997322	7.999435	8.001538	8.003631	8.005714	•
35	8.007787	8.009850	8.011903	8.013947	8.015981	8.018005	25 24
36	8.020021	8.022027	8.014023	8.026011	8.027989	8.029959	23
37	8.031919	8.033871	8.035814	8.037749	8.039675	8 041592	22.
38	8 043501	8.045401	8.047294	8.049178	8.051054	8 052922	21
39	8.054781	8.056633	8.058477	8.060314	8.062142	8.063963	20
•		-					
40	8.065776	8.067582	8.069380	8571171	8.072955	8.074731	19
41	8.076500	8.078261	8.0800.8	8.081764	8.083504	8.085238	18
42	8.086965	8.088684	8.090398	8.092104	8.093804	8.095497	17
43	8.097183	8.098863	8.100537	8.102204	8.103864	8.105519	16
44	8.107167	8.108809	8.110444	8.112074	8.113697	8.115315	15
45	8.116926	8.118532	8.120131	8.121725	8.123313	8.124895	14
46	8.126471	8.128042	8.129606	8.131166	8.132720	8.134268	13
47	8.135810	8.137348	8.138879	8.140406	8.141927	8.143443	12
48	8.144953	8.146458	8.147959 8.156852	8.149453 8.168216	8.150943	8.152428	11
49	8.153907	8.155382	-	8.148316	8.159776	8.161231	10
50	8.162681	8.164126	8 165566	8.167002	8.168433	8.169859	9
5t.	8.171280	8.172697	8.174109	8.175517	8.176920	8.178319	8
52	8.179713	8.181102	8.182488	8.183868	8.185245	8.186617	7
53	8.187985	8.189348	8.190707	8.192062	8.193413	8.194760	6
54	8.196102	8.197440	8.198774	8.200104	8.201430	8.202752	5
55	8.204070	8.205384	8.206694	8.208000	8.209302	8.210601	4
56	8.211895	8.213185	8.214472	8.215755	8.217034	8.218309	3
57	8.219581	8.220849	8.222113	8.223374	8.224631	8.225884	2
58	8.227133	8.228380	8.229622	8.230861	8.232096	8.233328	I
59	8.234557	8.235782	8.237003	8.238221	8.239436	8.240647	0
	6011	50''	40′′	30"	20′′	10"	M
ارسساد			Casine 10				

Se-sing 89 Degrees.

LOGARITHMIC TANGENTS.

Tangent O'Degree,

		,	Tangent	O Degree,			<u> </u>
M	0"	10"	20′	30.,	40"	50"	
0		5.685575	5.986605	6.162696	6.287635	6.384545	59
1	6.463726	6.530673	6.588665	6.639817	6.685575	6.726968	58
2	6.764756	6.799518	6.831703	6.861666	6.889695	6.916024	57
3	6.940847	6.964329	6.386605	7.007794	7.027998	7.047303	56
4	7.065786	7.083515	7.100548	7.116939	7-132733	7.147973	55
5	7.162696	7.176937	7.190725	7.204089	7.217054	7.229643	54
6	7.241878 7.308825	7.253777	7.265359	7.276640	7.287635	7.298359	53
7 8	7.366817	7.319044 7.375772	7.329028 7.384546	7.338788 7.393146	7·348333 7·401579	7.357673 7.409852	52 51
9	7.417970	7.425939	7.433764	7.441451	7.449004	7.456428	50
10		7.470906	7.477968	7.484917			49
111	7.463727 • 7.505120	7.511651	7.518085	7.524426	7.491756 7.530675	7.498490 7.536835	48
12	7.542909	7.548900	7.554808	7.560638	7.566390	7.572068	47
13	7.577671	7.583204	7.588667	7.594062	7.599391	7.604655	46
14	7.609857	7.614996	7.620076	7.625097	7.630060	7.634968	45
1.15	7.639820	7.644619	7.649366	7.654061	7.658706	7,663301	44
16	7.667849	7.672350	7.676804	7.681213	7.685578	7.689900	43
17	7.694179	7.698416	7.702612	7.706768	7.710885	7.714962	42
. 18	7.719003	7.723005	7.726972	7.730902	7-734797	7.738658	41
19	7.742484	7.746277	7.750037	7.753765	7.757462	7.761127	40
20	7.764761	7.768365	7.771940	7-775485	7.779002	7.782490	39
21	7.785951	7.789384	7.792790	7.796170	7.799524	7.802852	38
22	7.806155	7.809432	7.812686	7.815915	7.819120	7.822302	37
23	7.825460	7.828596	7.831710	7.834801	7.837870	7.840918	36
24	7.843944	7.846950	7.849935	7.852900	7.855844	7.858769	35
25 26	7.801074	7.864560 _* 7.881483	7.867426 7.884240	7.870274 7.88698 r	7.873104	7.875915	34
27	7.895099	7.897771	7.900428	7.903068	7.905692	7.892410 7.908301	·33
28	7.910894	7.913471	7.916034	7.918581	7.921113	7.923631	31
29	7.926134	7.928623	7.931098	7.933559	7.936006	7.938439	30
30	7.940858	7.943265	7-945657	7.948037	7.950404	7:952758	29
31	7.955100	7.957428	7.959745	7.902049	7.964341	7-966621	28
32	7.968889	7.971145	7.973389	7.975622	7.977844	7.980054	27
33	7.982253	7.984441	7.986618	7.988785	7.990940	7.993085	26
34	7.995219	7.997343	7.999456	8.001560	8.003653	8.005736	25
35	8.007809	8.009872	8.011926	8.013970	.8.016004	8.018029	24
36	8.020044	8.022051	8.024047	8.026035	8.028014	8.029984	23
37	8 03 1945	8.033897	8.035840	8.037779	8.039701	8.041618	22
38	8.043527	8.045428	8.047321	8.049205	8.051081	8.052949	21
39	8.054809	8.056661	8.058506	8.060342	8.062171	8.063992	20
40	8.065806	8,067612	8.069410	8.071201	8.072985	8.074761	19
41	8.076531	8.078293	8.080047	8 081795	8.083536	8.085270	18
42	8.086997	8.088717	8.090430	8.092137	8.093837	8.095530	17
43	8.097217	8 098897	8.100571	8.102239	8.103899	8.105554	16
44	8.107202	8.118569	8.110481 8.120169	8.12110	8.113734	8.115352	15
45	8.116963	8.128081	8.120109	8.131206	8.123351	8.124933	14
47	8.135851	8.137389	8.138921	8.140447	8.141969	8.13430 8 8.143485	13
48	8.144996	8.146501	8.148001	8.149497	8.150987	8.152472	115
49	8.153952	8.155426	8.156896	8.158361	8.159821	8.161276	10
- 50	8.162727	8.164172	8.165613	8.167049	8.168480	8.169906	
51	8.171328	8.172745	8.174158	8.175566	8.176969	8.178368	8
52	8.179763	8.181152	8.182538	8.183919	8.185296	8.186563	7
53	8.188036	8.189400	8.190760	8.192115	8.193466	8.194813	6
54	8.196156	8.197494	8.198829	8.200159	8.201485	8.202808	5
55	8.204126	8.205440	8.206750	8.208057	B.209359	8.210658	4
56	8.211953	8.213243	8.214530	8.215814	8.217093	8.218369	3
57	8.219641	8.220909	8.222174	8.223434	8.224692	8.225945	2
58	8.227195	8.228442	8.229685	8.230924	8.232160	8.233392	1
59	8.234621	8.235846	8.237068	8.238286	8.239501	8.240713	0
1	60"	50"	40"	30"	20"	10"	M
نبنت ا			Cathoment	89 Berrees			

Co-Ougent 89 Begrees-

Sine 1 Degree

			Sine 1 I				
M	0′′	10	20"	307	40"	50"_	
0	8.241855	8.243060	8.244261	8.245459	8.246654	8.247845	59
1	8.249033	8.250218	8.251400	8.252578	8.253759	8.254925	58
2	8.256094	8.257260	8.258423	8.259582	8.260739	8.261892	57
3	8.263042	8.264190	8.265334	8.266475	8 267613	8.268749	56
4	8.269881	8.271010	8 272137	8.273260	8.274381 8.281045	8.275499 8.282145	55
5 6	8.276614 8.283243	8.277 726 8.284339	8.278835 8.285431	8.279941 8.286521	8.287608	8.288692	54 53
7	8.289773	8.292852	8 291928	8 293002	8.294073	8.295141	52
8	8.296207	8.297270	8.298330	8.299388	8.300443	8 301496	51
9	8.302546	8.303594	8.354639	8.35,681	8.306711	8.327759	50
10	8.308794	8-304827	8.310857	8.311885	8.312910	8.313933	49
11	8.314954	8.315972	8.316987	8.318001	8.319012	8.320020	48
12	8.321027	8.322031	8.323033	8.324032	8.325029	8.326024	47
13	8.327016	8.328007	8.328995	8.329480	8.330964	8 331945	46
14	8.332924	8.333901	8.334876	8.335848	8.336819	8.337787	45
15	8.338753	8.339717	8 3406-8	8.341638	8.342596	8.343551	44
16	8.344504	8.345455	8.346405	8.347352	8.348297	8 349240 8 354855	43
17	8.350180	8.351119	8.352056	8.352991	8.353924		42
	8.355783 8.361315	8.356710 8.362230	8.357635 8.363143	8.358558	8 .359479 8.364964	8.360398 · 8.365871	41
19				8.3640;4			
20	8.366777	8.367681	8.368582	8.369482	8.370380	8.371277	39
21	8.372171	8.373063	8.373954	8 374843	8.375730	8.376615 8.381889	38
23	8.377499 8.382762	8.378380 8.383633	8.379260 8.384502	8.380138 8.385370	8,381015 8,386236	8.387100	37 36
24	8.387962	8.388823	8.389682	8.390539	8.391395	\$ 392249	35
25	8.393101	8.39395t	8.394800	8. 345647	8.396493	8.397337	34
26	8.398179	8.399020	8.399859	8.400696	8.401532	8.402366	33
27	8.403199	8.404030	8.404859	8.405687	8 406513	8.407338	32
28	8.408161	8.408983	8.409803	8.410621	8.411438	8.412254	31
29	8.413068	8.413880	8.414691	8.415500	8.416308	8.417114	30
30	8.417919	8.418722	8.419524	8.420324	8.421123	8.421921	29
31	8.422717	8.423511	8.427304	8.425096	8.425886	8.426675	28
32	.8.427462	8.428248	8.429032	8.429815	8 430597	8.431377	27
33	8.432156	. 8 432933	8.433709	8.434484	8.435257	8.436029	26
34	8.436800	8.437569	8.438337	8.439103	8.439868	8.440632	25
35	8.441394	8.442155	8.442915	8.443674	8-444431	8.445186	24
36	8.445941	8.446694	8.447446	8.448196	8.448946	8.449694	23
37 38	8.450440	8.451186	8.451930	8.452672	8.453414	8.454154	21
	8.454893	8.455631 8.460032	8.456368 8.460761	8.457103 8.461489	8.457837 8.462215	8.458570 8.462941	20
39	8.459301						
40	8.463665	8.464388	8.465110	8.465830	8.466 = 50	8.467168	19
41	8.467985 8 472263	8.468701	8.46941 6 8.473679	* * * * * * * * * * * * * * * * * * * *	8.470841	8 47 1553	17
42 43	8.476498	8.472971 8.477200	8.477901	8.474386 8.478601	8.475091 8.479299	8.475795 8 479997	16
44	8.480693	8.481388	8.482082	8.482775	8.483467	8.484158	15
45	8.484848	8.485536	8.486224	8.486910	8.487596	8.488280	14
46	8.488963	8.489645	8.490326	8.491006	8.491685	8-492363	13
47	8.493040	8.493715	8.494390	8.495064	8.495736	8.496408	12
48	8.497078	8.497748	8.498416	8.499384	8.499750	8.500415	11
49	8.501080	8.501743	8.502405	8.503067	8.503727	8.504386	10
50	8.505045	8.505702	8.506358	8.507014	8.507668	8 508321	9
50	8.508974	8.509625	8.510275	8.510925	8.511573	8.512221	8
52	8.512867	8.513513	8.514157	8.514801	8.515444	8.516086	7
53	8.516726	8.517366	8.518005	8.518643	8 519280	8.519916	6
54	8.520551	8.521186	8.521819	8.522451	8.523083	8.523713	5
55	8.524343	8.524972	8.525599	8.526226	8.526852	8-527477	41
56	8.528102	8.528725	8.529347	8.529969	8.530589	8.531209	3
57 58	8.531828	8.532446	8.533063	8.533679	8.534295	8.534909	2
1 - 1	8.535523 8.539186	8.536136	8.536747 8.540401	8.537358	8.537969	8.538578	0
59		8.539794		8.541007	8.54.612	8.542216	
	60''	50".	40"	30"	·20·'	10"	M
			Co-sine 88	1)			- 7

Co-sine 88 Degrees.

Tangent 1 Degree.

		1	angent 1	Degree.			
M	0"	10"	20"	30"	40*	50"	
0	8.241921	8.243126	8.244328	8.245526	8.246721	8.247013	59
1	8.249101					8.254996	58
2	8.256165	8.257331	8.258494	8.259654	8.260811	8.261965	57,
3	8.263115	8.264263	8.265408	8.266549	8.267688	8.268824	56
4	8.269956		8.272213				55
Ş	8.276691	8.277804	8.278913	8.280020	8.281124	8 282225	54
6	8.283523	8.284419	8.285512	8.280002	8.287689	8.288774	53
78	8.289856		8.292012				52
1	8.296292 8.302633	8 202682	8 204727	8.205770	8.2068 41	8.301583! 8.307849.	_
9			-				50
10	8.308884		8.310948 8.317081				49
12	8.315046 8.321122		8.323129				48 47
13	8.327114	8.228106	8.329093	8. 2 20080	8.221064	8.222045	46
14	8.333025	8.114002	8.334977	8.335050	8. 236021	8. 337800	45
15	8.338856	8. 339821	8.340783	8.341743	8.342701	8.343657	44
16	8.344610		8.346512				43
17	8.350289	8.351229	8.352166	8.353101	8.354035	8.354966	42
18	8.355895	8.356823	8.357748	8.358671	8 359593	8.360512	41
19	8.361430		8.363259			The state of the s	40
10	8.366894	8.367799	8.368701	8.369601	8.370500	8.371397	39
21	8.372291	8.373184	8 374076	8.374965	8.375853	8.376738	38
22	8.377622	8.378504	8.379385	8.380203	8.381140	8.382015	37
23	8.382889	8.383760	8.384630 8:389812	8 400676	0.300304	8 002281	36
24	8.388092 8.393234	8.204085	8.394934	8.205782	8.206628	8.807472	35 34
25 26	8.398315	8.2004.56	8.399996	8.400834	8.401670	8.402505	33
27	8.403338	8.404170	8.405000	8.405828	8.406655	8.407480	32
28	8.408304	8.409126	8.409946	8 410765	8.411583	8.412399	31
29	8.413213	8 414026	8.414837	8.415647	8 416456	8 417262	30
30	8.418068	8.418872	8.419674	8.420475	8.421274	8.422072	29
31	8.422869	8.423664	8.424458	8.425250	8.426040	8.426830	28
32	8.427618					8.431536	27
33	8.432315	8.433093	8.433870	8.434045	8.435419	2 430191	26
34	8.436962	8.437732	8.438500 8.443082	8 442841	8.444500	8 446255	25
35 3 6	8.441560 8.446110		8.447616				24 23
37	8.450613		8.452104				22
38	8.455070		8.456545				21
39	8.459481	8.460212	8.460942	8.461670	8.462398	8.463124	20
40	8.463849	8.464572	8.465295	8.466016	8.466736	8.467455	19
41	8.468172	8.468889	8.469604	8.470318	8.471031	8.47.1743	18
42	8.472454	8.473163	8.473871	8.474579	8.475285	8.475990	17
43	8.476693	8.477396	8.478097	8.478798	8 49 544	8.480195	16
44	8.480892	8.48 [588	8.482 1 83 8.4864 2 8	8 487146	8.427801	8.488494	15
45 46	8.485050	8.480822	8.490534	8 401212	8.401804	8.402672	14
47	8.489170 8.493250	X.402027	8.494602	8.405276	8.40 5040	8.406622	12
48	8 497 493	8.407967	8.498632	8.499300	8.499967	8.500632	11
49	8.501298	8.501962	8.502625	8.503287	8.503948	8.504608	10
50	8.505264	8.505025	8.506582	8.507238	8.507893	8.508547	9
51	8. (00 200	8.500852	8.510503	8.511153	8.511802	8.512451	8
52	8.513098	8.413744	8.514389	8.515034	8.515677	8.516319	7
53	8.516961	8. < 17602	8.518241	8.518880	8.519517	8.520154	6
54	8.520790	8.531425	8 4040	8 - 264-2	8 527324	8.523956	5
55	8.524586	8.525215	8.525844	8.520218	8,620840	8.531460	4
56 57	8.528 <u>3</u> 49 8.532080	8, c 22602	8.522216	8.532022	8,534540	8.535164	3 2
57 58	8.535779	8.526202	8年2700年	8.537616	8 578227	8 5 3 8 8 3 7	7
59	8.539447	8.540055	8.540662	8.541269	8.541875	3.542480	0
	60"	50"	40	30	20"	10#	M
a 1	\$0"	J.C.	- 			- ``	2012

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3	8.8560g	_			+ 15:435*44	10.000000	13.135144	29
3	8.16304			180	- 13:059153	10.000000	13.059153	57
4	8,169K				11 934814	10 0000000	12.9]4214	
	8.2766			2.760	12 837304	10.000000	12 837 304	>1
5	8.1831				12.758122	10000001	12.75\$123	54
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- 8	8, 3y6			. ,00517		10 000001		32
9	8.302			-41,970			12,581031	51
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12	8 3:			j~ 543909		10.000003		45
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61	8.			7 66 7849		10.000005		44
17	8.		4999995	7.694179		10 000005		+3
18			+049994	7.719003	12 280997		12.281003	43
19				7-741484		10.000001		41
20	-\$	4.1	4.999993		12235139			-13
81	5	4.1	9.999992	7.785951	12-214049		13.214057	>9
31	7	,0		7.806155			12-193854	- ,
23	,	2,4		7.825460		10 0000 10		3 *
24		- 14		7-843944		10 000011		30
25		12		7.861674		10.000011		3.5
26		57/4		7 878708		10.000011		34
27		1 18		7-895099		10.000013		
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19		5.19	9 9999%5	7.936134		10.000015		31
30	š.	1		7 9408 38		10.000017		30
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32	[2]	7 968870			_	10.000018		2.5
13	[5]	7,981133			12 017747			2"
34	[54]	7,995198					12.004302	
35		8.007787		8.007\$09		10.000013		25
3	36	8 020021 8 031919		8.020045 8.031945			11.979979 11.968081	· 부
	37	8.013501		8.041527			11.956499	32
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		8 076503			11.923404		11.933500	15
	42	N.086965			LE-913003 EE-902783			1.
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	14	8.10716° R.116926					11 883074	
	45	8. 42647 t			11.873490			1.5
	47	8.135810	0 0000to	8.176844	11 804140	10.000041	11.864190	13
		8.144953	9 9949 (8	8.141006	£1 855004	10.000041	11 \$55047	13
		8.153901			11.846048			11
		8.162681	9.999954	8 162727	11 837273	10 000046	11 837310	15
		8,171280	$\overline{}$		11828672			4
	4 1	8.179763	# 444A) v	8 120262	11.820237	10.000010	11 810182	b
		8.187985			11.811964			-
		8,196102			11.803844			6
	1	8 204070			61 795B74			,
		8.211895	9 900011	8 211042	## 788047	10.0000 (8	61.588104	
		8 219581	9.900040	8,319641	t1.780359	10.0000000	11,780419	3
		8,117134	9.999933	8.227195	11.772805	10.000061	11 772866	7 7 2
		8.234557	9 9999 36	8 234611	11.765374	10.000064	11.764443	
		8.241855	9.994914	8 241922	11.7 480-8	10-000066	11758145	
	N I	Co-sine	bine	Co tang	Tang.	Co-secr (M
	1		2	and county		· ·		_

39 Degrees.

1 Degree.

				Degree.			
M	Sine.	, Co-sine.	Tang.	Co-tang	Secant.	Co-sec.	K
-0	8 24 1855	0.000024	8.241021	11.758079	10.000066	11.758145	60
				11.750898			59
2				11.743835		11.743906	
3				11.736885		1 7 7	
4				11.730044			
ζ	- • .		_	11.723309			
6				11.716677			54
	8.289773			11.710144			53
				11.703708			52
				11.697366			51
				11.691116			
-				11.684954			49
12	8.321027	0.000005	8.321122	11.678878	10.000005	11678973	
				11.672886		, , , ,	47
				11.666975			
				11.661144			45
				11.653390			44
17	8 350181	9.999891	8.350289	11.649711	10.000109	11.649819	43
18	8.355783	9.999888	8.455895	11.644105	10.000112	11.644217	42
19	8.361315	9.999885	8.361430	11.638570	10.000115	1 T.638685	41
20	8.366777	9.999882	8.366895	11 633105	10.000118	11.633223	40
21	8.372171	9.999870	8.372202	11.627708	10.000121	11.627829	39
	8.377499	9.999876	8.377622	11.622378	10.000124	11.622501	38
23	8.382762	9.999873	8.382889	11.617111	10.000127	11.617238	37
24	8.387962	9.999870	8.388092	11.611908	10.000130	11612038	36
25	8.393101	9.999867	8 393234	11 606766	10.000133	11.606899	35
26	8.398179	9.999864	8.398315	11.601685	10.000136	11.601821	34
				11.596662			33
28	8 408 161	9.999858	8.408304	11 59 1696	10 000 142	11.591839	32
29	8.413068	9 999854	8.413213	11.586787	10.000146	11.586932	31
30	8.417910	9 999851	8.418008	11.581932	10.000149	11.582081	30
31				11.577,131			_
				11.572382			28
				11.567685			27
				11.563038			26
				11.558440			25
	-			11.553890	-		2.4
				11.549387			
				11.544930			22
				11.540519			
40				11.536151			
41				11.531828			
				11.527546		11.527737	18
				11.523307			
44	2 42 40 40	9.999801	8 42 -0 -0	71.519108	10.000199	11.515167	
45	8 438060	9 ,44,79 7	2 420170	11.514950	10.000206	11.515152	
47	8.402040	0.000700	8.402250	11.506750	10 000210	11.06060	14
				11.502707			
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	THE RESERVE THE PERSON NAMED IN						
				11.490800 11.486902			
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				11.460553	T. 1	11.460814	1
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) M	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec,	Secunt.	31
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LOGARITHMS OF NUMBERS:

No.	0	1 1	2	3	1 4	5	6	1 7	8	9
760	880814	880871	88092	.€0985	881042	881099	881156	881213	881270	881328
761	881385									881898
762	1									882468 883037
763 764										883605
765	883661	383718	883775	883832	883888	883945	884002	884059	884115	884172
766	384229	88418	884342	884399	884455	884512	884569	884625	884682	884739
767										885305
768 769	1									885870 88 6 434
770	_ <i></i>		.] [.							886998
771	887054	887111	887167	887223	887280	887336	887392	87449	887505	887561
772	887617	887674	887730	887786	887842	887898	887955	888011	888068	888123
773										888685 889246
774 775										889806
776	889862	889918	889974	890030	890086	890141	890197	890253	890309	890365
777	890421	890477	890533	890589	890,644	890700	890756	890812	890868	890924
778	801677	891035	801640	801705	891203	801259	891314	801028	201082	891481 892039
779			.] (.		892317			. ———	-	
780 781					892873					
782					893429					
783	893762	893817	893873	893928	893984	894039	894094	894150	894205	894261
784 785	894316	894371	894427	804026	894538	894593	894648	805252	807713	894814
78 6	805423	895478	845533	895530	895643	895140	895754	895257	895864	805020
787	895975	896030	896085	846140	896195	896251	896306	896361	896416	896471
7.88	1896526	896581	896636	896692	896747	896802	896857	896912	896967	897022
789	.]				897297					
790	897627	897682	897737	897792	897847	897902	897657	898012	898067	898122
791 792	808726	808780	898835	898840	898396 898944	808000	800054	800100	80016A	800218
793	899273	899328	899383	899437	899492	899547	899602	899656	899711	899766
794	899820	899475	899930	899985	900039	900094	900149	900203	900258	900312
795 796					900586					
790 797					901676					
798	902003	902057	902112	902166	902221	902275	902329	902384	902438	902492
799	902547	902601	902655	902710	902764	902818	902873	902927	902981	903036
800					903307					
801 802					903849					
803	904715	904770	904824	904878	904931	904986	904499	905094	905148	905202
804	905256	905310	905364	905418	905472	905526	905580	905634	905688	905742
805	_		_		906012		1	-		
806 807					906550;; 907089;;					
808					907626,					
809					908163					
810	908485	908539	908592	908646	908699	908753	908807	908860	08914	908967
811	909021	909074	909128	9091811	909235.9	909288	909342	909395 9	9094 49 9	909502
812 813	909550	9090091	909003	010261	909770	10268	909877	010464	10018	10037
	910624									
815	911158	911211	911264	911317	911371 9	11424	911477	911530 9	14584	11637
816 817	911690	911743	911797	911850	911903 9	11956	912009	12063 9	12116	12169
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819	913284									
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9	913814	913867	913920	913973	914026	914079	914131	914184	914237	914290
821	614242	014106	014440	014502	014555	914008	914000	914713	914700	914019
822	014872	014025	914077	1015030	101 6083	1915130	912199	915241	1915294	19153471
823 824	915400	915453	915505	016086	915011	916101	916242	916296	916349	915874 916401
825	016454	016507	916559	916612	1916664	916717	:916770	916822	910875	910927
826	080010	017032	017085	417138	917190	917243	.917295	917348	917400	9174531
827	917505	917558	917610	917663	917715	917708	917820 1018245	917875	917925	917978
828	918555	018607	018650	018712	018764	918816	918869	918921	918973	918502
										919549
830 831	10601	010653	914705	919758	919810	919862	919914	1919907	920019	920071
832	020122	929475	920228	920280	920332	920384	920430	, 9 20489	920541	920598
833	920645	920697	920749	920801	920853	920900	920958	921010	921002	021624
834 835	921166	921718	921270	921342	9213/4	921946	921998	922050	922102	922154
1 826	922206	922258	922310	922362	922414	922466	922518	922570	922022	922074
837	032725	922777	922829	923881	922933	922985	923037	923046	923140	923192
838	923244	923296	923348	923399	923451	923503	943555	923007	923050	923710
839	923702	y 230 14	y23005	945917	923909	724041	024580	024641	024602	924228
843	924279 924796	924331	924383	924434	944400	924054	926106	925157	925200	925260
841 842	025212	925264	025415	025467	925518	925570	925021	925073	925724	9257701
843	0268281	026870	025021	925982	026034	926085	920137	920188	920239	9202911
844	926342 926857	926394	926445	926497	920548	920000	920051	920702	920754	027210
845	927370	920900	920959	087524	927576	927627	927678	927730	927781	027832
846 847	1027882	927926	a 27a861	028027	928088	928140	928191	936342	940293	9 203451
848	028206	928447	928498	928549	928601	928652	928703	928754	928805	920050
849	928908	928959	929010	929061	929112	929163	929214	929200	929317	929300
850	929419	929470	929521	929572	929623	929574	979725	929776	929827	929878
	929930 930440	97998 I	930032	930503	939134	930604	930746	930796	950847	030898
852	010040	931000	931051	931102	931153	931203	931254	931305	931356	931407
854	931458	931509	931560	931610	931661	931712	931763	931814	931864	931915
8 55	931966 93 24 74	932017	932068	932118	932109	933220	932271	022820	957372	952423
856 857	93 24 74 934981	934544	9345/5	933133	933181	931234	933285	933335	933386	933437
858	933487	933538	933588	933639	933690	933740	933791	933841	933892	9339431
859	913993	934044	934094	934145	934195	934246	934296	934347	934397	93444
860	934498	934549	934599	934650	934700	934751	934801	934852	934902	934953
861	935003	935054	935104	935154	935205	935255	935300	935350	935440	935457
862 863	016011	026061	036111	936162	936212	936262	930313	930303	930413	9394031
864	1936514	926564	936614	936664	936715	936765	936815	930805	930910	930906
865	037016	037066	937116	937167	937217	937267	937317	937397	937418	9374081
866 867	937518	937508	937618	937008	937718	937779	32/919	938370	338420	93/909
868	938520	938570	938620	938670	938720	938770	938820	938870	438920	93897 0
859	939020	939970	939120	939170	939220	939270	939319	939309	939419	939404
	939510	939569	939619	939669	939719	939769	939819	939868	939918	939968
871	810018	940068	940118	940168	940218	940267	940317	940307	940417	940407
872 872	740516 941014	940500!	940010	940000	940710	040705	940015	940305	940915	941462
873 874	041511	941561	941611	941660	941710	941760	941804	941059	941909	941958
875	1012008	042058	042107	042157	942206	942250	942300	9423551	942405	942454
876	942504	942554	942603	942653	942702	942752	942801	942851	942900	942950
87.7 87. 8	943000	943049	943099	943148	943198	945247	945297	943346 943841	943800	943930
879	943480	944038	94:38	944137	944186	944236	944285	944335	944384	944433
	0	1	2	3	4	5	6	7	8	9
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No.	0	1	2	3	4	5	6	7	8	9
880	944483	944532	944581	944631	944680	944729	944779	944828	944877	944917
881	944976	945025	:945074	945124	945173	945222	945272	945321	945370	945410
882 883	945469	945518	945507	945016	945005	945715	945764	945813	945862	945911
884	046152	046501	1946059 1946060	940108	0.16640	046608	946747	046706	946354 946845	940403
885	946943	946992	947041	947090	947139	947189	947238	947287	947336	947385
886	947434	947483	947532	949581	947630	947679	947728	947777	947826	947875
88 ₇ 888	947924	947973	948021	948070	948119	1948168	948217	948266	948315	948364
889	9464-3	948402	1948511	949248	948003	1940057	040106	040244	948 8 04 949 29 2	948853
890									949780	
891	949878	949926	949975	950024	950073	950121	950170	949/3	950267	949029
892	1950365	950413	950462	950511	950560	950608	950657	950705	950754	950801
893	950851	950900	1950949	950997	951046	951095	951143	951192	951240	9 51 289
894 895	951337	1951380	951435	951483	951532	951580	951629	951077	951726	951774
896	952308	952356	95-920	951909	952502	952550	052500	952103	952 211 95 2696	952259
897	1952792	952841	.952889	952938	952986	953034	953083	953131	953180	953228
898	1953276	953325	953373	953421	953470	1953518	953566	953615	953663	053711
899	953700	953808	953856	953905	953953	954001	954049	954098	954146	954194
900	954242	954291	954339	954387	954435	954484	954532	954580	954628	954677
901 902	1954/25	954773	1954021 1954021	054009	954910	054900	955014	955002	955110	955158
903	1955688	955736	1955784	1955832	955880	955928	955976	956024	056072	0 56 120
904	1950108	956216	956264	1956312	956361	956400	956457	956505	956552	9 56601
905	1950049	495 009 7	1950745	1950792	950840	1956888	956936	956984	957032	0.57080
90 6 907	057607	957170	1957224	957272	957320	957308	1957410	957404	957511	957559
908	958086	958134	958181	958229	95/799	958325	95/094	95/ 91 2 958420	958468	950030
909	1958564	958612	958659	958707	958755	958803	958850	958898	958946	958994
910	959041	959089	959137	959184	959232	959280	950328	959375	050412	050471
911	1959518	959566	959614	1959661	959709	959757	959804	1959852	959900	0 00047
912	1959995	;900042 ≀060£18	1:900090 1:060 <i>5</i> 66	19 0 0138	1900185	1900233	960281	960328	960376 960851	960423
914	960946	960994	961041	961089	961136	1961184	961231	960804	961326	061274
915	1901431	1901409	901510	-901503	1961631	1961658	1961706	1961763	196 t 80 r	061242
916	1901895	1901 9 43	1901990	1902038	1902085	962172	662180	062227	962275	062222
917. 91 8	962842	1962417	19 0240 4	062086	1902559	1902006	962653	902701	962748 963221	962795
919	963315	963363	963410	963457	963504	963579	963500	063646	963693	06274
920	1963788	963835	961882	963929	963977	064024	064071	064118	964165	264212
921	1904200	904307	!904354	1904401	1001448	064406	064542	la64caa	064627	06.684
922		,7~4//~	7904023	19040/	, 404414	904900	1000013	100 (000	140 (100)	0051568
923 924	1905202	905249	.905290	1905343	1905390	1005437	'065484	1066631	1005578	06:626
925	1900143	900189	1900230	1900283	900320	966176	066422	066470	966048 966517	066264
926	300011	,900050	.900705	1900752	1900798	966845	066802	la66ata	10660261	067027
9 1 7 9 28	190/000	907147	907173	1907320	1907207	·007714	067361	067408	007454	967591
929	068016	-907595 -068062	907042 068100	068166	907735	967782	967829	967875	967922	967969
930	068 182	668520	:0684-4	0686-	0694	900249	908290	900343	968389	908430
931	968950	.900530 968996	900570	909023	1900070	060127	908703	908810	96885 6 9693 23	908903
932	303410	,909402	909509	1009550	900002	'ababaa	ahabar	060742	0607881	nhall a ce
933	303007	, 909928	1 9 09975	970021	970068	1070114	970161	070207	0702 CA	9701001
JJT	1212341	, y /~393	· y / '44' '	9/400	970533	1970579	0700201	070072	0707101	0707661
936	9,0012	19/0054	9/0904	970951	9 709 97	071044	071000	071127	0771821	071226E
937	. 7/ ~ / 4~	7/1/00	9/1056	47 1070	971025	071071	07201X	072004	971 64 7 9 7211 0	0791661
73-	7,31	7/7	9/4411	4/4(42)	U722081	072424	N794XDI	ハクタドタケリ	のファイマット	ハマッた・ヘー
<u>939</u>	37,000	972712	3/2/30	9/2004	972851	972897	972943	972989	973035	973082
	0	1 /	2	3	4	5	6	7	8	9
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No.	0	1	2	3	4	5	6	7	8	9
940	973128	973174	973220	973266	973313	973359	973405	973451	973497	973543
941										974005
942		974097								
943		974558								
944		975018 975478								
945 946	9/5434	975470	975983	476029	976075	976121	976166	976212	976258	976304
947	976350	976396	976442	976487	976533	976579	976625	976671	976717	976762
948										977220
949										977678
950										978135
951		978226								
952	978037	978683	470184	970774	970275	970221	970266	070412	979002	979503
953 954	9/9093	070504	974639	979685	979730	979776	979821	979867	979912	979958
955	980003	980049	980094	980140	980185	980231	980276	980322	980367	980412
956	980458	980503	980549	980594	980640	980685	980730	980776	980821	980867
957	980912	980957	981003	981048	981093	981139	981184	981229	951275	981320
958	981305	981411	981450	981501	901547	981592	981037	9811083	981728	981773
959										982226
960	981271	982316	982302	982407	902452	082040	902543	903500	902033 082084	982678 983130
961 962	082175	983220	082265	982210	08236	982491	983446	9834G1	983536	983581
963	983626	983671	983716	983762	983807	983852	983897	983942	983987	484032
964	084077	084122	984167	984212	984257	984302	984347	484392	984437	984482
965	984527	984572	984617	984662	984707	984752	984797	984842	984887	984932
966	984977	985022	985007	985112	985157	985202	985247	985292	985337	985382
967 968	985420	085070	085065	086010	086066	086100	086144	086180	086234	985830 986279
969	986324	986369	986413	986459	986503	986548	986593	986637	986682	986727
970										987174
971	987219	987264	987309	987353	987398	987443	987487	987532	987577	987622
972	987666	987711	987756	987800	987845	987890	987934	987979	988024	988068
973	988113	988157	988202	988247	988291	988336	988381	988425	988470	988514
974	988559	988603	988048	988093	908737	980782	080272	988871	980261	988960 989405
975 976	080450	080404	989539	989583	080628	989672	989717	989310	989806	989850
977	080805	989939	989983	990028	990072	990117	990161	990206	990250	990294
978	990339	990383	990428	990472	990516	990561	990605	990650	990694	990738
979	990783	990827	990871	990916	990960	991004	991049	991093	991137	991182
980	991226	991270	991315	991359	991403	991448	991492	991536	991580	991625
186	991650	991713	991757	99 t 802	991846	991890	991934	991979	992023	992007
982	992111 992553	992156	992200	992244	992208	992333	9943/7	992421	002007	992509 992951
983 984	992553	994598	992082	992000	993172	993216	993260	993304	993348	993392
985	993436	993480	993524	993568	993613	993657	993701	993745	993789	993833
986	993877	993921	993965	994009	994053	994097	994141	994185	994229	994273
987	994317	994361	994405	994449	994493	994537	994581	994025	994009	994713
	994757	994801	994845	994889	994933	994977	995021	995004	995168	995152
989		995240								
990	995635	995079	995723	995797	995811	995054	995090	995942	006424	996030 996468
991 992	990074	990117	390101	990403	996687	996730	996774	996818	996862	9964 68 996905
902	laa6a4a	laabaaz	997037	997080	997124	997168	997212	997255	997 299	997343
004	407286	997430	997474	997517	997561	997605	997648	997692	997730	99 7? 79
OOT	007823	997867	997910	997954	997998	998041	998085	998128	998172	998210
	998259	998303	1993346	998390	998434	990477	990521	000000	9999042	000087
997	998095	998739 999174	990/02	3900261	1000301	Dadsv8	990302	999435	999478	999522
9 98 22 9	6 00 50 5	999609	999652	999696	999739	999783	999826	999870	499913	999957
	()	1	2	3	4	5	6.	7	8	9
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_				Degrees.	-		_
М	Sine	Co-rine	Tateg	Lostang	Secant	Co-eec.	36
0				124+8380		10.980765	60
1	9.020435	9.99 1601	y 022834	10 977166	10.002399	19 9-9464	- 59
1				10 475456		10.978368	- 51
3				10-974749		10 977175	- 5
4				10.973545		10 97 5984	-51
5				10.972345		10 974797	5
6				10.971148		10.973614	54
T					10.002420		5.
8				13 968763		10.9712,6	5
9				13 46-6-6		10 970021	5
15	0 031350	9 04"+40	9 23 1420	13 950 341	10 001530		51
ш	9.03115"	9.99"466	9 034741	10.965209	10 002534	10.967743	-45
11	90,3411	9 957412	40,,949		17.002,48		4
13	9.034582	9.99"439	9 037144	10.962856	10.002501	10 965418	43
14	9.035741	9 99 48 5	9078316	10.961684	10.003,75	10.964239	4
15	9 036846	9-997411	9034445	1296.,15	10 002589		4
61	9 038048	9.99"39"	9.040051	10.959349	10,002603	13 961952	44
17	9 039147	9 99 7 38;	9041813		10.002617	10.960803	4.
£\$	9-040342	9 99 309	9.04297;		10 002611	10.959658	41
19		4 49"355			10.002645		4
10	9.042635	9-997341	9 045 244	10.954716	10.001659	10:957375	44
11	9 041-01	9 49 731	4 346EE	10.953566	10 001673	13 956238	3
12				12952418		10.955105	31
13				10.951273		10 953974.	3
24				13 950131		10 952846	3(
24				1-941791		10 951721	3
16				10.947856			34
37				10 946747		10.949481	3.
18					10.002772		3
29					10 002786		3.
30					10.002801		30
31					10.001814	10.945034	20
31						10.943929	2
33					10 002844		2
34					10 002859		3
35					10.002873	1	3
36						10.939540	
37				10.935547		10.938449	2
30					10 001917		2:
39					10 001932		1
40					10.002947		30
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1 4					10.002961		E S
42	9 00095	9.997024	9,009938	10.930001	10 002978	10 011051	
43	9 0000,0	1 44-334	9.071027	10 92897]	10.002491	10 071904	H
44					10.003006		1
45					10.003021		1.
46					10.003051		1
18					10.003066		1
49					10.003081		
50					10.003096		R
_			1	_			_
51				10.920350		10.923457	
52					19 003126		
53					10.003143		
54						10.930324	
55					10:003172		- 1
56					10 00 31 38.		
57					10.00;127		1
ş B					10 203218		
59					10 003134		- 3
60	005 /xe1	9940751	9.089144	10.910 36	10.003249	10.914106	
						Sccant.	

#3 Degrees.

7 Degrees.

I M	Sine.	Co-sine.		Co-tang.	Secant	Co-sec.	M I
					10.003249		
					10.003265		
	2 9.087947				10.003280		
	3; 9.088970	9.996704	9.092266	10.907734	10.003296	10.91 1030	_
1 4	19.089990	9.996688	9.093302		10.003312		56
	9.091008	9.996673	9.094336		10.003327	10.908992	~ ~ [
	9.092024				10.003343	10.907976	- · I
	9.0930 3 7 819.094047				10.003359		
	9.094047				10.003375	10.905953 10.904944	52 51
10	9.096062	9.996594	9.099468	10.900532		10 403938	50
1	9.097065			10.899513		10.902935	
	9.098066	0.006562	0.101201		10.003438	10.901934	49 48
1 13	9.099065	9.996546	9. 102519		10.003454	10.900935	47
	9.100062			10.896468	10 003470		46
	9.101056			10.895458		10.898944	45
	9.102048			10.894420		10.897952	44
	9.103037			10.893444		10.896963	43
	9. 104025			10.892441			42
	9.105010			10.891440	10.003551 10.003567	10.894990 10 894008	41. 40
	9.106973 9.107951			10.889444		10.893027 10.892049	39
1 2	9.108927	0.006284	0.112542	10.887457			38 37
	9.109901				10.003632	10.890099	36
					10.003649		35
					10.003665		34
2	9.112809	9.996318	9.116491	10.883509	10.003682	10.887191	33
2	9-113774	9.996302	9-117472	10.882528	10.003698		32
20	9-114737	9.996185	9.118452	10.881548	10.003715		31
3					10.003731		30
3	9.116656	9.996252	9.120404	10.879596	10.003748		29
3	19.117013	9.996235	9-121,377	10.878623	10.003765		28
33	9.118507	9.990219	0.122340	10.877652	10.203781		27
34	10.120460	0.006186	0.124284	10.875716	10.003798	10.280481	26
1 3	9.121417	9.996168	9.125249	10.874751	10.003833	10 878 683	25 24
3	9.122362	9.996151	9 126211	10.873789	10.003849		23
1 38	9 123306	9.996134	9.127172	10.872828	10.003866		22
30	9.124248	9.996117	9.128130	13.871870	10.003883		21
40	9.125187	9.996100	9.129087	10.870913	10 003900)	10.874813	20
	9.126125			10.869959	10.003917		19
42	9.127060	9.996066	9.130994	10.869006		10.872940	
4.	9.127993	9.995049	9-131944	10.868056	10.003951	10.872007	17
	9.128925			10.867107	10.003968 10.003985		16
1 4	9.129854	9.990015	0.121781	10.865216		10.8/0145	15
	9.131706					10.868294	13
1	9.132630	9.995963	9.136667	10.863333	10.004037		12.
4	9-133551	9.995946	9.137605	10.862395	1	10.866449	11
50	9.134470	9.995928	9.138542	10.861458	10.00.4071	10.865530	10
15	9.135387	9.995911	9.139476	10.860524	10.001089	10.864613	9
	2 9.136303	9.995894	9.140409	10.859591	10.004106	10.863097	8
1 5	2 9.137216	9.995876	9.141340	10.858600	10.001124	10.862784	7.
1 5	1 9.138128	9.995859	9. 142269	10.857731	10.004141	10.861872	6
5	9.139037	9.995841	9.143190	10 8 - 19 -	10.004159	10.800963	
1 5	39944	9.995823	9-144121	10.824026	10.004174	10.800050	
5	RIDITALTEA	0.00 c 2 X X	19.144066	10.854034	10.004312	10.8 (8246	3 2
1 2	9.1426cc	9.996771	9.146885	10.853115	10.004229	10.857245	,
6	9.143555	9-995753	9.147803	10.852197	10.001247	10.856445	0
· 1	Co-sinc	-	}		Co-sec.	1	M
,	- OU SHIC			Degrees.			,AL

				Degices.	Sacart		
M	Sine.	Co-sine.	Tang.	Co-tang.	Sccant.	Co-sec.	- M
C	9-143555	9.995753	9-147803	10.852197	10.004247	10.856445	60
1	9.144453	9.995735	9.148718	10.851282	10.004265		59
2	9.145349	9 995717	9.149632	10.850368	10.004283	10.854651	58
3	9.146243	9.995699	9.150544	10.849456	10.004301	10.853757	57
4	4	9.995681	9.151454	10.848546	10.004319	10.852864	56
5	9.148026	9.995664	9.152363	10.847637	10.004336		55
6	9.148915	9.995646	9.153269	10.846731	10.004354	10.851085	54
7	9.149802	9 995628	9.154174	10.845826	10.004372	10.850198	53
8	9.150686			10.844923	10.004390		52
9			9.155978	10.844022	10.004409	10.848431	51
	9.152451	9.995573	9.156877	10.843123	10.004427	10.847549	50
		9 995555	, —	10.842225	10.004445	10.846670	49
11	9.153330	0.005527	0.158671	10.841329	10.004463		48
1	9.155083	0.993337	0.150665	10.840435	10.004481	10.844917	47
1 3	9.155957	0.002101	0.160457	10.839543	10.004499	^	46
1 14	9.156830	0.005482	0.161247	10.838653	10-004518		45
1 :5	9.157700	0.005464	0.162226				.44
1	9.157/00	0.006446	0.162122	10 836877	10.004554		43
17	9.150509	0.002127	9.163123		10.004573	10.840565	42
19	9.159435	0.006400	0.161802		10.004591	10.839699	41
19	9.160301 9.161164	0.005200	0.165774		10.004610		40
21	9.162025	9.995372	9.100054	10.833346	10.004628		39
22	9.162885	9.995353	9.107532	10.832468	10.004647	10.837115	38
23	9 163743	9.995334	19.103409	10.831591	10.004666		37
24	9.164600	9.995316	9.109284	10.830716			36
25	9.165454	9.995297	9-170157	10.829843	. •		35
1 26	9 166307	19.995278	19.171029	10.328971	10.004722		
27	9.167159	9.995260	9.171899	10.828101	10.004740		33
28	9 168008	9.995241	9.172707	10 827233	10.004759	10.831992	32
29	9.168856	9.995222	9.173034	10.826366	10.004778	10.830298	_
30	9.169702	9.995203	9.174499				30
31	9 170547	9.995184	9 175362	10 824638	· · · · · ·		29
32	19.171389	19.995165	9.170224		10.004835	10 828611	28
33	9.172230	[9.995146	.9.177084	10.822910	10 004854	10 827770	27
37	9.173070	9.995127	9.177942	10.822052	10.004873		26
1 35	9.173908	9.995108	<u> </u>	10.821201	10.004892		25
36	9-174744	19.995089	9.179055	10.820345	10.004911	10.825256	24
37	19.175578	19.995070	,9.180508	10.019490	10.004930		23
38	9.176411	9.9950 <u>5</u> 1	9-181360	10.818040	10 004949		22
39	9.177242	9.995032	9 182211	10.817789	10.004968		21
40	9.178072	9 995013	19.183059	10.816941	10.504987	10.821928	20
) ————	,	10.816093	10.005007	10.821100	19
1 41	9.178900	0.00.1074	9.184752	1 0 5	1		18
42	9.179726 9.180551	0.0040cc	9.185507	10.814403	-		17
43	9.181374	D-004027	0.186420		_ :-	10.818626	16
44	9.181374	0.004016	0.187280	•	10.005084		15
45	9.183016	0.004806	0.188120			10.816984	14
40	9.183834	0.004877	9.1880cX	10.811042	-	10.816166	13
	9.184651			_ •		10.815349	12
40	9.185466	0.004828	9.140620			10.814534	11
49	9.186280	0.007818	9.191462	10.808538			10
51	9.187092	9.994798	19-19-294		10.005202	10.812097	9 8
52	9.107903	9 994779	9-195124	10.806876	10.005241	10.811288	7
53	9.103712	9.994759	9.495953	10.806047	10.005241	10.810.20	7 6
5+	9.109519	9-994739	9.194780	10.805220	10.005201	10.80067	
55	9.190325	9.994720	9.195000	10.804394	10.005201	10.809675	5
1 56	9.191130	9.994700	9.190430	10.803570	10.005300	10.808870	4
57	9.191933	9.994080	9.197253	10.802747	10.005320	10.800007	3 2
58	9.192734	9.994000	9.190074	10.801926	10.005340	10.80/200	_
59	9.193534	9.994040	9.190394	10.801106	10.005300	10.80-669	1
60				10.800287			
М	Co sine.	Sme.	Co-tang.	Tang.	Co-sec.	Secant.	M
-			43.0	1)0177400			

9 Degrees.

•					regices.			
1	M	' Sine.	Co-sine	Tang.	, Co-tang	Secant.	Co-sec.	, M
1-	0	0.104222	0.004620	·	10.80028		10.805668	60
-	ī				10.79947		10.804871	ł
1	2	0.105025	9.994580	9.20134	10.79865	10.005420	10.804075	,
ł	3	9.196719	9.994560	9.202150	10 79784	10.005440	10.803281	1 -
ł	4					10.005460		
1	5					10.005481		
ı	б	9.199091	9-994499	9.204592	10.79540	3 10.005501	10.800909	
ł	7					10.005521	10.800121	53
ł	8					10.005541		52
-	9					10.005562		•
1	0	9.202234	9.994418	9.207817	10.79218	10.005582	10.797766	50
1	1	9.203017	9.994398	9.208619	10.791381	10.005602	10.796983	49
1	2					10 005623		48
1	3					10.005643		47
12	4	9.205354	9.994336	9.211018	10.788982	10.005664	10.794646	46
1	_	9.206131	9.994316	9.211815	110.788185	10.005684	10.793869	45
L						10.005705		44
41	•					10.005726		43
1						10 00 5746		42
	- 1					10.005767		41
20			-		·	10.005788		40
2	- 1		9.994191			10.005809	10.789240	39
2						10.605829	10.788474	38
2	- 1					10 005850		37
2.							10.786945	36
2						10.005892		35
2	ł	,			10.779508	1	10.785421	34
2	_				10.778728	10.005934	10.784662	33
1					10.777948		10.783903	32
30	-				10.776393		10.782391	31
1-								30
3	'	9.218303	9.993982	9.334362	10.775618	1	10.781637	29
3			9.993960				10.780884	28
33			9.993939		10.774071		10.780132	27
34					10.773300		10.779382	26
35					10.771761		10.778633	25
4 -:		·· I	9.993854		10.770993		10 777139	24 23
37			9.993832		10.770227		10.776394	22
39	•				10.769461		10.775651	21
40			9.993789		10.768698		10.774908	20
-								}
41			9.993768		10.767935		10.774167	19
42			9-993746 9-993725		10.767174		10.773427	18
43 44			9-993723		10.765655	1	10.771952	16
44 45		2.228784	9.993/03	0.22(102	10.764897		10.771216	15
46			9.993660			10.006340	′ ' - 1	14
47						10.006362		13
48			9.993616			10.006384		12
49						10.006406		11
50		.232444			10.761128		10.767556	10
5 L	-	.233172					10.766828	9
53	- 1 -				10.759629	• • •	0.766101	8
53						10.006494		7
54						10.006516		6
55						10.006538		5
56						10.006560		4
57						10.006582		3
58					10.755161	10.006604	10.761765	2
59	9	.238953 9	.993374	-245579	10.754421	10.006626	10.761047	1
60						10.006649	10.760330	0
×	(Co sine.	Sine.	Co-tang	Tang.	Co-sec.	Secant	Ж
	`							

10 Degrees.

				regrees.			
M	· Sine.	Co-sine	Tang	Co-tang.	Secant.	Co-sec.	M
	0.220670	0.04.2251					60
0				10.753681	. •		
1				10.752943			59
2				10.752206		10.758899	58
3	, -		,	10.751470		10.758186	57
4				10.750736		,	56
5	19.243237	9.993240	9.249998	10.750002	10.006760	10 756763	55
6	9.243947	9 993217	9.250730	10 749270	10.006783	10.756053	54
7	9.244656	9.993:95	6.251461	10.748539	10.006805	10.755344	53
8				10.747809			52
9				10.747080			51
10	0.216775	0.003127	0.253648	10.746352	10.006873	10.753225	
				ļ	· 		
111				10.745626			49
12				10.744900			48
13				10.744176			47
14	ig. 249 583	j y 993036	9.256547	10 743453	10.006964	10.750417	46
115				10.742731			45
16				10.742010			44
17				10.741290		_	43
18	,	1	i	10.740571			42
19				10.739854	_		41
20	- ,	[~		10.739137			
21				10.738422			
22				10.737708			
23	9.255834	9.992829	9.263005	10.736995	10.007171	10.744166	-
24			9.263717			10.743477	
25				10.735572			
26				10.734862			_
27			9.265847		· .		
_		I			10.007264		
28			9.266555		10.007287	•	
29			9.267261		10.007311	10.740049	-
30	9 260633	9.992006	9 267967	10.732033	10 007334	10.739367	30
31	0.261314	9 992643	9.268671	10.731320	10.007357	10.738686	29
32				10.730625			
33			9.270077		10.007404		•
34				10.729221			
35				10.728521			
36				10.727821			,
37				10.727124			23
38				10.726427			22
39	9.266723	9.992454	9.274269	10.725731	10.007546	10.733277	21
40			9.274964	1	10.007570		
41			9 275658	·			
,					10.007594		I I I
42		1 _	9.276351		10.007618		
43				10.722957			
44				10.722266			
45				10.721576			
46				10.720887			
47	9.272064	9.992263	9.279801	10.720199	10.007737	10.727936	13
48	9.272726	9.992239	9.280488	10.719512	10.007761	10.727274	12
49	9.273388	9.992214	9.281174	10.718826	10.007786	10.726612	11
.50			9.281858			10.725951	10
-		-	†				
51	19.4/4708	9 992100	9.202542	10.717458	10.007834	10.735292	9
52	9.275307	9.992142	9.283225	10.716775	110 007858	10.724633	8
53	9.270025	9.992118	9.2 83907	10.716093	10.007882	10.723975	7
54	9.276681	.9.992093	.g.284588	10.715412	10.007907	10.723319	6
55	49-277337	9.992069	19.285268	10.714732	10.007931	10.722663	5.
56	.9.277991	9.992044	9.285947	10.714053	10.007056	10.722000	ā
57	9.278645	9.992020	9.286621	10.713376	10.007080	10.721266	3
58	9.270207	9.991996	9.287201	10.712699	10.008004	10.720702	
59	9.270048	9.001071	0.287077	10.712023	10.008020	10.720052	
60	9.280500	Q.QQ1047	0.288662	10.711348	10.008022	10.71040	0
1				The second name of the last of	,		
M	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant.	M
				Joorgoog			

11 Degrees.

M	Sine.	Co-sine.	Tang.	Co-tang	Secant.	Co-sec.	M
					10.008053		60
			9.289326		10.008078		59
2	0.281847	9.991897	9.189999	10.710001	10.008103		58
			9.290671		10.008127		57
4	9.283190	9.991848	9.291342	10.708658		10.716810	56
					10.008177		55
			9.292682		10.008201		54
			9.293350		10.008226		53
			9.294017		10.008251		52
			9.295349		10.008276		51
						-	50
			9.296013			10.712312	
			3.296677 9.297339		10.008351		48 47
			9.298001	,	10.008401		46
		9.991574		, , ,	10.008426		45
			9.299322		10.008451		44
	•		9.299980		10.008476		43
18	9 292137	9.991498	9.300638	10.699362	10.008502	10.707863	42
			9.301295	10.698705	10.008527	10.707232	41
20	9.293399	9.991448	9.301951	10.698049	10.008552	10.706601	40
			9,302607		10.008578		39
		9-991397	-	1	10.008603		38
			9.303914		10.008628		37
24	9.295913	9.991340	9.304507	10.695433	10.008654	10.70408	36
26	0.207164	0.001205	0.206860	10.604131	10.008679	10.702826	35 34
					10.008730		33
					10.008756		32
					10.008782		31
30	9.299655	9.991193	9.308463	10.691537	10.008807	10.700345	30
31	9.300276	9 991167	9.309109	10.690891	10.008833	10.699724	29
			9.309754		10.008859		28
					10.008885		37
					10.008910		26
					10.008936		25
					10.008962 10.008988		24 23
					10.009014		22
					10.009040		21
40	9.305819	9.990934	9.314885	10.685115	10.009066	10.694181	20
1			9.315523		10.009092		19
			9.316159		10.009118		18
			9.316795		10.009145		17
			9.317430	10.682570	10.009171	10.691741	16
45	9.308867	9.990803	9.318064	10.681936	10.009197		15
		9-99 ^C 777			10.009223		14
			9.319329		10.009250		13
			9.319961 9.320592		10.009276		12 11
			9.320392	10.678778	10.009305	10.688107	10
		-					
			9.321851		10.009355		9
1 52	9.311608	9.990601	9.327106	10.676804	10.009302	10.686202	7
54	9.314297	9.990565	9.323732	10.676267	10.009435	10.685703	6
55	9.314897	9.990538	9.324358	10.675642	10.009462	10.685103	5
56	9.315495	9.990511	9.324983	10.675017	10.009489	10.68.4505	4
					10.009515		3
					10.009542		2
					10.009569		1
1					10.009596		<u> </u>
} M	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant.	M

12 Degrees.

				A 40 .	Degrees.			
M	r i	Sine.	Co-sine	Tang.	Co-tang.	Secant.	Co-sec.	M
1	0 0	317870	9.000404	0.327474	10.672526	10.000506	10.682121	60
-					10.671905			59
1							10.680934	58
ł	1 -						10.680342	
•					10.670047			56
}							10.679160	55
1							10.678570	
ł					10.668197			53
•					10.667582			52
1							10.676800	51
1.							10.676220	50
-					-	-		
							10.675634	49
1	2 9	.324950	9.990079	9.334871	10.665129	10.009921	10.675050	
1	3 9	.325534	9.990052	; 9 . 33 548 2	10.664518	,10.009948	10.074466	47
					10.663907			46
					10.663298			45
					10.662689			44
					10.662081			43
					10.661473			42
1	9 9	.329021	9.989887	9.339133	10.660867	10.010113	10 670979	41
1_2	:0 <u>)</u> 9	·3 29 599	9.989860	9-339739	10.660261	10.010140	10.670401	40
2		.330176	9.489872	9.340144	10.659656	10.010168	10.660824	39
2	2 0	.330742	9.986801	9.340048	10.659052	10.010106	10.660247	38
					10 658448			37
	- ,	_			10.657845	_		36
					10.657243			35
-	- 1 -						10.666949	34
•	,				10.656042			33
-	1				10.655442			32
-			4		10.654843			31
					10.654245			30
_	-							
					10.653647			29
					10 653051			28
3	3 9	337043	9.989497	9.347545	10.652455	10.010503	10.002957	27
					10.651859			26
					10.651265			25
					10.650671			24
					10.650078			23
-			_		10.649486			22
					10.648894			21
4	<u>0 9.</u>	340996	9.989300	9.351697	10.648303	10.010700	10.059004	20
4	1 9.	341558	9.989271	9.352287	10.647713	10.010729	10.658442	19
					10.647124			18
		_			10.646535			17
					10.645947			16
					10.645360			15
	_				10.644773			14
_	1 -	1			10 644187	-		13
					10.643602			12
					10.643018			11
					10.642434			10
	-							
					10.641851			9
15	2/9.	248240	9.909950	y.339/31	10 64049	10.011044	10.052513	
5.	5 9.	348200	0.08880	7·3795 3	10.040007	10.011073	10.651760	7
154	+ 9.	340/92	A. 08884	y·359093	10 640137	10.011102	10.051200	
15	5:9.	349343	9.900009.	9.300474	10.639526	10.011131	10.050057	5
159	19.	349093	y.ycco40.	y.301053°	10.638947	10.011100	10.050107	4
45	9.	350443	9 900011	y. 301032	10.638368	10.011189	10.049557	3
					10.637790			2
					10.637213			1
100	—				10.636636			0
þí	C	o-sine	Sinc. '	Co-tang.	Tang.	Co-sec.	Secant.	M
1	-				Dagrage			

77 Degrees. .

13 Degrees.

13 Degrees.										
М	Sine.	Co-sine.	Tang.	Co-tang.	, Secant.	Co-sec.	м			
 					10 011276	10.647912	60			
	9 352088			1 a a 3	•		59			
1	9.352635	9.988666		10.635485			58			
2		9 988636		10.634910		10.646274	57			
3			9.365664		10 01 1393		56			
4		9.988578		10.633763		4	55			
6	9.354015	0.088648	9.366810		•	10 644642	54			
1			9.367382	10.632618	1	_ , , .	53			
7	0.355901	9.988489	0. 2670 62	10.632047		10.643557	52			
	9.356984	0.088460	0.368524	10.631476		10.643016	51			
10	9.357524	0.088430	0.360004				50			
	9.358064			10.630337		10.641936	49			
	9.358603			10.629768			48			
1	9.350003	0.088242	9.370799			10.640859	47			
13	9.359141			10.628633	. 1 .	10.640322	46			
15	9.359070	9.988282	0.271022		10.011718	, -	45			
	9.360752			10.627501		10.639248	44			
17			9.373064		, ,		43			
18		9.988193		10.626371		10.638178	42			
19		9.988163		10.625807	10.01 1837		41			
20			9.374756				40			
21			9-375319		10.011897	10.636578	39			
22		9.988073		10.624119		i	38			
23		9.988043			10.011957		37			
24		9.988013		10.622997						
25			9.377563			10.634454	9			
26	0.266076	0.087053	0.378122	10.621878		10.633925				
27		9.987922		10.621319	10.012078	10.633396				
28			9.379239		10.012108		32			
29			9.379797		-	10.632341				
30			9.380354		10.012168	10.631815	30			
31			9.380910	10.619090	10.012100	10.631289	29			
32			9.381466	10.618534		10.630764	28			
33			9.382020		10.012260	,	27			
34	0.270285	9.987710	0.282575			10.629715	26			
35			9.383129		10.012321		25			
36	0.371330	9.987649	9 383682		10.012351		24			
37			9.384234	_	10.012382		23			
38	0.372373	9.987588	9.384786	, •	10.012412		22			
39	9.372894	9.987557	9.385337	10.614663	10.012443	10.627106	21			
40	9.373414	9.987526	9 385888		10.012474		20			
41			9.386438		10.012504	10.626067	19			
42	0.274412	0.087466	9.386987	10.613013	10.012535	10.625548	18			
43	0 274070	9.987474	9.387536	10.612464			17			
44	9.375487	9.987403	9 388084		10.012597	10 624513	16			
45			9.388631		10.012628		15			
46	9.376519	9.987341	9.389178	10.610822	10.012659		14			
47	9-377035	9.987310	9.389724	10.610276	10 012690		13			
48	9-377549	9.987279	9.390270	10.609730	10.012721		12			
49	9.378063	9.987248	9.390815	10.609185	10.012752	10.621937	11			
50	9.378577	9.987217	9.391360	10.608640	10.012783	10.621423	10			
51	9.370080	9.987186	9.391902	10.608097	10.012814	10.620911	9			
52	0.270601	0.087155	0.302447	10.607553	10.012845	10.620399	9			
53	0.280112	9.987124	9.392989	10.607011	10.012876	10.019887	7			
54	0.280624	a.a870a2	0.393531	10.506469	10.012908	10.019370	6			
55	0.281124	9.987061	9.304073	10.605927	10.012939	10.618800	5			
56	lo. 281642	.0.087030	0.304614	110.60 < 386	10.012970	10.018357	4			
57	9.382152	9.986998	9.395154	10.604846	10.013002	10.617848	3			
58	9.382661	.g.g86g67	9.395694	; 10.604306	10.013033	10.017339	2			
59	0. 282168	0.086936	9 396233	10.603767	10.013064	10.610832	1			
60	' <u>9.3</u> 83675	9.986904	9.396771	10.603229	10.013096	10.010325	0			
M	Co-sine.	Sine.	Co.tang.	Tang.	Co-sec.	Secant.	M			
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11 Degree

I m Sine Cosme lang Cotang Secant Cosec- M
1 1 4 384182 a 68444 6 3343 b) 1, paspet 10 21312 10 41 2121 20
2 19 384087 9 964841 9 394 440 10 602664 22 41 2759 10 91 32 3 58
3 1 3 39 2175 2 7808-6 2 342 93 10 6. 161 - 152 51 1181 115 41 7808 2.
4 9 38669-19 480-18 9 53641, 1 bulabi (G.G.) 3322 10 81430] \$6
5 y 166201 9.080-49 y 1945y 1 1 h025y41 20.013254 1- 013749 55 0 y 186404 y 1667 1419 339900 10 h00010 17 D13226 20 h13246 54
7 14 1884 7 9 985682 9 450524 10 50 14 0, 10 21 332 11 0 62 21 93 53
\$ 4 , Rmon) 19 9000 12 9 40 10 18 17 4 18 4 2 2 4 4 17 17 19 10 11 12 24 1 5 2
4 6 - 14 5 - 14 5 - 14 5 - 14 14 14 14 14 14 14 14 14 14 14 14 14
10 6 1884 11 a deuter la tracet to target to cate 10 611284 40
\$1 14 \$2 42 11 9 465, 5 9 4 20 50 10 547 \$44 10 013445 10 (12780) 44
22 Q.58QT11 Q QBH.23,14 4.515T BU 5GBB13 10 7354TT 13 673384 AA 43 QUTU- 4 CI, 4006 (1) 4 A375KK 1 4 2 4 2 5 1 3 4 2 6 6 1 2 0 6 7 8 7 8 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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20 0.3036 N. W. 960200 La 207449 40 (925 NI) 10 013734 40 036314, 40
22 0 39417 979.956354 44 945 10 592355 47 063766 20 035821 49
22 (4 3940-1) 9 NH 212 3 4784-1 10 491439, 10 01313h 10 50 4327 38
23 G 24 (10 6) 4 10 10 3 40 10 60 10 10 10 10 10 10 10 10 10 10 10 10 10
24 4,395651 4557579 404,71 17 592479 17 013 67 (2 024) 62 36 25 4 39562 1 4561 4 9 11 44 12 36) 5 12 913 4 12 643 10 12
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29 3 308227 4 98 6 4 9 4 1 1 1 1 6 86 7 1 222 10 62 65 9 38
30 3 186 or 1, 5 '17 8 111422 15 19 10 11430 12 9214 W TO
132 4 1940 34 9 1449 14 14 15179 10 580 621 10 014441 10 600912 28
33 9,403,62,9,445,43,74142 4 10 585,70 110 01415 10 600425 22
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36 9 401/20 30/45-46 9 4162-5 10/684225 10/01/425/10 48460 24
36 9 40 248 9 9 4 4 2 2 2 3 4 4 4 2 4 2 2 3 2 3 2 3 2 3
[3] 19 402 172 9 98 36 19 9 41 326 10 38 2674 10 4 135 41 10 19 1 1 m
40 0 4-14-6 0 0,2411 341-84= 12 6,3128 12 -141, 12 20 -141 32
[41 9 4-74, B , 18, 467 4 418, 8 10 , 8:64-132-1442-13 5976#2 10
42 44 1470 4 \S41 541 541 587 10 \ 31 127 12 1 15 1 1 1 1 1 1 1
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84 10 478-31 1 48524 4 422484 10.576516 1-21475, 1 1 1-12 4
32 4 10000) 985212 9 423992 17 5 600 12 714 1 10 535 141 8
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15 Degrees.

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1					10.571443	10.0±5090 10.015124		59 58
1				9.429566		10.015158		57
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1				9.430573		10-015226		55,
1				9.431075		10.015260		54
1				9-431577		10015294		53
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4-				9.433580		10,015431	10.581850	
•				9.434080		10.015465		48
				9.434579	10 565421			47
				9.435078		10.015534		_
				9.435576		10.015568	7 · 7 · · · ·	45
				9.436073		10.015603		
	-			9·436570 9·437067	10.562933	~		43
_				9.437563	10.562437		10.578143	
				9.438059	10.561941		10.577682	
4	21	9.422778	9.984224	9.438554	10.561446	10.015776	10.577222	39
				9.439048	10 560952			38
				9-439543		10.015845		37
				9.440036		10.015880		36
					10.559471	10.015915	10.574927	
					10.558486		10.574470	
					10.557994		10.574013	
1	29	9.426443	9.983946	9.442497	10.557503	10.016054	10.573557	
7	}			9.442988		10.016089	10.573101	30
	3 1	9.427354	9.983875	9.443479	10.556521	10.016125	• •	29
•	_			9.443968			10.572191	28
				9·444458 9·444947				27 26
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	37	9 430075	9.983664	9-446411		10.016336		23
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1	44	9.433226	9.983416	9.449810	10.550190	10016584	10.566774	16
1	45	9.433675	9.983381	9.450294	10.549705	10.016619	10.566325	15
1	46	9 434122	9.983345	9-450777	10.549223	10.016655	10.565878	14
						10.016691	10.505431	13
				9.451743		10.016727		12 11
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1	7 j	q.4167a8	9.983176	9.453668	10.546772	10 016870	10.563202	8
	53	9.437242	9.983094	9.454148	10.545852	10.016906	10.562758	7
1.	54	9.437686	9.983058	9.454628	10.545372	10.016942	10.562314	
						10.016978		5 -
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1	6 ó	9.440338	9.982842	9.457496	10.542504	10.017158	10.559662	0
1	a	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secont.	M
4 -		والمستوال والمناد والمناد والمناد	بروجستوب برعادات			- برخورها و ب		

Mr. She. Coan	e Targ	Collang	Secuni	Co-scc	H 1
0 , 4453, 8 9 9828	42 9 45 496		10 . 1 . 1 58		60
1,9 -40178 9 9828	55 9 45 7973	12542047		10 359220	
2 9 441218 9, 1827	69 9 45 3444			10 337752	
3 9 44 658 9 982	33 9 450 925	10 34 973	10 01-10-	10 557342	57 58
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6 4 4 2 2 4 2 5 4 4 9 7 9	24 9 48 1349	10 439841	10 01 13 18	10.55*0**	54
- 0443310 6 9825	K [g, 40° 8a,	\$10.53917*	1750 413	10 556597	53
8 . 41:84- 0 0925	(1 14 46 1297	है।८५,874३	12.011449	12 (5615)	52
9 4 444284 6 9825	11,9 10,240	10 538270	at brutte	12 645-10	12
in 1444.5 0.0854					The real Party lies and the least lies and the leas
12 9 44 4500 0 9824	11/0 102,174	10 4 7 7 7 8 9 4	10.017.46	15 554045	49 45
13 9 44 652 5 9 9 X 2 3	6 - 9 26 (6 (8	110 676341	10 00 0011	30 6,3975	47
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1 1 9 316893 9 4822	94 4 464466	, 10 53,401	351033166	TO PASSEL	45
16 744"326 9 4822	37 4 405 66	10 634931	10.017*43	10 (510,4)	- 44
1 1 9 44 - 46 9 48 23	72 9 403 34	10 534461	10 017780	10 1/2341	43
18 9.448191 9 9821 19 9 448623 7 9821	aggar cook	410 443445	10 6 1 78 5 3	10 11174	41
23 14490,4 9 9821	5g g 466gs.	12 3 6	1001-801	10 510940	45
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22 9 440,1 5 9 98 10	1 9 40-R80	10 532120	10.017965	10 150083	38
1 21 4.4,034, 9 9819	18 4 46 34"	110.531653	10.018703	10 (4463)	3.4
24 9 4500 TS 6 9519	01 9 468814	10 (3)186	10 0185 39	Lu 14424 \$	36
26 9 45120 4 9 9819 26 9 451612 3 9818	2419 409280	10 (30720	10.018114	10 (48798	15 .
27 9 452060 9 1818	20 2 27 21 1	10,530254	10.018151	10 547980	
28 9 452488 9 4818	129 4-36-6	10 529324	10 018188	10 12"512	32
I 20 9 452925 9 9817	4 9 471141	10 528859	10 018228	10 547085	31
30 9 453342 9 9811	11 3 47160-	10 528395	10 012263	10 (468)8	15
31 9 453 168 9 451	JO 9 472068	10 527932	16/01/9300	14 (46974	29
32 9 454194 9 9816	9=10 412733	10 527468	10 - 18378	12 54 (806	28
33 9 454410 9 9816					22
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36 9 455843 9 981,	12 9 474381	10 525019	10 C (F 48%	10 (44/07	
3. 0.476319 8 4814.					33
38 9.456739 13 9814					137
39 9.457 (62 9 08) (79 9 4 5 00	10.514847	10 0 18h 20	10 (43.116	21
41 9458000 99813				-	19
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44 9 4,9268 9 68120	ng g 4-80sg	10.54/941	10 UTRIGH	40.340033	
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्रेष्ठ वे वेष्ट्राच्या विश्वति । वित्र वे वेष्ट्राच्या विश्वति ।					14
47 9 450946 9 981					
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5" 9 454994 9 98071	12 9.484981	10 (16018	Escuco CI	10 11:306	3
58 9 465108 9 7806	3 9 484 135	10 515565	1001332	10, 11,303	2
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17 Degrees.

				Magreca.	ويت بسيره د.	فكالت والمستخدين والمتحوي	
M	Sine.	Co-sine., T	ang.	Co-tang.	Secant.	Co-sec.	×]
0	0 46 5025	9.980596 9.4	ر سينيب ھي		12 010404	10.534065	60
1					10.019442		59
1	0.400340	9.980558 9.4	26242	10.514209		-	
2		9 980519 9.4			10.019481	10.533239	58
3		9 980480:9.4					57
4	9 467585	9.980442 9.4	57143	10.512857	10.019558		56
5	9.467496	9.980403 9.4	\$7593	10.512407	10.019597		55
6	9.468407	9.980364 9.4	38043	10.511957	10.019636	10.531593	54
7	9.462817	9. 980325 9.4	88492	10 211208	10.019675	10.531183	53
8		9 980286 9.48					52
19	9.469637	9.980247 9.48	39390	10.510610	10.019753		51
10	9.470046	9.980208 9.48	39838;	10.510162	10.019792	10.529954	50
II	0.470455	9.980169 9 49	0286	10.500714	10,019831	10.529545	49
12		9.980130 9.40					48
113	0 471271	9.980091(9.49	11180	10 508820	10.01000	10 528729	47
	2.47.570	9 980052,9.49	1627	10 508272	10.019948	10.528321.	46
114	9.4/10/9	9 900032,9.49	102/	10 507027			45
16	9.472384	9.980012 9.49	20/3	10 507927	10.019988	10.527508.	44
	9.472492	9-979973 9 49	12519	10.507481	10.020027	10 52/500	
17	9.472090	9-979934-9-49	74905	10.507035	10.020000	10.52/102	43
18	9 473304	9.979895 9.49	13410	10.500590	10.020105	10.530090	42
19	9-473710	9-979855 9 49	3054	10.500140	10.020145	10.520290,	41
20		9 979816 9.49			10.020184		40
21	9.474519	9.979776 9 49	4743	10.505257	10.020224	10.525481	39
22	9 474923	9-979737 9-49	5186	10.504814	10.020263	10.525077	38
23	9.475327	9.979697 9.49	5630	10.504370	10.020303	10.524673	37 .
24	é.475730	0.07065810.40	16073	10 503927	10.020342	10.524270	36
25	0.476133	9 979618 9.49	6616	10.503485	10.020382	10.523867	35
	0.476:36	9 979579 9 49	6657	10.503043	10.020421	10.523464	34
27	0 476028	9,979539 9 49	7 200	10 502601	10.020461	10 523062	33
28	0.477340	9 979499 9.49	7837	10.502150	10.020501	10.522660	32
29	9.47.734	9 979459 9.49	8282	10 501718	10.020541	10.522259	31
30	0.478142	9.979420 9 4	8722	10.601278	10.020580	10.521868	30
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31	9-478542	9.979380 9.4	99163	10.500837	10.020020	10.521458	29
32	9.478942	9 979340 9.4	9003	10.500397	13.020000	10.521058	28
33	9 479342	9.979300 9 50	20042	10 499958	10.020700	10.520058	27
34	9 479741	9.979260 9 50	20481	10.499519	10.020740	10.520259	26
35	9.480140	9.979220 9.50	00920	10.499080	10.020780	10.519800	25
36	9.480539	9.979180 9.50	359	10.498041	10.020820	10 519401	24
37	9.480937	9.979140 9.50	21797	10.498253	10.020800	10.519003	23
38	9.481334	9.979100 9 50	2235	10.497705	10.020900	10.518000	2.2
39	9.481731	9.979059 9.50	02672,	10.497328	10.020941	10.518269	21
40	9.482128	9.979019:9.50	3109	19.496891	10.020981	10.517872	20 !
41	0.482525	9 978979 9.50	3546	10.496454	10.021021	10.517475	1.9
42	0.482021	9 978939 9 50	3082	10 406018	10.021061	10.517079	18
43	0.482216	9.978898 9.50	14418	10.405582		10.516684	17
44		9.978858 9.50				· · · · · · · · · · · · · · · · · · ·	16
45		9 978817 9.50				1	15
46	D.ASA COT	9.978777 9 50) (72A	10.401276			14
47		9.978737 9.50				10.515105	13
48		9.978696 9.50				10.514711	12.
49		9.978655 9.50			_ , -,		11
50		9.978615 9.50				10.513925	10
Ã	Secretary or a second		-				
51	9 486467	9.978574 9 50	7893	10.492107	10.021420	10.513533	9
52	9 486860	9-978533 9-50	8326	10.491074	10.021467	10.513140	
53	9.487251	9.978493 9.50	08759.	10.491247	10.021507	10 512749	7
54	9 487643	9 978452 9,50	10100	10.490809	10.021548	10.512357	6
55	9.488034	9.978411 9.50	0622	10.490378	10.021589	10.511900	5
56	0.488424	9 978270lo.c	10054	19.489946	10.021630	10 511570;	4:
57	0.488814	9.07822010 51	10485	10.489515	10.021671	10.511186	3,
58	9.489204	0.07828819.51	(0016)	10.489084	10.021712	10.510790	2
59	a.4805u2l	0 078247 0.61	1246	10.488654	10.021753	10.510407	I
60	9 489982	9.978206 9.51	1776	10.488224	10.021794	10.510018	_
M	Co-sine	The same of the sa	tang.		Co-sec	Secant	M.
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м	Sine	Co-sme		Codang	Secapt.	Cossec	36 8
1-		g g=820tr				-	25
3	gianyana	9 9-8102	6112.6	ED 45 ** 34	1.02183.	13 (cot 25)	
2	9.490755	9978124	512455	10 18-212	1 6215-6	10 SUMBLE	25
3	4.49114	9-8083	51 24	17.485936	10.021917	15 958895	C7
4	4.491554	g arth fai.	es 3447	11,486,01	[1 / 21958]	1- 508409	- 55
15	9491932	g gott mark	03 3921	486019	12021299	10 30 50 78	55
6	9 491108	9 1919	1 (14)49	10 48 (644	10 /22041	1 301,43	3.4
8	0.445038	9 9 7 7 9 1 8	3 5 6 5 7 7 7	10 15 223	1 221.02	1. 1860.0	33 12
9		9 3835					3.5
13		3 077704				1 / 900 / 69	30
i e		9 9 7 7 5 2		_		_	
12	444441	9.411	9 (11 010	10 48,04	17 12228 ;	1 3000 4	44
13		99-1660					11
14	9 19-338	19 917628	9-517761	10483333	10 223 2	10 5 4012	45
15	9 495" 2				10.0555414		45
16		3 477544	2 3 1 8 6 1	1 481397	10 375179	5 5 3 K 4 B	14
18	3 4 4 5 5 3 T	49 - 45	0 51 -555	10 40 00 12	10 /22491	30 (7)	43 42
10	d #0, sc	9 4 - 4 3	4 5 988:	10 d 20 112	17023651	10 \$03000	
20	044785	(0 0 - 5)	9 52750 .	110 4-169	10 023622	10 245318	12
31		9 9 331					
122	9-195444	(A a 33,	9 521151	1347834	10 01:10	10 .1556	31
23	3 448925	[נפבררט ט	y satyig	10.578427	10 00 3749	10 304 174	4.
23		9.941339					10
±5		991167					34
26	19 494963				10 0228-5		31 3
23	9 500342 9 500342	0 971033			10 - 22939		
20	9 301599				10 023001		
30		9 37 95				1 248 524	20
31		9.0 0 1		·			
32	9 5022,1	997672	45-5-54	0.414641	1002,128	10 41 7 64	23
33	g 501601	14,01681	y gashint	134 4222	10.023,00	17 497345	27
34	19.50.2684	[[4] 975757]	9 , ** 19*	1 4 77 4	10 12 52 6	1. 49"010	96
35	9 201100	9 976745	1,26615	1,42,570	TO 024254	TTAVEDAL	2.5
36		4.9767.2 9.946680					2.5
37 38	9 50418			12 4 12131		12.494892	
19		y 9-45-4				1 495140	31
40		19 705,2			10 011469	494° 5	23
41		9370489		+	-		19
42		6010446					18
43	19 5 6354	9 976474	9.529957	13 4761,0	10 12,546	13 493641	17
44		9 976364					10
45		9 6 76 (18					15
46 47	10 50-83	9 9 6 2 3 2	o szeben	10. 58:32	0.023725	1 4929 6	2.4
48	9.505214	9 9 6189	9 117 /15	10 10-02	10 023 703		13 1
49	9 50858	9.916146	F 532411	10 467 61	10 32385.	10 431412	11
50	4 508951	1019-61	1 433844	15 465 4	សេកឧទ្ធន៍ទូក	12 Micts	10
51	9 500 20	49-5 6	9 55,266	10 466 34			٠
52	9-559695	ويد عجو وا	4 4130-1	10 406321	to 023983	17 11/1504	ĸ
53	9 51006,	4979 4	9 14092	10.463968	(- 324,726)	10419935	
54	9. 510484	9975032	534554	(3.355496)	13,5270.00	1, 1843, ,	
\$ \$ \$ 6	19 51030]	97588-	9 3 3 4 3 1 10	13 40 3 74	1201111	1 403 9".	3
57	9 511040	9 974844	9 5 5 5 5 5 6	10 30 126 2	10 . 113 4	10 423937	3
128		9.475 -47					
59	9 51 2275	9 975 143	9 536561	10 46;114	LAUSSES NO.	\$748-726	
6.3	19 512641	9.9"55" 4	4 536972	10,467026	11 024370	1041444	G
M	Cosme	1	Costing	3 ang	Cosec		30
				housees			

19 Degrees.

- M	Sine	Co-sine.	_	Co-tang.	Secant.	Co-sec.	M
0					10.024330		1
					10.024333		59
2	9.513375	9.975583	9-537792	10.462208	10.024417	10.486625	58
3					10.024461		57
4	9.514107	9.975496	9.538611	10:461389	10.024504	10.485893	56
5					10.024548		55
7					10.024535		54 53
8					10.024679		52
9	9.515930	9-975277	9.540653	10.459347	10.024723	10.484070	51
10	9.516294	9.975233	9 541061	10.455939	10 024767	10.483706	50
11			9.541468		10.024811		
12					10.024855		
13			9.542281		10.024899	• -	47 46
15			9.543094		10.024987		45
16			9-543499		10.025031		44
17			9-543905		10.025075		. 43
18			9.544310		10 025120	•	
19			9-544715	~~~	10.025164		
20	9.519911		9.545119				
21 22			9·545524 9·545928		10.025252		
23			9.546331		10.025341		
24					10.025386		36
25	9.521707	9.974570	9.547138		10.025430	10.478293	35
26		9.974525		10.452460		10.477934	1
27 28		9.974481	9·547943 9·548345	10.452057		10.477576	
29	_	9.974391		1	10.025564	10.477219	
30	-	9.974347	9	10.450851		10.476505	_
31			9.549550	10.450450		10.476148	
32		9.974257		10.450049	10.025743	10.475792	28
33	9.524564	9.974212	9.550352	10.449648	10.025788	10.475436	27
34			9.550752	10.449248	, , , ,	10.475080	26
35		9.974122		10.448848	10.025878	10.474725	25
36 37		9.974077	9-551952	10.448448 10.448048		10.474370	24 23
38		9.973987		10.447649		10.473661	22
39		9.973942		10.447250		10.473307	2 [
40	9.527046	9.973897	9.553149	10.446851	10.026103	10.472954	20
41		9.973852		10.446452	10.026148	10.472600	-
42		9.973807		10.446054	10.0e6193	10.472247	18
43		9.973761		10.445656		10.471895	17 16
44		9.973716 9.973671		10.445259	10.026329	10.471542	16
46			9.555536			10.470839	-
47		9 973580		10.444067	10.026420	10.470487	13
48			9.556329		10.026465	10.470136	
49			9.556725	10.443275	_	10.469785	11
50		9.973444		10.442879		10.469435	
51		9 973348		10.442483		10.469085	-
52		9.973352	9.557913	10.442087	10.026648	10.468735 10.468386	- ,
54					10.026739		6
55					10 026785		5
56	9.532661	9.973169	9.559491	10.440509	10.026831	10.467339	4
57					10.026876		3
58					10.026922 10.026968		2
59 160					10.020908		0
1	Co-sine	Sine.	Co-tang.	Tang.	Co-sec.	Secant.	M
		WHIT.		erree	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		<i>5</i> 4. (

_		C		Ca lead	Succes	Parameter.	- 10 -
12	Sure.	Co-sine	Tang	Co-tang	Secunt	Cossec	-11
3	9.534052	49-1980	9 501200	13.438934	10.017014	10 464443	603
1 1	9-534399	9.972040	9-501459	10 438541	10,017000	10.41 (00)	50
2	9-534745	9.9*2894	9.591051	10 436149	10 027100	10.405255	5R
2	d 222.302	19. 2 2040	0 - 61616	10-4304.6	Katerone	10 444462	17
1 1	9 535850	0 072766	0.522038	10.43 502	10.02"746	10 464217	50
5	4.131 43	4 0.4-00	0. 101710	10 436181	10 027191	15 46 3871	33 44
-	S C E L 2 3	10 073063	4 (6 (6 1)	10.436180	ranangge	17 463426	53
8	9 536818	9,971017	9 564202	10.434-98	roinar (8)	10 462182	52
9	9.537163	9 973570	9 554502	10.435403	10.021430.	10.462831	96
10	9:437597	9.974524	9 504687	10 43501"	13 021416	10 45 244	Ç3
1	19.5.7851	9 972478	9 505373	10.434625	10.021532	13 ch2+49	49
12	9 438194	19 972431	9 50 5763	10 434231	10.027553	10.451506	48
1.3	9.538:38	9972785	9.566143	10 433841	10.027615		47
1 14	9.538880	9 972338	9 500542	10 433458	10/01/602	10 4011 20	46
115	4.539223	9.972291	9 (66932	10.4337065	10 037 109	10 450777	44
16	9.539304	9.972245	3 20,300	10 43 2684	10 027755	10.4694341	44
57	9 519907	9 972198	3.50-709	10 432191	10.017801	10.410063	43
1.9	4.542249	9 972151	3 508.98	10 43 1902	10.01*845	10 AGGT 5 1 10 AGGATO	41
19	9 540 500	0 424018	0 06889	10.431514 10.431727	10.021945	10 4.956	41
_							#W
2.1	9 541272	9 972011	9 509361	10 430*39	10.02*ybg	10.4(8)20	34
22	9 541013	9.971904	0.570334	10 430342 20.424965	10,028083		35
1 23	9-541953	19-9" 1917 10-67 1870	0.570422	10.424578			34 36
24	0.242613	0 071832	9. 570806	17.420191	10.028177	10 41- 169	35
1 16	0 (126*1	9 971776	9 471194	10 428805			34
27	9 543310	9 471724.	9.571581	10-428419	10.028171	12 450690	33
主祭	9 543649	9 971682	9 571907	10 428033	10.038318	10 440321	31
20	9 543987	9 97 1635	4-5-2352	10 427648	10 038365	10.4560.3	31
30	4.544325	9 971388	4.502738	13.427252	10.058717	19.4539.2	3.5
11	9,544063	9-9"1540	4 5"3123	(3.426877	10 028460	10 Fy533"	19
1 22	9,545000	99"14931	9.573397	10 420493.	10.02850~	10 4 4 5000	28
1 3 5	4 545338	9 971446	3.5"3892	10 426108	10 028 (14)	10.454002	3"
14	9 545674	9 9 1398	4.514216	10 42 57 24	10.028002	10 474336	25
35	9 540011	9.971351	9 374600	10 425343	10 0580 19	10 45 (469)	25
36	9-546347	9 971 303	9-5-5944	10 414956	10 038241	10.423023	14
3"	9 240043	0.021108	n (4.8)0	10 4145"3	10 028702	10.423581	23
35	0.647261	0.021161	9 376101	12 41 180	12 0288 10	10.152046	31
1 40	0 547684	9 9 1113	1.576576	13 42 34 24	1002885		30
	+				10.018071	10 4514-6	12
1 41	9.545024	0.071318	0 477341	10:423939	10.028482		17
44	0 548602	מדמנים פ	9 5 7 7 7 2 1	10,42227"		12411301	17
43	9 544027	9 9"3913	9 5-8103	ro.42189h		1-4700-51	15
45	9 549360	9.970874	9 578486	10:421514	10 029126	10 450440)	25
46	9.549693	9 9 28 27	9.5-886-	10.421/33.	10.039173		14
47	9.550026	9 970779	9 579248	10.420152	10 029271		11
48	9.550359	9 9, 65 11	9 574629	10 430311			12
		9 970683		10 419991	10.029317		1.1
		9.970635			10.024365		10
51	9.5513,6	9-9-0586	9 220-69		10 029414		2
1 52	9 551085	9 970538	9 501149		10.029462		
53	9.552018	9-370490	0 (81002)	10 (1800)		30 437651	7 6
545	9-330-149	9 9*0442° 9 9*0394	o (X22X6)	10.117714		10: 11,120	5
22	0 (53040)	9 970145	9. 58266	10 41 777	10 424635		- 41
57	0. 551343	9 9"0297	9.58 2042		10 029703		3
28	9.553670	5 9 0 0 449	9 581422			1 , 446 133	á
59	9.5 540 000	9 970300	4 5×3800	10.416200	16 939 300	10.446000	
		9 970152		10415823	10 729848	10 445046	
М	Co-sine.	Sine.	Co-tang	Tang	Co-sec	Secunt	24
_				Jegrees.			

21 Degrees.

				negrees,			
X	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	M
0	9.554329	9.970152	9.584177	10.41 5823	10.020848	10.445671	60
3	9.554658	9.970103	9.584555	10.415445	10,020807	10.445342	59
				10.415068			58
				10 414691			57
				10.414314			56
5	0.545971	9.959909	9,586062	10.413038	10.030001	10.444029	55
6	9.556299	9.060860	9.586439	10.413938 10.413561	10.030140	10.443701	54
2	9.56626	0.069811	9.586815	10.413145	10.010184	10.442274	53
8	9. 556653	9 969762	9.487190	10.412810	10.030208	10.443047	52
9	0.447280	0.060714	9.587566	10.4131 ⁴ 5 10.412810 10.412434	10 030286	10.442720	51
10	9.557626	9.469665	9.587941	10.412059	10.030334	10.442394	50
				10.411684			49
				10.411309			48
				10.410934			47
				10.410560			46
							45
				10.409812			4+
12	y 559003	9.909321	9.590502	10.409438	10.030079	10.440117	43
10	0 56050	0.060000	7.370935	10.409065	10 02000	10.439793	42
				10.408692			41
				10.408319			40
				10.407946			39
				10.407574			38
				10.407202			37
24	9.562146	9-968976	9.593171	10.406829	10.031024	10.437854	36
25	9.502468	9.968926	9.593542	10.406458	10.031074	10.437532	35
						10.437210	34
				10.405715			33
						10.436567	32
			9.595027		10.031272	, , - ,	31
30	9-504075	9.908078	9-595398	10.404602	10.031322	10.435925	30
31	9.564396	9.968628	9.595768	10.404232	10.031372	10.435604	29
32	9.564716	9.968578	9.556138	10.403862	10.03 1422	10.435284	28
33	9.565036	9.968528	9 596508	10.403492	10.031472	10.434964	27
34	9.565356	9.968479	9.5 96 878	10.403122	10.031521	10.434644	26
35	9.565676	9.968429	9.597247	10.402753	10.031571	10.434324	25
				10.402384			24
				10.402015			23
				10.401646			22
				10.401278			21
40	9.567269	9.968178	9.59909 t	10.400909	10 03 18 22	10.432731	20
41	9.567587	0.968128	9.599459	10.400541	10.031872	19.432413	19
				10.400173		10.432096	18
				10.399806			17
				10.399438		10.431461	16
				10.399071		10.431144	15
	1					10.430828	14
T			9.601662			10.430512	13
•				10.397971		10.430196	12
49	9.570120	9.967725	9.602395	10.397605		10.429880	11
50	9.570435	9.967674	9.602761	10.397239	10.032326	10.429565	10
51	0.570751	9.067624	9.603127	10.306872	10.022276	10.429249	9
42	9.571066	9.067 672	0.602402	10.306107		10.428934	8
			9.603858	10.306142	10.032478	10.428620	
						10.428305	6
						10.427991	5
						10.427677	
						10.427364	
						10.427050	
						10.426737	•
60	Q. 577575	9.967166	9.606410	10.30350	10.032834	10.426425	0
	Co sine.		Co-tang		Co-sec.	Secunt	
1 -	O BINE.	SHIE.	Co-cang	Tang.	くわっちてじ	DECUM	

Sine Co-sine Tang Co-tang Secant Co-sec M	22 Degrees.								
1 0.573888 0.967115 0.606773 0.392827 10.032885 10.445680 58 29 2.574200 0.96704 0.607137 40.392863 10.032987 10.445680 58 3.574212 0.967010 3.968251 10.392873 10.435800 58 3.574217 0.966819 0.608285 10.391775 10.033091 10.445684 57 0.575788 0.966859 0.608285 10.391775 10.033091 10.443645 58 0.575789 0.966859 0.608285 10.391075 10.033192 10.442424 53 58 0.576379 0.966767 0.609674 10.390026 10.033294 10.423331 50 0.576389 0.966567 0.609674 10.389064 10.033295 10.423331 50 0.576389 0.966567 0.609674 10.389064 10.033491 10.423331 51 0.577309 0.966567 0.609674 10.389064 10.033491 10.423331 51 0.5776379 0.966567 0.6017679 10.389064 10.033491 10.423311 51 0.5776379 0.966567 0.611480 10.388906 10.033398 10.423001 49 49 577792 0.966447 0.611480 10.388580 10.033501 10.423073 49 49 577927 0.966447 0.611480 10.388580 10.033501 10.421073 49 49 577927 0.966447 0.611240 10.388799 10.033503 10.421073 49 49 577927 0.966136 0.612241 10.38799 10.033503 10.421073 49 47 47 47 47 47 47 47	M	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	M	
1 0.573888 0.967115 0.606773 0.392827 10.032885 10.445680 58 29 2.574200 0.96704 0.607137 40.392863 10.032987 10.445680 58 3.574212 0.967010 3.968251 10.392873 10.435800 58 3.574217 0.966819 0.608285 10.391775 10.033091 10.445684 57 0.575788 0.966859 0.608285 10.391775 10.033091 10.443645 58 0.575789 0.966859 0.608285 10.391075 10.033192 10.442424 53 58 0.576379 0.966767 0.609674 10.390026 10.033294 10.423331 50 0.576389 0.966567 0.609674 10.389064 10.033295 10.423331 50 0.576389 0.966567 0.609674 10.389064 10.033491 10.423331 51 0.577309 0.966567 0.609674 10.389064 10.033491 10.423331 51 0.5776379 0.966567 0.6017679 10.389064 10.033491 10.423311 51 0.5776379 0.966567 0.611480 10.388906 10.033398 10.423001 49 49 577792 0.966447 0.611480 10.388580 10.033501 10.423073 49 49 577927 0.966447 0.611480 10.388580 10.033501 10.421073 49 49 577927 0.966447 0.611240 10.388799 10.033503 10.421073 49 49 577927 0.966136 0.612241 10.38799 10.033503 10.421073 49 47 47 47 47 47 47 47						10.032834	10.426425	60	
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M Co-sine. Sine. Co-tang Tang Co-sec. Secant. M			904026	3.627852					
	M (Co-sine.	Sine.	Co-tang	Tang	Co-sec.	Secant.	М	

67 Degreest

H	Sine	Co-sine.		Co-tang	Secant:	Co-sec.	M
		·	جشدد بعيد	10.372148			60
	9.591376	0.062072	0.628203	10.371797	10.036028	10.407824	59
2	9-592473	9.963919	9.628554	10.371446			
3	9.592770	9.963865	9 628905	10.371095	10.036135		57
4	9.593067	9:963811	9.629255	10.370745	· · ·	10.406933	
5	9.593363	9.963757	9.629006	10.370394			55
6	4.593659	9.963704	9.629956		10.036296		54
3	9.593955	9.903050	0.030300	10.309094	10.036350		53 52
	9 · 5 9 42 51 9 · 5 94 <u>5</u> 47	0.963590	0.621006		10.036458		51
10	9.594842	0.063488	9.631355		10.036512		50
	9.595137				10 036566		49
11	9.595432	0.062270	0.632053		10.036621	10.404568	48
13	9.595727	0.963325	9 632401		10.036675	10.404273	47
14	9.596021	9.963271	9.032750		10.036729	10.403979	
15	9.596315	9.963217	9.633098		10.036783	10.403685	
16	9.59660 9	9.963163	9-033447		10.036837		44
17	9.596903	9.963108	9-033795		10.036892	10.403097	43
18	9.597196	9.903054	0.524143	10.3655510	10.036946	10.402510	42 41
20	9.597 490 9.597783	0.062046	0.624828		10.037055	10.402217	40
					10.037110		39
21	9.598075 9.598368	0.062826	0.62552		10.037164	10.401632	38
22	9.598660	9.962781	9.635879		10.037219		-
24	0. 508053	0.062727	0.6362261	10.363774	10.037273	10.401048	36
25	9-599244	9.962672	9.636572	10.363428	10.037328	10.400750	35
26	9-599536	9.902017	9.030919	10.303001	10.037303	10.400404	34
27	9.599827	9.962562	9.637265		10.037438		33
28	9.600118	9.902508	9.037011		10.037492		32 31
29	9. 600 409 9.600700	0.062208	0.628202		10.037602		
					10.037657	10.399010	29
31	9.600990 9.601280	0.904343	0.628002		10.037712	10.398720	28
22	9.601570	0.062233	9.630337		10.037767	10.398430	
34	9.601860	9.962178	9.639682		10.037822		26
35	9.602150	9.962123	9.040027		10.037877		25
36	9.602439	9.902007	9.64037:		10.037933		24
37	9.602728	9.962012	9.640716		10.037988		23
38	9.603017	9.901957	9.041000		10.038043		22 21
39	9 603305 9.603594	0.061846	0.641747		10.038154	10.396406	20
					10.038209		19
41	9.603882	9.901791	0.642424	10.357909	10.038265	10.395830	18
42	9.604170 9-604457	0.081980	4.642777		10.038320		17
44	9.604745	9.961634	9.643120	10.356880	10.038376	10.395255	16
45	0.605032	9.961509	9.043403	10.356537	10.038431	10.394968	15
46	9 625319	9.961513	9.043800		10.038487		14
47	9.605606	9.961458	9.044 148		10.038542		13
48	9-605892	9,901402	0.644490		10.038598 10.038654.		12
49	9-606179 9-606465	9.901340	0.645174		10.038710		10
-					10.088765		
51	9. 60 6751 9. 60 7036	9.901235	0.645857	10.254404	10.038821	10.202064	9
52	9.607322	0.061122	0.646100	10.352801	10.038877	10.392678	
-4	a.607607	9.961967	9.046540	10.353460	10.038933	10.392393	0
50	0.607802'	9.961011	9.040881	10.353119	, 10.038989	10.392108	5
56	0.608177	9.960955	9.647222	10.352778	10 039045	10.391823	4
57	9.608461	9.960899	9.647562	10.352438	10.039101	10.391539	3
58	9.608745	9.960843	9.047903	10.352097	10.039157	10.391255	2
59	9.609029 9.6 093 13	9.900780	0.6.18.22	10.251/5/	10.039214	10.300687	0
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					10.330998			
1	2				10.330668		10.373781	59
I							10.373510	
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ł	5	1			10.329680		10.372700	55
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	10	9 028047	9.950084	9.071903	10.328037	10.043316	10.371353	50
ł	11 !	9.628916	9 956625	9.672291	10.327709	10.043375	10.371084	49
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1	13	9.629453	9.956506	9.672947	10.327053	10.043494	10.370547	47
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ł	15	9.629989	9.956387	9.673602	10.326398	10.043613	10.370011	45
1					10.326071			44
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-	19				10.325090			41
1	20	9.631326	9.956089	9.675237	10.324763	10.043911	10.368674	40
	21	9.631593	9.956029	9.675564	10.324436	10.043971	10.368407	39
1	22				10.324110		10.368141	38
ŀ	23				10.323783		10.367875	37
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1	25				10.323131			35
ł	26	9.632923	9.955729	9.677194	10. 322806	10.044271	10.367077	34
1	27				10.322480			33
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	3 [0.634240	0.055428	0.678821	10.321179	10.044573	10.365751	29
	-				10.320854			28
8.			•		10.320529			27
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•					10.318908		_ ,	22
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•	55				10.316644		- - '	15
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2	9.642360	9.453537	9 692933	10 311170	10.046461	10.557640	18
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4	19 642877	9 95 34 3	3 000401	10 312437	10.04676	10 357123	36
1 3	9 043135	9 953312	3 400 104	10 (1021"	10.040040	10.356601	\$5
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26	0 648642	9 052743	6 606410	10.301530	19 04 05	10.351488	34
27	9 648766	2801700	a 695187	10 101211	30 0430 20	10 351234	33
28	9 644020	951917	9 69-103	10 301847	10 048587	10 350980	32
29	0.640274	9 95 18 54	9 597420	10 302586	10.048146	10 250126	31
30		9 951791			110 048209	10.350415	30
31				10 10104"	10048212	10 35 2219	20
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40	9 65 2052	9 951159	0 200803	10 299101	10 048841	10 347 348	30
41	9 652304	9 951046	9 701208	10 298192	10 048904	10.34-666	19
42	9 652555	,9.951012	9 701523	10 498477	10 048968	10 347445	18
43	9 652806	9 950968	9 701837	10.298,63	10.049032	10 347104	17
44	9 653057	19 950905	9 702152	10.397848	20 049695	10.140443	10
45				10 297534			15
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47						10.346194	73
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49						15- 145001	16
50				10,295964	-		10
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1		9,949816	•		10.050184	10.342705	59
3			9.707790		10.050248	10 342458	58
3		9.949688			10.050312	10.342210	57
4			9.708414		10.050377	10.341963	56
5			9.708726		10.050442	10.341716	
6		9-949494			10.050506		54
7		-	9.709349		10.050571	10.341222	53
		•	9.709660		10.050636	10.340975	52
9		9.949300			10.050700		1 - 1
10	9.059517	9.949235	9.710282	10.289718	10.050765	10.340483	50
11	9.659763	9.949170	9.710593	10.289407	10.050830	10 340237	49
12	9.660009	9.949105	9.710904	10.289096	10.050895	10.339991	48
13	9.660255	9.949040	9.711215	10.288785	10.050960		
14	9.660501	9.948975	9.711525	10.288475		10.339499	
15	9.660746	9 948910	9.711836	10.288164	10.051090		45
16	9.660991	9.948845	9.712146		10.051155		44
17			9.712456		10.051220		43
18			9.712766		10.051285		42
119		9.948650	-	10.286924			
20			9.713386			,	
21			9.713696			-	
22						10.337786	39
23			9.714005 9.714314	10.285995	• •		38
					10.051612		37
24	9.002940	9.940323	9.714624	10.285376		10.337054	36
26				10.285067		10.336810	35
					10.051808		34
27					10.051874		33
28						10.336080	•
29			9-716168		10.052005		31
30			9.716477		10.052071	10.335594	30
31	9.664648	9.947863	9.716785	10 283215	10.052137	10.335352	29
32	9.664891	9.947797	9.717093	10.282907	10 052203	10.335109	28
33	9.665133	9.947731	9.717401	10.282599	10.052269	10.334867	27
34					10.052335		26
35	9.665617	9.947600	9718017	10.281983	10.052400	10.334383	25
36			9718325		10.052467		24
37	9.666100	9.547467	9.718633		10.052533		23
38			9.718940		10.052599		22
39					10.052665		21
40			9.719555				20
41			9-719862	•			
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43					10.052930		17
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45 46					10.053063		15
•				10.278604		10.331733	14
47 48	5.000500	0.046949	9.741704	10.5/0490	10.053196	10.551494	13
B -					10.053262		12
49				30.277685		10.331014	11
50					10.053396		10
51					10.053462		9
52					10.053529		8
53					10 053596		7
					10.053663		6
55	9.670419	9.946270	0.724149	10.275851	10.053730		5.
56	9.670658	9.946203	9.724454	10.275546	10.053797	10.329342	4
57	9.670896	9.946136	9.724759	10.275241	10.053864		3
58	9 671134	9-9 46069	9.725065	10.274935	10.053931	10.328866	2
59	9.671372	9.946002	9.725369	10.274631	10.053998		. 1
60					10.054065		0
X	Co-sine.		Co-tang.		Co-sec.	Secant.	×
		~:	30 tang.		170-11.U1	occur.	

28 Degrees. ,

-				Degrees.	`		
_ M	Sine.	Co-sine	Tang.	Co-tang.	Secant.	Co-sec	M
	- 62.600						
	9.671609			10 274326			60
1				10.274021			59
2	9.672084	9.945800	9.726284	10 273716	10.054200	10.327916	58
3	9.672321	9-945733	9.726588	10.273412	10.054267	10.327679	57
4				10.273108			56
٤				10.272803			55
6	9.673032			10.272499			
							54
7				10.272105			53
8				10.271891			52
				10.271588	10.054672	10.326259	51
10	9.673977	9-945261	9.728716	10.271284	10.054739	10.3 26023	50 '
	9.674213	0.015103			10.054807		
							49
	9.674448				10.054875		48
	9.674684				10.054942		47
	9.674919				10.055010		46
15	9.675155	9.944922	9.730233	10.269767	10.055078	10.324845	45
16	9.675390	9.944854	9.730535	10.269465	10.055146	10.324613	44 '
	9 675624				10.055214		43
	9.675859				10.055282		42
	9 676094				10.055350		
20	0 626219	7.344050	0.72174	10.268255			41
6 —	9.676328				10.055418	10 323672	40
21	9.676562	9-944514	9.732048	10.267952	10.055486	10.323438	39
	9.676796					10.323204	
25		9.944377		•		10.3 22970	
	9.677264				10.055691	10.322736	36
				10.266743			35
	9.677731					10.322269	34
						10.322036	33
	9.678197					10.321803	
	9.678430					10.321570	31
30	9.678663	9.943899	9-734764	10.265236	10.056101	10.321337	30
1					10.056170	10.321105	29
				10.264633			28
						10.320640)
							27
				10.264031			26
						10.320176	25
				10 263430			24
				10.263129			23
38	9.680519	9.943348	9.737171	10.262829	10 056652	10 319481	22
						10.319250	21
10	9.680982	9.917210	9.737771	10.262220		10.319018	20
				-			
	9.681213				10.056859		19
	9.681443			_	10.056928	(18
	9.681674			_	10.056997		17
	9.681905			10.261029	10.057066	10.318095	16
45	9.682135	9.942864	9.739271	10.260729	10.057136	10.317865	15
46	9 682365	9.942795	9-739570	10.260430			14
47	9.682595	9.942726	9.739870	10.260130	10.057274	10.317405	13
48	9.682825	9.912656	9.740160	10.259831	10.057744	10.217176	12
40	9.68 2055	0.042587	9.740168	10.259532	10.057412	10.216045	11
50	9.683284	0.012512	0.740767	IG 250222	10.057483	10 216716	10
1							
511	4.083514	9.942448	9.741066	10.258934	10.057552	10.316486	9
52	9.683743	9 942378	9.741365	10.258635	10.057622	10.316257	8
53	9.683972	9.942308	9.741664	10.258336	10.057692	10.316028	7
54	9.68.1201	9.942230	9.741962	10.258038	10.057761	10.315700	6
55	9.684433	9.942160	9.742261	10.257730	10.057821	10.315570	5
56	9.681628	0.012000	Q.742550	10.257441	10.057001	10.216242	
27	9.68388-1	0.042020	0.7428-6	10 257140	10.057907	10.315342	4
28	0 68: 1 -	0.041010	0 7 11 - 6	10.25/142	10.05/9/1	10 313113	3
	0.69	9.94 (959)	3./43 I 20	10.250844	70.058041	10.314885	
29"	y.un5343	9.941889	9.743454	10.250546	10.058111	19.314657	1
-00	9.035571	9.941819	9-743752	10.256248	10.058181	10.314429	0
M	Co-sine.	Sine.	Co-tang.	l'ang.	Co-sec.	Secant.	M
-					 		

29 Degrees.

м	Sine.	Co-sine.	Tang	Co-tang	Secant.	Co-sec.	М
0	9.685571	9.9418:9	9.743752		10.058181	10.314429	60
1	9.685799	9-941749	9.744050	10.255950	10.058251	10.314201	59
2	9.686027	9 941679	9-744348	10.255652	10.058321	10.313973	58
3	9.686254	9.941609	9.744645	10.255355	10.058391	10.313746	57
4	9.686482	9.941539	9.744943	10.255057	10.058461	~ ~ ~ .	56
5	0.686026	9.941409	9.745240	10.254760	10.058531	10.313291	55
7	0.687162	0.041390	0.745330	10.254462	10.058602		54
8	0.687380	0.041268	0.746132	10.253868	10.058742	10.312837	53 52
9	9 687616	9.941187	9.746429	10.253571	10.058813	10.31284	51
10	4.687843	9.941117	9.746726	10.253274	10.058383	10.312157	50
11	9.688069.						49
12	9.688295	9.940975	3-747319	10.252681		10.311705	48
13	9.688521	9.940905	9.747616			10.311479	47
14	9.688747			10.252087		10.311253	46
15	9.688972	9.940763	9.748209			10.31 1028	45
16	9.689198	9.940093	9.748505	10.251495	• • •	10.310802	44
17	9:689423 9 689648			10.251199	, ,		43
19	9.689873	0.040480	9.749097 0.740202	10.250903 10.250607		10.310352	42
	9.690098	9.940409	9.749589	10.250311	10.059591	10.310127 10.309902	40
21	9.690323						
22	9.690548	0.040267	0.750281	10.250015	-		39 38
23	9.690772	9.9.10196	9.750576	10.249424		10.309432	37
24	9.690996	9.940125	9.750872	10.249128			36
25	9.691220	9.940054	9.751167	• •	10.059946		35
26	9.691444			10.248538	81000018	10.308556	34
27	9.691668	9.939911	9.751757	10.248243	,	10.308332	33
28	9.091892	9.939840	9.752052		10.060160		32
29 30	9.692115 9.692339		9.752347		10 060232		31
						10.307661	30
31 32	9.692562		9-752937	10.247063	10.060375		29
33	9 693008	0.020182	0.752526	10.246769 10.246474	• •	10.307215	28
34	9.693231			10.246180	_	_ //	27 26
35	9.693453	9.939339	9.754115	10 245885			25
36	9.693676	9.939267	9.754409	10.245591	10.060733	10.30632.4	24
37	9.693898	9.939195	9.754703	10.245297		• •	23
38	9.694130	9.939123	9.754997	10.245003		~ ~ .	22
39	9.694342	9.939052		10.244709			21
40	9.6945.64			10.244415	10.061020		20
41	9.694786	9.938908	9.755878	10.244122	10.061092		19
42	9.695007	9.938836	9.756172	10.243828			18
43 44	9.695229 9.695450			10.243535		10.304771	17 36
45	9.695671			10.243241		10.304550	15
46	9.6 15892	9.938547	9.757345	10.242655	10.061453		- 1
47	9.696113	9-938475	9.757638	10.242362	10.061525		13
48	9.696334	9.938402	9.757931	10.242069		,	12
49	9.696554	9.938330	9.758224	10.241776	10.061670	10.303446	11
50	9.696775	9.938258	9.758517	10.241483	10.061742	10.303225	10
51	9.696995	9.938185	9.758810	10.241190	10.061815	10.303005	9
52	9-697215	9.938113	9.759102	10.240898	10.061887	10.302785	8
53	9.097435	9.938040	9.759395	10.240605	10.061960	10.302565	7
54	9.097054	9.937967	9.759687	10.240313	10.062033	10.302346	6
55 56	9.09/0/4	9.93/095 0.027822	9.759979	10.240021	10.062105	10.302126	5
57	9.608212	9.027740	9.760ch 1	10.239/28	10.002178	10.301900	4
58	9.698532	9.937676	9.7608 66	10.230144	10.062324	10.301468	3 2
59	9.698751	9.937604	9.761148	10.238852	10.062346	10. (01249	1
ÓΟ	9.698970	9 <u>93</u> 7531	9.761439	10.238561	10.062469	10.301030	0
, —	Co-sine.		Co-tang.		Co-sec.	Secant.	
-	-	-	-	Degrees			

M Sine.	Co-sine	Tang.	Co-tang.	Secatt.	Co-sec.	. 34 1
U 9.6989-0				-	10. ;010 10	
1 9.699189					13 300811	
2 9 699407	9 937385	9 761013	10 237977	10 062615	10.300593	58 .
				10-062588		
				[10,062762 10,062834		_
0 9 200180						
				(10 06298)		
1 9 750716						52
9 9.10 933	8-9308 TZ	9 164961	10 23,939	10.063128		
10 9.701131					10 adkgite	-
12 9.701368						
13 9. 201801	9. 4205-8	9 10 (734	10 234176	10 06 3322	to redied	47
14,9-702019	9 43650	4 705514	10 234486	10 063445	10 26 68 1	40
15 9,703236	9 010431	9-165805	10 224195	12.063569	10 397764	45
16 9 TOZ452 17 9.702669						44
18 9.702885				10:063-00		4J 45
19 9.703101,						
20 9 101317						46
21 9 203133	9 935988 .	9 767545	10 232445	10064012	10 296461	19
22 9 7 3 49						38
23 9 703964				10 004100		37 36
				10 06430%		35
26 9 704614						34
21 9.101824						33
				10 664531		32
30 0 105469						31
31 9.70(68)			-			39
30 9 5848						28
33 9 100162	9 933097	9 771015	10 228485	10.004913	10 193230	27
34 9 = 26326						35
\$5 9 700539 36 9 706753						25
319 106967						23
18 0.00180						22
				10,065351		21
40 9 121806						10
				10.065501		19
42 9.00 KD32	9 339444	3.773806	10.220397	10.065051	10 201757	18 1
44 84:8						16
43 30-3	9-934199 5	7744741	10-226529	10/04,801	10 191310	45
46 9 708881						14
48 9 709306,						13
46 9 709518						2.0
50 9. 7097 30						10
51 4 154941						3
52 9 121731	\$ 93,6m1 r	-6483	10 223518.	10/256379	in abolique	
\$3 9 T103"4 9						6
54 974 5786 9						5
50 4.7 6447						- 4
57,9 11,205 9	933247 4	****465	16. 111589	10 UASTON 1	a affing a	- 3
58 9 7114.9 9						1
6019 74183 , 4						6
at Co-steel		Cotang			Secani	H
			Kices.			'

31 Degrees.

M	Sine.	Co-sine.		Co-tang.	Secant.	Co-sec.	M
6						10.288161	[]
				10.220940			59
2	9.7.12260	9.932914	9.779346	IC 220654	10.067086	10.287740	58
3	9.712469	9.932838	9.779632	10.220368	10.067162	10.287531	57
4	9.712679	9.932762	9.779918	10.220082	10.067238	10.287321	56
5				10.219797			55
6	9.713098	9 932609	9.780489	10.219511	10 067391	10.286902	54
7 8	9.713308	9 932533	9.780775	10.219225	10.067467	10.280092	53
z. 1	9.713517	9.932457	9.781000	10.218940 10.218654	10.067543	10.286483	52
9	0-712025	9.932300	0.781621	10.218369	10.067606	10.286066	50
	The second line of the last of		·				
11			9.782201	10.218084			49 48
13				10.217514			47
14			9.782771		10.068202		46
15				10.216944			45
16			9.783341		10.068155		44
17	9-715394	9.931768	9.783626	10.216374	10.068232	10.284606	43
18		9.931691			10.068309		42
119		9.931614			10.068386	• •	41
20	9.716017	9.931537	9.784479	10.215521	10.068463	10.283983	40
21			9.784764		10.068540		39
22	9.716432	9.931383	9.785048	10.214952			38
23				10 214668		10.283361	37
24				10.214384			36
25				10.214100			35
26				10.213816			34
27 28						10 282534	33
29				10 21 3248 10.21 2964			32
30				10.212681		10.281915	31
				-	_		30
31				10.212397			29
32 33				10.211830			28 27
34				10.211547			26
35				10.211264			25
36				10.210981			24
37				10.210698			23
38				10.210415			22
39				10.210132			21
40	9.720140	9.929989	9.790151	10.209849	10.070011	10.279860	20
41	9-720345	9.929911	9.790433	10.209567	10.070089	10.279655	19
42			9.790716		10.070167		18
43				10.209001			17
44				10.2087:9			16
45			9.791563		10.070401		15
46				10.208154			14
47				10.207872	1		13
48			9.792410		10.070636	·	12
49 50	9.722181		9.792092	10.207308	10.070714		11
51				10.206744			9
5 2 53				10.206462		10.277412	7
54				10 205899	-		6
				10.205617			5
_				10.205336			4
57				10.205055			3
				10.204773			2
59	9.724007	9.928499	9.795508	10.204492	10.071501	10.275993	1
460						10.275790	0
M	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant.	M
			······································				

			. ندن	Degrees.			-
M	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	M
				10.204211	10.071680	10.275790	60
	0.724.112	0.028342	9.796070	10.203930	10.071658	10.275588	59
2	0.724614	0.028267	9.746351	10.203649	10.071737	10.275386	58
-	0.724816	9.928183	9.796632	10.203368	10.071817	10.275184	57
1	0.725017	9.928104	9.796913	10.203087	10.071896	10.274983	56
5	0.725219	9.928025	9.797194	10.202806	10.071975	10.274781	55
6	9.725420	9.927946	9-797475	10.202525	10.072054	10.274580	54
7	9.725622	9.927867	9-797755	10.202245	10.072133	10.274378	53
8	9.725823	9.927787	19.798036	10.201964	10.072213	10.274177	52
9	9.726024	9.927708	9.798316	10.201684	10.072292	10.273976	51
			·	10.201404		10.273775	50
11	9.726426	9.927549	9.798877	10.201123	10.072451	10.273574	
12	9.726626	9.927470	9.799157	10.200843	10.072530	10.273374	
13	9.726827	9.927390	'9 799437	10.200563	10.072610	10 273173	47
14	9.727027	19.927310	9.799717	10.200283	10.072090	10.272973	46
				10.200003			45
				10.199723			44
				. 10. 199 443			43
				10.198884			41
				10.198604			40
			·	10.198325			
				10.198345			
						10.271175	
2.1	0.724024	9.926511	9.802513	10.197487	10.073489	10.270976	36
25	9.729223	9.926431	9.802792	10.197208	10.073569	10 270777	35
26	9.729422	9 926351	9.803072	10.196928	10.073649	10.270578	34
						10.270379	33
						10.270180	
						10 269932	
						10.269783	30
				10.195534		10.269585	
				10.195255			
				10 194977			
34	9.731009	9.925707	19.805302	10.194698	10.074293	10 268991	'
35	9.731200	0.925020	10.805850	10.194420	10 074374	10.268794	-
27	0.721602	0.025465	a.806127	10 193863	10.074433	10.268596. 10.268398,	- ,
				10.193585		10.268201	22
30	0.731996	9.925363	9.806693	10.193307	10.074697		21
40	9.732193	9.925222	9.806971	10.193029	10.074778	10.267807	20
				10.192751			19
42	0.732587	0.025060	9.807527	10.192473	10.074039	10.267413	18.
42	9.732784	9 924970	9.807805	10.192195	10.07 (02)	10.267216	17
44	9.732985	9.924897	9-808083	10.191917	10.075103	10.267020	16
45	9.733177	9.924816	9.808361	10.191639	10.075184	10.266823	15
46	9.733373	9.924735	9.808638	10.191362	10.075265	10.266627	14
				10.191084			13
				10.190807			12
49	9.733901	9.924491	9.009471	10.190529	10.075509	10.266039	11
				10.190252	·		10
51	9.734353	9.924328	9.810025	10.189975	10.075672	10.265647	9
52	9.734549	9.924246	19.810302	10.189698	10.075754	10.265451	
53	9-734744	9.924104	9.010580	10.189420	10.075836	10.265256	7
54	9.734939	9.924083	10 811124	10.189143	10.075917	10.205061	6
55	y./33135	0.022010	0.811410	10.100000	10.075999	10.264865 10 264670	5
27	9.725525	9.027827	0 811687	10.188712	10.076164	10.264475	4
28	Q.735710	9.923755	9.811064	10.188036	10.076245	10.264281	3 2
				10.187759			7
60	9.736109	9.923591	9.812517	10-187483	10.076400	10.262801	0
	Co.sine.		Co-tang.			Secant.	N
1	30.01101	~		Domese	, OU-366.	- Secant. I	A

		•	33 1	Degrees.		المي المبادرات عرود والمراجع الم	-
×	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-se c	M ·
10	726100	0.022501	0.812517	10. 187483	10-076400	10.26 2891	60
1 ,	'0.736203	0.623600	0.812704	10.187206	10.276491	10.263697	5
1 2	0.726408	0.021427	0.812070	10.186930	10.076572	10.263502	58 .
2	0.726602	0.022245	0.813347	10.186653	12.076655	10.263308	5-
3	9.736886	0.022262	0.812622	10.186377	10 076737	10.263114	56
14	9.73000	9.923281	0 812800	10.186101	10.076810		55
5 6	10 727274	0.022008	0.814175	10.185825	10.076002		54
7	9-73:-74	0.923036	0.814162	10.185548	10.076084		53
8	0.727661	0.022022	0.814728	16.185272	10.077067	10.262339	52
4	0 727855	0.022861	0.815004	10.184996	10.077140	10.262145	51 ;
10	9.737033	0.022768	0.815270	10.184721	10.077232	10.261952	50
111	19.738241	9.922686	9.815555	10.184445	10.077314	10.261759	49
12	9.738434	9.922603	9.815831	10.184169	10.077397	10.261566	48
13	9.738627	9.922520	9.810107	10.183893	10.077480	10.261373	47
.14	9.738820	9.922438	9.816382	10.183618	10.077502	10.261180	46
15	9.739013	9.922355	9.816658	10.183342	10.077045	10.260987	45
16	9.739206	9.922272	9.816933	10.183667	10.077728	10.260794	44
17	9.739398	9.922189	9.817209	10.182791	10.077811	10.260602	43 1
18	9.739590	9.922106	9.817484	10.182516	10.077894	10.260410	42
119	9.739783	9.922023	9.817759		10.077977		41
20	9.739975	9.921940	9.818035	10.181965	10.078060	10.260025	40
21	9.740167	9.921857	9.818310	10.181690	10.078143	10.259833	39
22	9.740359	9.921774	9.818585	10.181415	10.078226	10.259641	38
123	9.740550	9.921691	9.818860	10.181.140	10.078309	10.259450	37
24	0.740742	9.921667	9.810125	10.180865	10.078393	10.259258	36
25	9.740934	0.021524	9.819410	10.180590	10.078476	10.259066	35
. 26	9.741125	0.921441	9.819684	10.180316	10.078559	10.258875	34
27	9.741316	9.921357	9.819959	10 180041	10.078643	10.258684	33
28	9.741508	9-921274	9.820234	10-179766	10.078726	10.258492	32
4 29	9-741600	9.921190	9 820508	10.179492	10.078810	10.258301	31
30		9.921107	9.820783	10.179217	10.078893	10.258111	30
-		9.921023		10.178943		10.257920	29
31	9.742060	9.921023	0.821037			10.257729	28.
32	_	9.920939	0.821532	10.178304	10.079144		27
33		9.920856			10.079144		26
34	9.742052	9.920772	0.822154	10.177846	10.079312	_	25
35	9.742042	9.920688	9.822134	10.177571			24
36				10.177297			23
37					10.079564		22
138		9.920436			10.079648	,	21
339		.9.920352 y.920268		_ *	10.079732	1	20
40							
41		9.920184		_	10.079816		19
42		9.920099			10.079901		18
43		9.920015			10.079985		17
44	9-744550	9.919931	9.824519			10 255450	16
45		9 9 1 9 8 1 6	9.8 24 893		10.080154		15
46	1			10.174834	10.080238	10.255072	14
47		9.919677			10 080323	1 - 1	13
48	J '	9-919593	9.825713		10.080407		12
49						10.254506	11
50		9.919424				10.254317	10.
51	9.745871	9.919339	9.826532	10.173468	10.080661	10.254129	9
52	9.746060	9.919254	9.826805	10.173195	10.080746	10.253940	8
53	9.746248	9.919169	9.827078	10.172922	10.080831	10.253752	7
54	9.746436	9.919085	9.827351	10.172649	10.080915	10.253564	6
55	9.746624	9.919000	9.827624	10.172376	10.081000	10.253376	5
56	19.746812	9.918915	9.827897	10.172103	10.081085	10.253188	4
57	9.746399	9.918830	9.828.170	10.171830	10.081170	10.253001	.3
58	9.747187	9.918745	9.828442	10.171558	10.081255	10.252813	. 2
59	9.747374	9.918659	4 828715	10.171485	10.081341	10.252626	1
د 6.	7.717562	9.918574	9.828987	10.171013	10.081426	10.252438	0
- (Co-tang.		Co-sec.	Sicant	
.T_M	Co-sine	· JIIIC.	· Co-tailg.	. 1 % . X .	00-300.	Di Calit	AL I

				Jegrees.			
×	, Sine.	Co-sine.	Tang.	Co-tang.	Secant '	Co-sec.	×
0	9.747562	9.918574	9.828987	10.171013	10.081426	10.252438	60
i	9.747749	9.918489	9.829260	10.170740	10.081511	10.252251	59
2				10.170468		10.252064	58
3	9.748123	9.918318	9.829805	10 170195			57
4	9.748310	9.918233	9 830077	10.169923	10 081767	10.251690	56
5	9.748497	9.918147	9.830349	10.169651		10.251503	55
6				10.169379		10.251317	54
7				10.169107	10.082024	10.251130	53
8				10.168835	10.082109	10.250944	58
9				10.168563	10.082195	10.250757	51
10		·		10.168291		10.250571	50
11		9.917634		10.168019			49
12			9.832253	10.167747	10.082452		48
13			9.832525	10.167475	10.082538		47
14				10.167204		, , , ,	46
115			9.833068		10.082713		45
16			9.833339		10.082790	10.249457	44
17			9.833611 9.833882	10.166389	10.082968	10.249271	43
•			9.834154		10.082988		42 41
19			9.834425		10.083141	10.248716	40
I						}	
21			9.834090 9.83 496 7	10.165304		10 248531	39
22				10.164762		10.248346	38
73				10.164491	10.082486	10.247977	37 36
24 25						10.247792	35
26				10.163949		10.247608	34
27				10.163678		10.247424	33
28				10.163407		10.247240	
29				10.163136		10.247056	31
30				10.162866		10.246872	30
31	9.753312	9.915907	9.837405	10.162595	10.084093	10.246688	29
32						10.246505	28
33					10.084267		27
34						10.246138	26
35				10.161513		10.245954	25
36	9.754229	9.915472	9.838757	10.161243	10.084528	10.245771	24
37						10.245588	23
38						10.245405	22
39						10.245222	21
40	1				10.084877		20
41					10.084965	1	19
42				10.159622		10.244674	18
43						10.244492	17
44						10.244310	16
45				10.158813		10.244128	15
46				10.158543		10 243946	14
47 48				10.158274		10.243764	
49				1	10.08 : 666	10.243400	II
50						10.2432181	
					-	10.243037	
5 I 52	0.757144	0.014020	0.842074	10.15/195	10.005042	10.243037	9
53					10.086018		7
54						10.242493	6
55					10.086194		5
56						10.242131	4
57						10.241950	3
58	9.758230	9.913541	9.844689	10.155311	10.0864591	10.241770	2
59	9.758411	6.913453	9.844958	10 155042	10.086547	10.241589	. 1
60	9.758591	9.913365	9.845227	10.154773	10.086635	10.241409	0
M	Co-sine.	Sine.	Co-tang	Tang.	Co-sec	Secant	M
				20000			

-				begrees.			• • • • • • • • • • • • • • • • • • • •
M	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	М
0	9.758591	0.013365	9 845227	10.154773	10.086635	10.241.100	60
]]	9.758772	9.913276	9.845496	10.154504	10.086724	10.241228	59
2	9.758952	9.913187	9.845764	10.154236	10.086813	10.241048	58
3	9.759132	9.913099	9.846033	10.153967	10.086901	10.240868	57
4	9.759312	9.913010	9.846302	10.153698	10.086990	10.240688	56
5	9.759492	9.912922	9.846570	10.153430	10.087078	10.240508	55
6	9-759672	9.912833	9.846839	10.153161	10.087167	10.240328	54
7	9.759852	9.912744	9-847107	10.152893	10.087256	10.240148	53
8	9.760031	9.912655	9.847376	10.152624	10.087345	10.239969	52
9	9.700211	9.912500	9.847644	10.152356	10.087434	10.239789	51
					10.087523		50
1 2	9-760569	9.912388	9.848181	10.151819	10.087612	10.239431	49
12	9.700748	9.912299	9.848449	10.151551	10.087701	10.239252	48
13	9.700927	9.912210	9.848717	10.151283	10.087790	10.239073	47
1 :4	9.701100	9.912121	9.848980	10.151014	10.087879	10.238894	46
1 :2	9.701205	9.912031	9.049254	10.150740	10.087969	10.238715	45
17	0.761642	0.011862	0.049522	10.1504/8	:0.088058 10.088147	10.238536	44
18	0.761821	0.011762	9.849/90	10.130210	10.088237	10.230350	43
1 10	9.761999	0.011674	9.850325	10.140675	10.088326	10.238001	42 41
20	9.762177	9.911584	4.850593	10.149407	10.088416	10.237823	40
					10.088505		_
22	9.762524	0.011405	9.050001	10.149139	10.088595	10.237044	
23	9.762712	0.011316	0.851306	10.148604	10.088685	10.237488	38 37
24	9.762889	9.911226	9.851664	10.148776	10.088774	10.237111	36
25	9.763067	9-911136	9.851931	10.148069	10.088664	10.236023	35
26	9.763245	9.911046	9.852199	10.147801	10.088954	10.236755	34
27	9.763422	9.910956	9.852466	10.147534	10.089044	10.236578	33
28	9.763600	9.910866	9-852733	10.147267	10.089134	10.236400	32
29	9.763777	9.910776	9.853001	10.146999	10 089224	10.236223	31
30	9.763954	9.910686	9.853268	10.146732	10.089314	10.236046	30
			9.853535	10.146465	10.089404	10.235869	29
32	9.764308	9.910506	9.853802	10.146198	10.089494	10.235692	28
33	9.764485	9.910415	9.854069	10.145931	10.089585	10.235515	27
34	9.764662	9.910325	9.854336	10. 145664	10.089675	10.235338	26
			9.854603	10.145397	10.089765	10.235162	25
30	9.705015	9.910144	9.854870	10.145130	10.089856	10.234985	24
			9.855137	10.144803	10.089946	10.234809	23
30	0.765544	0.000872	0.866671	10.144590	10.090037	10.234033	22
40	0.765720	0.000782	0.855018	10.144062	10.090127	10.234450	21
							20
41	0.766077	0.000601	0.866.	10.143790	10.090309	10.234104	19
42	0.766947	9.909001	0.856727	10.143529	10.090399	10.233928	18
41	9.766422	0.000410	0.857004	10.143203	10.090490	10.2225753	17 16
45	9.766508	9.900128	9.857270	10.142720	10.090672	10.222402	15
	9.766774	9.900277	9.857577	10.142462	10.090763	10,22226	14
47	9.766949	9.909146	9.857803	10.142197	10.090854	10.233061	13
48	9.767124	9.909055	9.858069	10-141931	10.090945	10.232876	12
49	9.767300	9.908964	9.858336	10.141664	10.091036	10.232700	11
50	9.767475	9.908873	9.858602	10.141398	10.091127	10.232525	10
51	9-767649	9.908781	9.858868	10.141132	10.091219		
52	9 767824	9.908690	9.859134	10.140866	10.091310	10.232176	9
53	9 767999	9.908599	9.859400	10.140600	10.091401	10.232001	7
54	9.768173	9.908507	9.859666	10.140334	10.001403	10.231827	6
55	9.768348	19.908416	9.859932	10.140068	10.001584	10.231652	5
56	9.768522	9.908324	9.860198	10.139802	10.091676	10.231478	4
57	9.708097	9.908233	9.860464	10.139536	10.091767	10.231303	3
50	9.700071	9.908141	9.860730	10.139270	10.091859	10-231129	2
1 59	9.709045	9.908049	9.800995	10.139005	10.091951	10.230955	I
	distances of the last of the l				10.092042		0
M	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant	×
-			54 D	egrees.			

36 Degrees.

-		والمستقول المراجع المراجع المراجع	مرور ومرجو بمجيوني	Degrees.	ب کارست فرسیت پیستی		
31	Sine.	Co-sine.	Tang.	Co-tang	Secant.	Co-sec.	×
0	2.760210	0.027058	0.861261	10.138739	10.002042	10.230781	60
				10.138473	10.092134		54
				10.138208	:	10.230434	
				10.137942		10.230260	
				10.137677		10.230087	
				19.137411		10.229913	_
				10.137146		10.229740	
				10.136881	1 7 7 1 1	10.229567	
				10.136615		10.229394	52
				10.136350		10.229221	5 t
				10.136085		10.129048	50
T							
				10.135820		10.228875	49
						10,228530	47
			_	10.135025			46
						10.228185	_
						10.228013	45
				10.134230			43
_ ,			9.866035			10.227669	42
						10.227497	41
						10.227325	40
5 !		ı ———				-	
			9.866829		10.093982		39
						10.226982	38 -
			9.867358			10.226810	37
			9.867623		10.094261		36
26	9.773533	,9.905045	9.867.667	10.132113	10.094355	10.226467	35
						10.226296	
28	9·//3º/5	9.905459	0.868680	10.131504	10.094541	10.226125	33 32
						10.225783	
						10.225612	
							~
			9.869473			10.235442	29
			9.869737		10.095008		28
			9.870001		10.095102	-	27
			9.870265			10.224930	26
			9.870529			10.224760	25
			9.870793		10.095383		24
			9.871057			10.224420	23
			9.871321		10.095571		31
10	9.775920	9.904335	9.871585	10.128415	10.095665		
			9.871849			10.223910	20
				10.127888			19
				10.127624			18
				10.127360			17
				10.127097			16
						10.223063	15
				10.126570			14
						10.222725	13
40,9	7·// 444	9.903487	9.073957	10.126043	10.090513	10.222550	12
				10.125780			11
 .				10.125516			10
51/9	9.777950	9.903203	9.874747	10.125253	10.096797	10.322050	9 .
52'9	9.778119	9.903108	9.875010	10.124990	10.096892	10.221881	
53:5	3.778287	9.903014	9.875273	10.124727	10.096986	10.321713	7
				10 124464			6
55!5	7.778624	9.902824	9 75800	10.124200	10.097176	10.221376	5 ;
50.9	778792	9.902720	v. # 10063	10.123937	10.097271	10.221208	4.
57 9	778960	9 902734	9.876326	10.123674	10.097366	10.221040	3
58 9	779128	9.902539	9.876589	10 123411	10.097461	10 220872	2
59 9	779295	9 902444	9.876851	10.123149	10.097556	10.220705	1
0.9	779463	9.902349	3.877114	10.122896	10.097651	10.230537	<u> </u>
м	Co-sine.	Sine.	Co-tang	lang '	Co-s c	Secant	M
	-		30				

37 Degrees.

37 Degrees.									
M	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec_	M		
	0.770461	0.003240		10.122686		10.220537	60		
	9.779631				10.097747		4		
				10.122360			59 58		
				10.122097			57		
						10.219867	56		
						10.219700	55		
						10.219533	54		
						10.219366	53		
						10.219199	52		
						10.219032	51		
	9.781134					10.218866	50		
					l i				
				10.119997			49		
12	9.781408	9.901202	9.880205	10.119735	10.098798	10.218532	48		
13	9.781034	9.901106	9.880528	10.119472	10.098894	10.218366	47		
14	9.781800	9.901010	9.880790	10.119210	10.098990	10.218200	46		
15	9.781900	9.900914	9.881052	10.118948	10.099086	10.218034	45		
10	9.782132	9.900818	9.881314	10.118686	10.099182	10.217868	44		
17	y. 703295	9.900722	9.001576	10.118424	10.099278	10.217702	+3		
40	9.702404	9.900020	9.001039	10,118161	10.099374	10.217536	42		
19	9./04030	9.900529	9.002101	10.117899	10.099471	10.217370	41		
						10.217204	40		
21	9.782961	9.900337	9.882625	10.117375	10.099663	10.217039			
22	9.783 127	9.900240	9.882887	10.117113	10.099760	10.216873	38		
23	9.783292	9.900144	9.883 t48	10.116852	10.099856	10.216708	37		
24	9.783458	9.900047	9 883410	10.116590	10.099953	10.216542	36		
25	9.783623	9.899951	9.883672	10.116328	10.100049	10.216377	35		
26	9.783788	9.899854	9.883934	10.116066	10.100146	10.216212	34		
27	9.783953	9.899757	9.884196	10.115804	10.100243	10-216047	33		
28	9.784118	9.899660	9-884457	10.115543	10.100340	10.215882	32		
29	9.784282	9.899564	9 884719	10.115281	10.100436	10.215718			
30	9.784447	9.899467	9.884980	10.115020	10.100533	10.215553	30		
31	9.784612	9.899370	9.885242	10.114758	10.100630	10.215388	29		
32	9.784776	9.899273	9-885503	10.114497	10.100727	10.215224			
				10.114235		10.215059	27		
				10 113974		10.214895	. •		
				10.113712		10.214731			
				10.113451		10.214567	24		
				10.113190		10.214403	23		
				10.112928	_	10.214239	22		
				10.112667		10.214075	21		
				10.112406		10.213911	20		
			-			10.213748	19		
						10.213584	18		
						10.213421	17		
						10.213258	16		
						10.213094	15		
				10.1110840			14		
47	0.787222	9.807810	9.880421	10.110.70	10.102100	10.212768	13		
48	9.787205	9.807712	0.880682	10.110218	10.102288	10.212605			
40	9.787557	9.807614	9.880042	10.110067	10.102286	10.212443	11		
50	9.787720	9.897516	0.800204	10.100706	10.102484	10.212280			
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51	9./0/303	9.09/410	9.090405	10 109535	10.102582	10.212117	9		
52	0 28620	9.097320	9.090725	10.109275	10 102080	10.211955	0		
53	0 465444	9.097222	9.890986	10.109014	10.102778	10.211792	7		
54	y. / 00370	9.097123	9-091247	10.108753	10 102877	10.211630	6		
5.5	7./00532	9.897025	9 891507	10.104493	10.102975	10.211468			
50	9. / 00094	9.090920	9.091708	10.108232	10.103074	10.211306	4		
57	y /00050	9.090028	9.892028	10.107972	10.103172	10.211144	3		
5.0	9.709018	9.090729	9.892289	10.107711	10.103271	10.210982	_		
59	9.709180	9.090031	9.892549	10.107451	10.103369	10.210828	I		
00			9.092810	10.107190	10.103468	10.210650	0		
м	Co-sine.	Sine.	Co-tang	Tang.	Co-sec.	Secant.	м		
1				Degrees					

52 Degrees.

38 Degrees.

-				Degrees.			
M	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	×
0	9.789342	9.896532	9.892810	10.107190	10.103468	10.210658	60
1	9.789504	9.896433	9.893070			10.210496	59
2		9.896335			10.103665	10.210335	58
3		9.896236		_ * *	10.103764	, , ,	57
4		9.896137		10.106149		10.210013	56
5		9.896038			10.103962		55
6		9.895939			10.104061	10.209690	- '
7		9.895840			10,104160		
		9.895741 9.895 6 41			10.104259 10.104359	10.209368 10.209207	- 1
9					10.104458		50
! -					-	-	
11		9.895443			10.104557		
		9.895343 9.895244					
13				10.103548			46
15					10.104955	•	45
16		9.894945				10.208083	44
17					10.105154	•	43
18		9.894746			10.105254		42
19	9.792397	9.894646	9.897751	10.102249	10.105354	_ 1	41
20	9-792557	9.894546	9.898010	10.101990	10.105454	10.207443	40
21	9.792716	9.894446	9.898270	10.101730	10.105554	10.207284	39
22	9.792876	9.894346	9.898530	10.101470	10.105654		
23		9.894246					
24	9.793195	9.894146	,9.899049	10.100951	10.105854		
25	9.793354	9.894046	19.899308	10.100692	10.105954	10.206646	35
26						10.206486	_
27						10.206327	
28						10.206168	
29 30						10.206009 10.205850	
31						10.205692	
32					10.106657		
33 34					10.106858		_
35		_			10.106959		
36						10.204899	_
37) " ·			10.204741	
38	9.795417	9.892739	9 902679	10.097321	10.107261	10.204583	22
39					10.107362		
40	9.795733	9.892536	9.903197	10.096803	10.107464	10.204267	20
41	9.795891	9.892435	9.903455	10.096545	10.107565	10.204109	19
42	9.796049	9.892334	9.903714	10.096286	10.107666	10.203951	
43	9.796206	9.892233	9.903973	10 096027	10.107767	- 1 - 1	
44				10.095768	•	10.203636	
45		9.892030					
46					10.108071		14
48					10.108173		- 1
48 49					10.108274 10.108376		
50				10.094216			
J	·						
51					10.108579 10.108681		
52						10.2023/9	7
53						10.202066	6
55						10.201909	
56						10.201753	
57					10.109191		
58	9.798560	9.890707	9.907852	10.092148	10.109293	10.201440	2
59					10.109395	1	
60	9.798872	9.890503	9.908369	10.091631	10.109497	10 201 128	0
M	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant	M
	-			Jegrees			

M					Degrees.			
2	7	dine.	Co-sinu	Tang	Co-tang	Secant	Co-are.	м
1 0.790088 0.800082 0.000638 10.000708 10.000816 5 7.790189 8.800193 0.000164 10.000708 10.000661 5 7.790189 8.800193 0.000664 10.000856 10.000807 10.000666 5 7.790806 0.800808 0.000668 10.000080 10.000666 5 7.790806 0.800808 0.800818 0.000808 10.000080 10.00080 10.0	ŀ			_ 	10.00144		10 10111	64
1	1 2	9.798873	d eletel		10.091031	10 loggy	10 101112	- 1
2 9 1993 18 1901 19 1904 10 10 10 10 10 10 10	1	& TOUGHT	n. Hydadc	9.900038	10 091171	to toduco	10.1130371	39
0 1790000 1800000 1900000 10 1000000 10 10	1.5							-
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0	1 4	9 799691	e Becky t	9 909401	to oposal	10.109907	10.100505	56
		0.700011	e Hiseso	g gayáta	10 090340	10.113010	10 100 140	44
1	14							
	L							
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13		9.000427	9.449477	1. Ca. 1. A.A.				
	44	g.floog Ba	9. 689314				F F -	49
	1.3	9.800157	g. Bligare	9 9 1 1 4 6 7	, , , , , ,			48
16	11	g Bootigs	a \$80 - 68	9.911784	10-088176	10 110671	10.199108	47
1.	14	9 BD1047	g. \$14064	a figit se o	10 085013	10 110936	10.198943	46
16	14				10 08*750	10.111014	10.165700	-
	1.6				16.087 (01	10.111148	10 198644	
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20	1	4 '						
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1	11	9.802148	m ** 41	9.913787	10 056213	10.111659	10.197871	
1	11	g Boasta	9 2 2 7 2 2 7	9-914044	10 OF COL	10.111763	10.197718	36
0 0 0 0 0 0 0 0 0 0	11	9 804416	9 15 hart 4	9 914305	10.00 5698	10-11-506	, 19. 197 5041	
10 0.800897 0.1 1.1 0.9 1.6817 10.0 10.11 10.19 10	14	9.801480	9 5 22	9-914580	10.06 4440	10.111970	10 (9.44)	36
10 0.808807 0.11 11 0.011607 10 0.101607 13 0.101609 13 14 0.101609 13 0.101609 13 0.101609 13 0.101609 13 0.101609 13 0.101609 13 0.101609 13 0.101609 14 0.101609 13 0.101609 14 0.101609 15 0.101609	1.0		g filmerði	9 914817	10 085183	10.111074	[19.197257]	35
1			mat tag	9-914974	10 084985	[10.612178	10.197103	
10 10 10 10 10 10 10 10			g to vell	0-01(11)	10 684668	10.119189	10.196930	
29 9.807357 9 11 10 915847 10 084153 10 118400 10.190663 31 9.807314 9 17 10 9 16164 10 10.13596 10.118596 10.19080 30 10.19080 30 10.19080 30 10.19080 30 10.19080 30 10.19080 30 10.19080 30 10.19080 30 10.19080 30 10.19080 30 10.19080 31 10.1908			0 1 F - 0 A	0.415100	10 084410	10 111286	10 196796	
10 0.0986. 0.0086.								_
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	3.0	9.301444	4.337 JOS	9-910363				
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06 LOGARIFHENIC SERSE, TANCENTS, AND SECANTS.

_			40 1	Jegrees.			
26)	Sinc	Co-sine	3 ang	Co tang		Co-sec.	26
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1			9.924840		10.116171	10.191111	56
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-	, , ,	4	9.935352		10.116490		53
21	a South	9 887171	9-925866	10 074175	10.116596	10 100711	51
	o Scorio	0 88110	9 925131	10.072578	10.116703	20, 190 (81	51
10	o. Boacha	u 881191	9 926 27\$	10 0* 1612	10.116809	10 190431	50
				10.073366		10 100382	49
011	0 \$20868	u. \$8.20**	6 0268uC	12 27 3710		10.190753	48
	0 \$13017	0.882871	9.927147	10 011853	10.117129	10.189481	47
			9.927403	,		10.119833.	46
				10.073341		10 119684	45
		1.	9 927915	10.072085	10.117450	10.189535	44
12	9.810614	9 882443	4 4281"1	10 071319			43
			9 928427			10 189137	48
19	9.710912	9 882229	9 928683	10.071317		10.189088	41
20,	9.811061	9 882121	9 928440	10.071060	10 117879	10.181939	40
11,	9 \$11310	9 862314	9.929196	10.070804		10.188790	39
			1	10 010548			38
23	g Stigor	9.881799		10 070191			4
34	9.311655	9.881692	4 030004	10 0 00 00 16	19.11\$30\$	10.185345	36
			9 9 30 120		10. 618416	10.188196	35
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			9.931494	10.068501			10
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3-	9 \$13578	9.880180	9.933180	10 066-11	10.119711	10.186412	23
					10. 119820	10.186275	31
39.	9.813878	9 5500-2	4 913800	10 066 200	10 119928	10.186128	31
40	9.814019	9 8-9963	9 954055	10.06 5944	10.130037	10.185981	30
411	9.8:4168	9 879856	9 934311	10.06 5684	10.140145	10.185834	19
443.	9 814313	19 8 9 46	9 9:456"	10 06 (433	10.120154	10.135681	18
431	9.814460	9 879637	9.934813	10.065177	10.120363	10.185540	12
441	9 R 1460"	198-9529	9 9350-8	10.064932	10.110471	10.115393	16
					10 130220		LS
40	9 814900	9 8 9311	9 935589	10.064411	10 123689	10.185100	14
					10,130798		13
40	9 015193	9 879093	9 9 30 100	10.063900	10 120907	10.184807	-
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4.		9.847088	9-377670	9.939418				59.
łi -			9.877560			10.122440		58
41				9.939928		10.122550	_	57
£	4	9.817524	9 577340	9.940183		10.122660	_ • •	56
1.	5	9.817668	9.877230			10-122770		55
4			9.877120			10.122880	_ ' '	54
1	7	9.817958	9-877010	9.940949	10.059051	10.122990	10.182042	53
j .	8	9.848103	9.876899	9.941204	10.058796	10.123101	10.181897	52
ŀ			9.876789		10.058542	10.123211	10.181753	51
1 1				9.941714	10.058286	10.123322	40.181608	50
- I					-	Street, or other Persons and Publishers.	-	
			9-876568			10.123432		
•		•	9-876457			10.123543		
				9.942478		10.123653		47
-	•	-	9.876236			10.123764		46.
				9.942988		10.123875		45
			9.876014			10.123986		44
4	17	9.819401	9.875994	9-943498		10.124096		43.
1 1	18	9.819545	9.875793	9-943752	10.056248	10.124207	10.180455	42
			9.875682		10.055993	10.124318	10.180311	414
			9.875571			10.124429		427
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			9.875459				10.180034	39
			9.875348				10.179880	_
				9.945026		10.124763		37.
			9.875136			10.124874		36
1 2	25	9.820550	9.875014	9-945535	10.054465	10.124986	10.179450	, 35
1 1	26	9.820693	9.874903	9-945790	10.054210	10.125097	10.179307	, 34,2
1 1	27	9.820836	9.874791	9.946045	10.053955	10 125209	10.179164	33.
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1 :	20	0.821122	9.874568	9-946554	10.053446	10.125432	40.178878	31
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	32	9.824 550	9.074232	9-947318			10.178450	
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				9.948844			10.177596	
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1	40	9.822688	9.873334	9-949353	10-050647	10.126665	10.177312	20
	<u> </u>		9.873223		10.050202	10.126777	10.177170	19.
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				9-959879		10.127341		14
14	47	9.843080	9 072547	9.951133	•	10.127453		13
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1	58	9.325230	9-07/301	9.953929	10.040071	10.128099	10.174776	2
	59	9 835371	9-371187	9.954183	10.045817	10.128813	10.174629	1
	60	9.825511	9-871073	9-954437	10.045563	10.128927	13.174489	
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и,	Sine-	Co-sine.	Tang	Co-tang	Secant	Co-sec.	30
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11	9 933919	9.804010	9,909909	10.030001	10 135990	10 160001	19
2	9 834264	9 30 3891	9 9 70162	10.010939	10 136108	10 102010	58
3	9.834189	9 \$63774	9 9 704 16	13.029584	10 136216	10 165811	57
4	9.814116	9.863656	9.970669	10.029331	10 136344	40.165675	56
اة	4. 8 24460	9 86 25 28	0.070011	10.020078	10 136462	10.16 (140	55
6	0 824.06	0 862410	0.071176	10.018824	10 136581	10 165405	54
<u> </u>	7 -34191	9 26 1404	9971179	10 018-01	10 136699	10 16 (170)	
61	9 834-30	9 803301	4 971449	10.0145	10 130099	10.10,270	53
					10-136817		52
9	8 3499A	9 80 1004	9 971935	10.028005	10. 136936	10 10 5001	51
10	9-835134	9.862946	9 972188	10.017811	10.137054	10 164866	50
						10.164731	
	9 113 1 209	9.00202	9 9 3444	10.027559			49
				10.027306	10 137291		48
				10 034053	10.137410		47
14	9 8356-2	9.862471	9 97 3 201	20.026799	10.137529		46
15,0	9.835807	9.862357	9 97 1454	10.016546	10.13-647	10.164193	45
26.4	140218.0	9. 86232A	9.97 1707	10.020293	10. 137766		44
17	8 26075	9 862111	0.022060	10,026040	10.137885		43
42	8 16200	0.861006	3.47,3400	10.025787	10-138004		
	8 14 2 4	24.8-	4 4 4 4 1 3	10.0025			42
19	0 10343	9.001377	3 34400	10 025 534	10 138123		41
30.	9 8 30477	9-201758	9 974719	10 025 181	10 138242	10.103523	40
21	9 8 16611	9.861638	G G*AG71	10.025027	10.138361	10 161180.	39
22	0.82674	0.861.10	9 9 9 5 2 2 6	10.014774	10 138481		39
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44	9 837012	9.001250	9-975738	10.024268	10 138710		36
25	9 837146	6-201101	4 975985		10 138839		35
30	9 537279	9.861041	9.976138	10.013762	10 138459	10-162721	34
37	9 837412	9.860922	9.976491	10 023509	10 139078,	10.162522	33
28	9 827546	9.960802	9.976744	10.023256	10 139198		32
20	9 817679	0 860682	9 476947	10 023003	10 139318		31
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31	9 83-945	9.860442	9 9 503	10.022497	10 139558	10-101055	19
31	9.838078	9.860322	9.97776	10.011344	10 139618	10-161913	18
33	9 8 3 8 2 1 1	9 860201	9.978000	10,021991	10 139798	10.161789	27
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			9 980033		10 140761		19
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45	9 839830	9 8 , 87 56	9.981044	10.018956	10.141244		16
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		9 858272		10.017944	10.141728	10. 159672	11
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29 COGARITHMOCHINES, TARGENTS, AND SECANDRA

44 Begrees.

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TABLE. III.

Natural Sines.

In this table the natural sines are exhibited to every degree and minute of the quadrant, and arranged so that the degrees corresponding to the sines are to be taken from the top of the page with their minutes in the left side columns, and the degrees answering to the co-sines from the bottom with their minutes in the right side columns.

The natural sine or co-sine of any number of degrees, &c. more than 90, is the same as the natural sine or co-sine of its supplement, found by subtracting them from 1800; or the natural sine or co-sine of an arch greater than 900 is the natural co-sine or sine of its excess above 90°.

To find the natural Sine or :Co-sine of a given Number of Degrees,
Minutes, and Seconds:

Or, to find the degrees, Minutes, and Seconds, corresponding to a given natural Sine or Co-sine.

These are to be found as directed for the logarithmic sines, &c. except that the differences to 100" are to be taken from the bottom of that column containing the given degrees in the former case, or the nearest natural sine or co-sine in the latter.

EXAMPLE L

Require The n	red the atural	natu: sinc	ral Sine of 320	of 3202 21' is	21'45 ' -	', or i -	its Suj	pplem -	ent 147	9 38' 15". 535090
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TRAMPLE 11.

Required the natural Co-sine	of 710	40'	25", 0	1080	19'	35".
The natural co-sine of 71° 40' is	•	•	•	•	•	314545
The difference 460, multiplied; by	85, poin	ting	off two	figure	3, i	115

Remainder is the natural co-sine required - - - 314430

EKAMPLE III.

Required the Degrees, Minutes, and Seconds, answering to the natural Sine 495994.

The natural sine next less to that given is 495964, answering to 29° 44'; the difference between this natural sine and the given one is 30, to which two cyphers being added, and that divided by 422, the difference at the bottom of the column, gives the quotient 7" to be annexed to 29° 44'. Hence 29' 44' 7", or its supplement 150° 15' 53", are the degrees, &c. required.

EXAMPLE IV.

Required the degrees, Minutes, and Seconds, answering to the natual

The natural Co-sine next greater to that given is 368936, to which answers 68° 21'; the difference between this natural sine and the given one is 131, to which two cyphers being added, and that divided by 451, the difference found at the bottom of the column, gives the quotient 29". Hence 68° 21' 29", or its supplement, 111° 38' 31" are the degrees, &c. required.

To find the natural versed Sine of a given Number of Degrees, Minutes, and Seconds.

If the given arch be less than 90°, find its natural co-sine, which subtract from 1000000, and the remainder will be the natural versed sine required. But if the given arch exceed 90°, find the natural co-sine of its supplement, which add to 1000000, and the sum will be the natural versed sine required.

EXAMPLE Í.

Required the natural versed Sine of 20° 39'.

The natural co-sine of 20° 39' is 935752, which subtracted from 1000000, leaves 064248, the natural versed sine of 20° 39'.

EXAMPLE ÍÍ.

Required the natural versed Sine of 146° 38' 40."

The natural co-sine of 33° 21' 20" (the supplement of 146° 38' 40") is 835274, which added to 1000000, the sum 1835274 is the natural versed sine required.

To find the Degrees, &c. corresponding to a given natural versed Sine.

Take the difference between the given natural versed sine and 1000000, and the remainder will be a natural co-sine; the degrees, &c. corresponding to which, will be those required, if the given natural versed sine be less than 1000000, but if otherwise, it will be their supplement.

EXAMPLE I.

Required the Degrees, &c. answering to the natural versed sine 098965.

The above subtracted from 1000000, leaves 901035, which taken as a natural co-sine, corresponds to 25° 42′ 20″.

EXAMPLE II.

Required the Degrees, &c. answering to the natural versed Sine 1160172. Here 1000000 subtracted from the above, leaves 160172, which taken out as a natural co-sine, corresponds to 80° 46′ 59″; therefore its supplement 99° 13′ 1″ are the degrees, &c. required.

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<u></u>	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	_	81	33	45			
		71	84	22		71		
		7	87	11	15	3		}
East.	West.	8	90	0	0		East.	West.

TABLE V.

A TRAVERSE TABLE,

To every Degree and Quarter Degree of the Compass or Horizon.

EXPLANATION.

This Table is calculated for the easy and expeditious solution of the several cases of Right-angled Plane Trigonometry. It is generally esteemed a useful and requisite assistant to the Surveyor, the Navigator, and to every one, who has any concern with trigonometry in the exercise of his profession. The manner of using it must be very obvious to all, who are acquainted with the principles of that excellent branch of geometry; but to those, who have only a superficial knowledge of the subject, the following description and examples will be necessary.

In this Table, one of the acute angles—whether given, or required—
if less than 45°, is found, to the nearest 15' at the top of the page; but,
if more than 45°, it must be sought at the bottom, where the numbers
are found in a retrograde order. And whether the angle under consideration, be at the top, or bottom, the Hypothenuse, if less than 120, is
always in a Distance column; against which, in a column marked Latitude, is found the side contiguous to the angle; and in a column,

marked Departure, the side opposite the angle.

When the given numbers exceed the limits of the table, any aliquot parts, such as a half, one third, &c. may be taken; and those found corresponding are to be doubled, trebled &c. that is, multiplied by the same figure, that the given number is divided by.

BXAMPLEL

1. Let the Hypothemuse of a right angled triangle = 96 and one of

the acute angles=33° 45'; required the sides.

Under 33° 45' at the top of the table, and against 96 in a Distance column, are found 79.84 in a Latitude column for the side contiguous to the given angle, and 53.34 in a Departure column for the side opposite the given angle.

2. Let the sides of a right angled triangle be=89.33 and 66.02;

required the angles and Hypothenuse.

By inspecting this table, till these two sides are found against each other in adjoining columns of Latitude and Departure, the angle opposite the longest side is found to be 530 30°, the other, 36° 30° and the Hypothenuse, 111.

In this manner all the cases of Right-angled Plane Trigonometry can be readily solved; but for more particular directions, beeks on this

subject should be consulted.

	15	1	Die	30		Dist.	45	
Dist	Lat.	Dep.	-	Lat.	Dep.	7	Lat.	Dep.
1	1.00	0.00	1	1.00	0.0 E	1	1.00	10.0
2	2.00	0.01	2	2.00	0.02	3	2.00 3.00	0.03
3	3.00 4.00	0.01 0.02	3 4	3.00 4.00	0.03	4	4.00	0.05
5	5.00	0.02	, ;	5.00	0.04	5	5.00	0.07
6	6.00	0.03	6	6.00	0.05	6	6.00	0.08
7	7.00	0.03	7 8	7.00	0.06	7	7.00 8.00	0.09
8	8.00 9.00	0.03	9	8.00 9.00	0.07	9	9.00	0.10 0.12
10	10.00	0.04	10	10.00	0.09	10	10.00	0.13
11	11.00	005	11.	11.00	0.10	11	11.00	0.14
12	12.00	0.05	12	12.00	0.10	12	12.00	0.16
13	13.00	0.06	13	13.00	0.11	13	13.00	0.17
14	14.00	0.06	15	15.00	0.13	15	15.00	0.20
16	16 00	0 07	16	16.00	0.14	16	16.00	0.21
17	17.00	0.07	17	17.00	0.15	17	17.00	0.22
18	18.00	0.08	18	1800	0.16	18	18.00	0.24
10	19.00	0.08	19 20	19.00 20.60	0.17	20	20.00	0.26
21	21.00	0.09	21	21.00	0.18	21	21.00	0.27
22	22.00	0 10	22	22.00	0.19	22	22.00	0.29
23	23.00	0.10	23	23 00	0 20	23	23.00	0.30
24	24.00	0.10	24	24.00 25.00	0.21	24	25.00	0.31
26	25.00 26.00	0.11	25	26.00	0.23	16	26.00	0.34
27	27 00	0.12	27	27.00	0.24	27	27 00	0.35
28	28.00	0.12	28	28.00	0.24	28	28.00	0.37
29	29.00	0.13	29	29.00 30.00	0.25	2 9	29.00 30.00	0.38
33	30.00	0.13	30		0.27	31	31 00	0.41
31	31.00	0.14	31	31.00 32.00	0.28	32	32.00	0.42
33	33.00	0.14	33	33.00	0.19	33	33.00	0.43
34	34.00	0.15	34	34.00	0.30	34	34 00	0.44
35	35.00	0.15	35	35.00	0.31	35	35.00	0.46
36 37	36 00 37.00	0.16	36 37	36.00 37.00	0.32	37	36.00 37.00	0.47 0.48
38	38.00	0.17	38	38.00	0.33	38	38.00	0.50
39	39.00	0.17	39	39.00	0.34	39	39.00	0 51
40	40.00	0.17	40	40.00	0.35	40	40.00	0.52
41 42	41 00 42.00	81.0	41	41.00 42.00	0.36	41	41.00	0.54
43	43.00	0.19	43	43.00	0 38	43	43 00	0.56
44	44.00	0.19	44	44.00	0.38	44	44.00	0.58
45	45.00	0.20	45	45.00	0.39	45	45.00	0.59
46 47	46.00	0.20	46	46.00	0.40	46	46.00 47.00	0.60
48	47.00 48.00	0.21	47 48	47.00 48.00	0.42	48	48.00	0.63
49	49.00	0.21	49	49.00	0.43	49	49.00	0.64
50	50.00	0.22	.20	50.00	0.44	50	50.00	0.65
51 52	51,00	0.22	51	51.00	0.45	51 52	51.00 52.00	0.67
53	52.00 53.00	0.23	52 53	52.06 53.00	0.45	53	53.00	0.99
54	54.00	0.24	54	54.00	0.47	54	54.00	0.71
55	55.00	0.24	55	55.00	0.18	55	55.00	0.72
56	56.00	0.24	56	56.00	0.49	56	56.00	0.73
57 58	57.00 58.00	0.25	57	57.00 58.00	0.50	57 58	57.00 57.99	0.75
59 60	59.00	0.25	58 59	59.00	0.51	59	58.99	0.77
	60.00	0.26	60	60.00	0.52	60	59.99	0.79
Dist.	Dep.	Lat	Bt.	Dep.	Lat.	Dist.	Dep.	Lat.
F	45) '	Dist.	30	/	Ω	1.	5'
			8	Degre	es.	-		

H	15			3.1		E	45	-
Dist.	Lat.	Dep.	Dist.	Lat.	Desp.	Dist.	Lai	Dep.
61	61.00		61	61.00	-			0.80
62	62.00	0.27 0.27	62	62.00	0.53	61 62	60.99	18.0
63	63.00	0.27	63	63.00	0.55	63	62.99	0.82
64	64.00	0.28	64	64.00	0.56		63.99	0.84
65	65.00	0.28	65	65.00	0.57	65	64.99	0.85
66	66.00	0.29	66	66.00	0.58	66	65.99	0.86
67	67.00	0.29	67	67.00	0.58	67	66.99	0.88
68	68.00	0.30	68	68.00	0.59	68	67.99	0.89
69	69.00	0.30	69	69.00	0.60	· 6 9	68.99	0.92
70	70.00	0.31	70	70.00	0.61	70	69.99	0.92
71	71.00	0.31	71	71.00	0.62	7 =	70.99	0 93
72	72.00	0.31	72	72.00	0.63	72	71.99	0.94
73	73.00	0.32	73	73.00	0.64	73	72.99	0.96
74 75	74.00 75.00	0.32	74 75	74.60	0.65	74	73.99	0.98
				75.00	distant	75	74.99	
76	76.00 77.00	0.33	76 77	76.00	0.66	76	75.99	0.99
77 78	78.00	0.34	78	77.00 78.00	0.68	77 7 8	76.99 77-99	1.02
79	79.00	0.34	79	79.00	0.69	79	78.99	1.03
80	80.00	0.35	80	80.00	0.70	80	79.99	1.05
81	00.18	0.35	81	81.00.	0.71	81	80.99	1.06
82	82.00	0.36	82	82.00	0.72	82	81.99	1.07
83	83.00	0.36	83	83.00	0.72	83	82.99	1.09
84	84.00	0.37	84	84.00	0.73	84	83.99	1.10
85	85.00	0.37	85	85.00	0.74	85	84.99	1.11
86	86,00	0.38	86	86.00	0.75	86	85.99	1.13
87	87.00	0.38	87	87.00	0.76	87	86.99	1.14
88	88.00	0.38	88	88.00	0.77	88	87 99	1.15
89	89.00	0.39	89	89.00	0.78	89	88.99	1.16
90	90.00	0.39	90	90.00	0.79	90	89.99	1.18
9.1	91.00	0.40	91	91.00	0.79	91	90.99	1.19
92	92.00	0.40	92	92.00	c.80	92	91.99	1.20
93	93.00	0.41	93	93.00	0.81	93	92.99	1.22
94	94.00 95.00	0.41	94 95	94.00	0.82	94	93-99	1.23
9						<u>95</u>	94.99	
96	96.00	0.42 0.42	96 97	96.00	0.84	96	95.99	1.26 1.27
97 98	97.00 98.00	0.42	98	97.20 98.00	0.85	97 98	96.99 97.99	1.28
99	99.00	0.43	99	99.00	0.86	99	98.99	1.30
100	100.0	0.44	100	100.0	0.87	100	99.99	1.31
101	101.0	0.44	101	101.0	0.88	101	101.0	1.32
102	102.0	0.45	102	102.0	0.89	102	102.0	1.34
103	103.0	0.45	103	103.0	0.90	103	103.0	1 35
104	104.0	0.45	104	104.0	0.91	104	104.0	1.36
105	105.0	0.46	105	105.0	0.92	105	105.0	1.37
106	106.0	0.46	106	106.0	0.92	106	106.0	1.39
107	107.0	0.47	107	107.0	0.93	107	107.0	1.40
108	108.0	0.47	108	108.6	0.94	108	108.0	1.41
109	109.0	0.48	109	109.0	0.95	109	109.0	1.43
110	110.0	0.48	110	110.0	0.96	110	110.0	1.44
111	1110	0.48	111	0,111	0.97	111	111.0	1.45
112	1127	0.49	112	112.0	0.98	112	112.0	1.47
114	113.0	0.49	113	113.0	0.99	113	113.0	1.48 1.49
115	114.0	0.50	115	114.0	0.99	114	114.0	1151
			116					
1116	116.0	0.51	117	116.0	1.01	116	116.0	1.52
1118	117.0	0.51	118	118.0	1.03	118	118.0	1.53 1.54
110	119.0	0.52	119	119.0	1,04	119	119.0	1.56
120	1200	0.52	120	120.0	1.05	120	120.0	1.57
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57 58 57.99 1.01 57.99 1.27 57.98 1.52 57.97 1.77 58.99 1.03 58.99 1.29 58.98 1.54 58.97 1.80 59.99 1.05 59.99 1.31 59.98 1.57 59.97 1.83 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat.					, ,	56.98	_		
59 58.99 1.03 58.99 1.29 58.98 1.54 58.97 1.80 59.99 1.05 59.99 1.31 59.98 1.57 59.97 1.83 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat.		57.99	• -	57.99	1.27	57.98	1.52	57-97	1.77
Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat.	59	58.99 1.03		58.99		58.98		_	
G G' 45' 30' :5'	60	Market - Control of the last o			-	أحكونه نناونسانات			
GO Thomaso	ist								
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\$8 Degrees.

ਦੂ"।	0/		15	/	30		45	<u> </u>
3	Lat	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
61	60.99	1.96	60.99	1.33	60.98	1.60	60.97	1.86
62	61.99	1.08	61.99	1.35	61.98	162	61.97	1.89
63 64	62.99 63.99	1.10	62.98 63.98	1.40	62 9 8 63.98	1.65 1.68	62.97 63.97	1.92 1.95
65	64-99	1.13	64.98	1.42	64 98	1.70	64.97	1.99
66	65.99	1.15	65.98	1.44	65.98	1.73	65.97	2.02
67	66.99	1.17	66.98	1.46	66.98	1.75	66-97	2.05
68 69	67.99 68. 9 9	1.19	67.98 68.98	1.48 1.51	67.98 68.98	1.78	67.97 68.97	2.08
70	69.99	1.22	69.98	1.53	69.98	1.83	69.97	2.14
71	70.99	1.24	70.98	1.55	70.98	1.86	70.97	2.17
72	71.99	1.26	71.98	1.57	71.98	1.88	71.97	2 20
73	73.99	1.27	72.98 73.98	1.59 1.61	72.98	1.91 1.94	72.97 73.97	2.23 2.26
74 75	73-99 74-99	7.31	74.98	1.64	73·97 74-97	1 96	74-97	2.29
76	75-99	1.33	75.98	1.66	75-97	1.99	75.96	2.32
77	76.99	1.34	76.98	1.68	76.97	2.02	76-96	2-35
78	77.99	1.36	77.98	1.70	77.97	2.04	77.96	2.38
79	78.99 79.99	1.38	78.98 79.98	1.75	78.97 7 9-9 7	2.07 2.09	78.9 6 79. 9 6	2.41 2.44
81	80.99	1.41	80.98	3.77	80.97	2.12	80.96	2.47
82	81,99	J.43	81.98	1.79	81.67.	2.15	81.96	2.50
83	82.99	E.45	82.98	18.1	82.97	2.17	82.96	2.53
84 85	83.99	3.47	83.98 84.98	1.83	83.97 84.97	2.20	83.96 84.9 6	2.57 2.60
86	84-99	1.48	85.98	1.88		2.25	83.96	2.63
87	85.99 86.99	1.50	86.98	3.90	85.97 86.97	2.28	86.96	2.66
88	87.99	1.54	87.98	1.92	87.97	2.30	87.96	2.69
89	88-99	1.55	88.98	1.94	88.97	2.33	88.96	2.72
90	89.99	1.57	89 98	1.96	89.97	2.36	89.96	2.75
91 92	97,99	1.59 1.61	90.98	1.99 2.01	90.97 91.97	2.38 2.41	90.96 91.96	2.78 2.81
93	92.99	1.62	92.98	2.03	92.97	2.43	92.96	2.84
94	93.99	1.64	93.98	2.05	93-97	2.46	93.96	2.87
95	94.99	1.66	94.98	2.07	94-97	2.49	94.96	2.90
96	95-99	1.68	95. 9 8 96.98	2.09	95·97 96.97	2.51	95.96	2.93 2.96
97 98	96 99 97-99	1.71	97.98	2.14	97.97	2.54 2.57	96.95	2.99
99	98.98	1.73	98.98	2.16	98.97	2.59	98.95	3.02
100	99-98	1.75	99.98	2.18	99-97	2.62	99.95	3.05
101	1010	1.76	101.0	2.20	101.0	2.64	101.0	3.58
103	103.0	1.78	102.0	2.23 2.25	103.0	2.67 2.70	103.0	3.12
104	104.0	1.82	104.0	2.27	104.0	2.72	104.0	3.18
105	105.0	1.83	1050	2.29	105.0	2.75	105.0	3.21
106	106.0	1.85	106.0	2.31	106.0	2.77	106.0	3.24
107	107.0	1.87	107.0	2.33	107.0	2.80 2.83	107.0 108.0	3.27 3.30
109	109.0	1.90	109.0	2.38	109.0	2.85	1090	3.33
110	110.0	1.92	110.0	2.40	1100	2.88	110.0	3.36
111	111.0	1.94	111.0	2.42	111.0	2.91	111.0	3.39
112	1120	1.95	112.0	2.44	1120	2.93	112.0	3.42
114	113.0	1.97	113.0	2.49	113.0	2.96 2.98	113.0	3-45 3.48
115	115.0	2.01	115.0	2.51	115,0	3.01	115.0	3.51
116	116.0	2.02	116.0	2.53	116.0	3.04	116.0	3.54
117	1170	2.04	117.0	2.55	117.0	3.06	117.0	3.57
119	119.0	2.06	118.0	2.57	118.0	3.09	118,0	3.60 3.63
120	120,0	2.09	120.0	2.62	120.0	3.14	120.0	3.66
7.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
i	Dep. Lat. Dep. Lat.					7	15	<u> </u>
7	-	7/11/20	92	DEGR			-	البادية في المسجوع

1 5	1 0/		15	1	30		45	*
1 7	Lat.	Dep.	Lat.	Dep.	Late	Der	Lat.	Dep
	1,00	0.03	1.00	0.04	1.00	0.04	1.00	0.0,
2	\$.00	0.07	2.00	9.08	2,00	0.09	2.00	0.10
3	3.00	0.10	3.00	0.12	3.00	0.63	3.00 4.00	0.14 0.19
4 5	4.00 5,00	014	4.00	0.16	3-99 5.00	0.23	4.99	0.24
6	~ {	0.21	6.00	0.24	5.99	0.26	5.99	0.24
7	7.00	0.24	6.99	0.27	6.99	0.31	6.99	0.34
8	8.00	0.28	7.99	0.31	7.99	0.35	7.49	0.38
9		0.31	8-99	0.35	8-99	0.39	8.99 9-99	0.48
10		0 35	4-99	0.39	9.99	0.44	10.99	0.53
1 1 2	1	0.38	10.99	0.43	10.99	0.48	11.99	0.58
1.13		0.45	12.99	0.51	12.99	0.57	12.99	0.62
14		0.49	11.99	0 55	13.99	0.61	13.48	0.67
15	14.99	052	14.99	0.59	14.99	0.65	14.98	0.72
16		0.56	15.99	0.63	15.98 16 98	0.70	15.98 16.98	0.77
17		0.59	16 99	0.07	17.98	0.74	17.98	0.86
119		0.66	18 99	0.75	18.98	0.83	18.98	0.91
20		0.70	19 98	0.79	19.98	0.87	19.98	0.96
21	, , ,	0.73	20.98	0.82	20.98	092	20.98	1.01
21		0.77	21.98	0.86	21.98	0.96	21.97	1.06
23 24		0.80	22.98 23.98	0.90	22.98 23.98	1.05	22.97 23.97	1.10
25	1 - A	0.87	34 98	0.98	24 98	1.09	24.97	1.20
26		0.91	25.98	1.02	25.98	1.13	25.97	1,25
27	26.98	0.94	26.98	1.06	26.97	118	26 .97	1.30
28	-0 0	0.98	27.98 28.98	1.10	27:97 28.97	1.22	27.97 28.97	I.34
29 3d		1.05	29.98	1.18	29.97	1.3 Í	39.97	1.39 1.44
31	_]	1.08	30.98	1.22	30.97	1.35	30.96	1.49
32	1	1.12	31.98	1 26	31.97	1.40	31 96	£ 54
33	32.98	1.15	32.97	1.30	32.97	1.44	32-96	1.58
34		1.19	33.97	1.33	33 97	1.48	33.96 34.96	1.63 1.68
35	-	1.22	34-97		34·97 35·97	1.53	35.96	
36 37	1 -/ ^	1.26	35.97 36.97	1.41	36.96	1.65	35.96	1.73
38		1.33	37.97	1.49	37.96	1.66	37.96	1,82
39		1 36	38.97	1.53	38.96	1.70	38.96	1.87
40	- (1.40	39.97	1.57	39.96	1.74	39-95	1.92
41		1 43	40.97 41.97	1.61	43.96 41.96	1.79	40.95	1 97 2 02
42		1.47	42.97	1.69	42.96	1.88	42.95	206
44		1.54	43-97	1.73	43.96	1.92	43.95	2.11
45	44.97	1 57	44.97	1.77	44.96	1 96	44.95	2.16
46	1 .	1.61	45.96	1.81	45.96	201	45.95	2,21
47		1.64	46 96 47.96	1.85	46.96 47.95	2.05 2.0g	46.95 47 . 94	2,26 2,30
49	(· · · · · · · · · · · · · · · · · · ·	1.71	48.96	1.92	48.95	2.14	48.94	2.3
50		1.75	49.96	1.96	49.95	2.18	49-94	24
51	50.97	1.78	50.96	2.00	50.95	2.22	50.94	2.45
52		1.81	51.96	2.04	51.95	2.27	51.94	2.49
53 54		1.85	52.96 53.96	2.08	52 95 53 95	2.31 2.36	53.94 53.94	2-54 2-59
55		1 92	54.96	2.16	54.95	2.40	54-94	2.64
5		1.95	55.96	2.20	55.95	2.44	55.94	2.64
7	56.97	1.99	56.96	2.24	56.95	2.49	56.93	2.73
58	57 96	2.02	57.96	2.28	57 94	2.53	57.93	2.75 2 83
60	58.96 54.96	2.06 2.09	58.96 59.96	2.32 3.36	58-94 59 94	2.57 2.62	58.93 59.93	2 88
1	Dep	Li.	Dep	Lat.	Dep.	Lat.	Dely.	Lat
7		/ .	4.5		30		13	
			***	07 3334		,	4.0	

D	0'		15	157		1	4,5	7
st.	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
61	60.96	2.13	60.95	2.39	60.94	2.66	60 93	2.93
62	61.96	2 16	61.95	2.43	61.94	2.70	61.93	2.97
63 64	62.96 63.96	2.20 2.23	62.95 63.95	2.47	62.94 63.94	2.75	62.93 63 93	3.02 3.07
65	64.96	2.27	64.95	2.55	64.94	2.84	64.93	3 12
66	65.96	2.30	65.95	2.59	U5.94	2.88	65.92	3.17
67	66.96	2.34	66.95	2.63	66 94	2.92	66.92	3.21
68	67. 9 6	2.37	67-95 68.95	2.67	67.94	2.97	67.92	3.26
· 69 70	68.96 69.96	2.41 2.44	69.95	2.71 2.75	68.93 69.93	3.05	68.92 69.92	3.31 3.36
71	70.96	2.48	70.95	2.79	70.93	3.10	70.92	3 41
72	71.96	2.51	71.94	2.83	71.93	3 14	71.92	3.45
73	72.96	2.55	72.94	2.87	72.93	3.18	72 92	3.50
74	73.95	2.58 2.62	73·94 74·94	2.91 2.94	73 93 74:93	3.23 3.27	73.91 74 91	3.55 3.60
75	74-95	2.65	-	2.98	75.93	3.32	75.91	3.65
76 77	75.95 76.95	2.69	75 .94 76.94	3.02	76.93	3.36	76.91	3.69
78	77.95	2.72	77.94	3.06	77.93	3.40	77.91	3.74
79	78.95	2.76	78.94	3.10	78.92	3.45	78 91	3.79
80	79.95	279	79.94	3.14	79.92	3.49	79.91	3.84
8 t 8 2	80.95	2.83 2.86	80.94 81.94	3.18 3.22	80.92 81.92	3·53 3·58	80.91 81.91	3.89 3.93
83	82.95	2.90	82.94	3.26	82.92	3.62	82.90	3.98
84	83.95	2.93	83.94	3.30	83.92	3.66	83 90	403
85	84-95	2.97	84-93	3.34	84.92	3.71	84.90	4.08
86 87	85.95	3.00	85.93	3.38	85.92 86.92	3.75	85.90 86.90	4-13
88	86.95 87.95	3.04 3.07	86.93 87.93	3.42	87.92	3.79 3.84	87.90	4.17
89	88.95	3.11	88.93	3.49	88.92	3.88	88.90	4-27
90	89.95	3.14	89.93	3-53	89.91	3.93	89.90	4.32
91	90.94	3.18	90.93	3.57	90.91	3.97	90.90	4.37
92	91.94 92.94	3.21 3.25	91.93	3.61	91.91	4.01 4.06	91.89 92.89	4.46
93 94	93.94	3.28	93.93	3.69	93.91	4.10	93.89	4.51
95	94 94	3.32	94.93	3 73	94.91	4-14	94.89	4.56
96			95-93	3.77	95.91	4.19	95.89	4.61
97			96.93	3.85	96.91 97.91	4.23	96.89 97.89	4.65
98 99			97 92 98.92	3.89	98.91	4 32	98.89	4.75
100			99.92	3.93	99 90	4-36	99.88	4.80
101	100.9	3.53	100.9	3.96	100.9	4.41	100.9	4.85
102	101.9	3.56	101.9	4.00	101.9	4 45	101.9	4.89
103 104	103.9	3.59 3.63	102.9	4.04 4.08	102.9	4-49 4-54	102.9	4-94 4-99
105	104 9	3.66	104.9	412	104.9	4.58	104.9	5.04
106	105 9	3.70	105.9	4.16	105.9	4.62	105.9	5.09
107	106.9	3.73	106.9	4 20	106.9	4.67	106.9	5.13
801	107.9	3.77	107.9	4.2 4 4.28	107.9 108.9	4.71 4.75	107.9 108.9	5.18 5.23
109	108.9	3.80 3.84	109.9	4.32	109.9	4.80	109.9	5.28
111	110.9	3.87	110.0	4.36	110.9	4 84	110.9	5.33
112	111.9	3.91	111.9	4.40	111.9	4.89	111.9	5.37
E13	112.9	3.94	112.9	4.44	112.9	4.93	112.9	5.42
114	113.9	3.98	113.9	4.48 4.51	113.9	4.97 5.02	113.9	5.47 5.52
116		4.01	115.9		115.9	5.06	115.9	5.57
117	115.9	4.08	116.9	4·55 4·59	116.9	5.10	116.9	5.61
118	117.9	4.12	117.9	4.63	117.9	5 15	117.9	5.66
1119	118.9	4.15	118.9	4.67	118.9	5.19	118.9	5.71
120	119.9	4.19	119.9	4.71	119.9	5.23	1199 Deji.	5.76 L.L
ist.	Dep Lat. Dep Lat. D p 2 0' 45'					Lat.	15/	
19								
	87 DEGREES.							

1 0	0		. 15	/	30)'	4	7
Dist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
 			1.00	0.06	1.00	0.06	1.00	0.07
1 1	1.00	0.05	2.00	0.11	2.00	0-12	2.60	0.13
3	2.00 3.00	0.16	3.00	0.17	2.99	0-18	2.99	0.20
4	3.99	0.21	4.00	0.23	3.99	0-24	3.99	0,25
5	4.99	0.26	4.99	0.28	4-99	0,31	4-99	0.3
6	5.99	0.31	5.99	0.34	5.99	0.37	5.99	0.39
7	6.99	0.37	6.99	0.40	6.99	0.48	6 99	0.45
8	7.99	0.42	7.99	0.45	7.99	0 49.	7.98	0.52
9	8.99	0.47	8.99	0.51	8.98	0.55	8.98	0.59
10	9.99	0.52	9.98	0.57	9.98	0.61	9.98	0.65
11	10.98	0 58	10.98	0.62	10.98	0.67	10.98	0.72
12	31.98	0.63	11.98	0.68	11.98	0.73	11.97	0.78
13	12 98	0 68	12.98	0.74	12.98	0.79	12.97	0.85
14	13.98	0.73	13.48	0:79	13.97	0.85	13.97	0.92
15	14 -, 8	0.79	14.98	0.85	14-97	0.98	14.97	
16	15.98	0.84	15.97	0.91	15.97	0 98	15.97	1.05
17	16.98	0.89	16.97	0.95	16.97	1.04		1.11
18	17 98	0.94	17.97	1.02	17.97 18.96	1.10	17.96 18.96	1.24
19	18.97	0.99	18.97 19 . 97	1.08	19.96	1.22	19.96	1.31
	19.97				-	1.28	20.96	1.67
21 22	20.97	1.10	20.97 21.97	1.19	20.96 21.96	1.26	21.95	1.44
23	21 97 22 97	1.15 1.20	22.96	1.30	22.96	1.40	22.95	1.50
24	23.97	1.26	23.96	1.36	23.96	1 47	23.95	1 1.57
25	24.97	1.31	24.90	1.42	24 95	1.53	24.95	1.64
26	25.96	1.36	25.96	1.47	25.95	1.59	25.94	1.70
27	26.96	1.41	26.9 6	1.53	26.95	h65	26.94	1.77
28.	27.96	1.47	27.96	1.59,	27.95	1.71	27.94	1.83
29.	28.96	1.52	28.95	1.64	28.95	1.77	28.94.	1.90
30	29.96	1.57	29.95	1.70	29.94	1.83	29.94	1.96
31.	. 39.96	1.62	30.95	1.76	30.94	. 1.89	30.93	2.03
32	31.96	1.67	31.95	2.83	31.94	· 1.95.	31.93	2.09
33	32.95	1.73	32.95	1.87	32.94	2.01	32.93	. 2.16
34	33.95	3.78	33-95	1.93	33-94	2 08	33.93	2.22
. 35	34-95	1.83	34-94	1.98	34-93	2.14	34.93	2.29
36	35.95	. 1788	35.94	2.04	35.93	2.20	35.92	2.35
37	36.95	1.94	36.54	2.10	36.93	2.26	36.92	2.42
. 38	37.95	· I.99	37.94	2.15	37.93	2.32	37.92	2.49
39	38.95	2.04	38.94	2.28	38.93	2:38	38.92	2.62
40	39.95	2.09	39.94		39.93	2.44	39.91	
41	40.94	2.15	40.93	2.32	40.92	2.50	40.91	2.68
42	41.94	2.20	41.93	2.38 2.44	41.92	2.56 2.63	41.91.	2.75 2.84
43	42.94	2:25	42.93 43.93	2.49	42.92	2.69	43.91	2.88
44	43.94 44.94	· 2.30 2:36	44.93	2.55	43.92 44.92	2.75	44.90	2.94
ا سبب سبنه کا			-	2.61		2.81	45.90	3.01
46	45.94 46.94	2.41 2.46	45.93 46.92	2.66	45.91 46.91	2.87	46.90	3.01
48	47.93	2.40	47.92	2.72	47.97	2.93	47.90	3.14
49	48.93	2.56	48.92	2.78	48.91	2.99	48.90	3.20
50	49.93	2.62	49.92	2:83	49.91	3.05	49.89	3.27
51	50.93	2.67	50.92	2.80	50.90	3.11	50.89	3.34
52	21.93	2.72	51.92	2.95	51.90	3.17	51.89	3.40
53	52.93	2.77	52.91	3.00	52.90	3.24	52.89	3-47
54	53.93	2.83	53.91	3.06	53.90	3.30	53.88	3.53
55	54.92	2.88	54 91	3.12	54.90	3.36	54-88	3.60
56	55.92	2.93	55.91	3.17	55.90.	3.42	55.88	3.66
57	56.92	2.98	56.91	3.23	5 6 .89	2:48	56.88	3.73
58	57.92	3.04	57.91	3.29	.57 89	3-54	57.88	3.79
59	58.92	3.09	58.91	3.34	58.89	3.60	58.87	3.86
60	59.92	3.14			59.89	2.66	59.87	3.92
آنيه لا	Dep. Lat. Dep. Lat.				Dep	Lat.	Dep.	Lat.
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106 105.6 9.24 105.6 9.70 105.5 10.16 105.5 10.26 106.5 10.26 106.5 10.72 10.26 106.5 10.72 10.26 106.5 10.72 10.26 106.5 10.72 10.35 107.5 10.82 107.5 10.35 107.5 10.82 107.5 10.82 107.5 10.35 107.5 10.82 107.5 10.82 107.5 10.83 107.5 10.82 10.93 108.5 10.93 11.63 10.94 11.03 111 110.6 9.59 109.5 10.07 109.5 10.64 110.4 11.13 112 110.6 9.59 109.5 10.25 111.5 10.64 110.4 11.13 113 112.6 9.56 112.5 10.25 111.5 10.64 110.4 11.33 114 112.6 9.85 112.5 10.43 112.5 10.83 112.4 11.42 113 114.6	_								
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113			9.67	110.5					
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113 314.6 10.09 114.5 10.52 114.5 11.02 114.4 11.52 116 115.6 10.11 115.5 10.61 115.5 11.12 116.4 11.62 117.6 10.28 117.5 10.80 117.5 11.31 116.4 11.72 118.5 10.37 118.5 10.28 118.5 11.40 118.4 11.92 120 119.5 10.46 119.5 10.98 119.5 11.50 119.4 12.02 119.5 10.98 119.5 11.50 119.4 12.02 119.5 11.50 119.5 119.5 119.5 119.5 119.5 119.5 119.5 119.5 119.5 119.5 119.5 119.5 119.5 119.5 119.5 119.5 119.5 11	_								
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Sig Fi8.5 10.37 218.5 20.89 118.5 11.40 118.4 11.92 12.02			_ 1						
119.5 10.46 119.5 10.98 119.5 11.50 119.4 12.02	•								
G 45' 30' 15'		119.5	10.46	119.5	10.98			119.4	
	1 4							Dep.	Lat.
	<u> </u>	,				_	•	15'	

Dist	0		1	51	30)'	45	
2	Lat.	D-p	L.t.	Dep.	Lat.	Dep	Lat.	Dep
1	0.99	0.10	0.99	0.11	0.99	0.11	0 99	0.12
2	1.99	0.21	1.99	G.22	1.99	0.23	1.99	C.24
3	2 98	0.31	2.98	0 33	2 98	0.34	2.98	0.35
4 5	3.98 4-97	0.42	3.98 4.97	0.44	3.97	0.45	3.97 4.97	0.47
6	5 97	0.63	5 96	0.65	4-97	0.68	5.96	071
•	6.96	0.73	6.96	0.76	5 96 6.96	0.79	6 95	0.82
7 8	7.96	0.84	7.95	0.87	7.95	0.91	7.94	0.94
9	8.95	0.94	8.95	0 98	8 94	1.02	8.94	1.06
10	9.95	105	9.44	1.09	9.94	1.13	9.93	1 18
111	10.94	1.15	10.93	1.20	10.93	1.25	10.92	1.29
12	11 93	1 36	11.93	1.42	11.92	1.36	11.92	1.53
14	1392	1.46	13.92	1.52	13.91	1.58	13.90	1.65
15	14.92	1.57	1491	1.63	14.90	1.70	14.90	1.76
16	15.91	1.67	15.90	1.74	15.90	1.81	15.89	4.88
17	16.91	1.78	16.90	1.85	16.89	1.92	16.88	2.00
18	17.90	1.88	17.89	1.96	17.88	2.15	17.88	2.12
19 20	19.89	2.09	19.88	2.18	19.87	2.26	19.86	2.35
21	20.89	2.20	20.88	2.29	20.86	2.38	20.85	2.47
22	21.88	2.30	21 87	2.40	21.86	2.49	21.85	2.59
23	22.87	2 40	22.86	2.50	22 85	2.60	12.84	2.70
24	23 87 24.86	2.51	23 86	2.61	23.85	2.72	23.83	2.82 2.94
25 26		2.72	24 85	2.83	24.84		24.83	3.06
27	25.86 26.85	2.82	25.85 26.84	2.94	25.83 26.83	3.06	25.82	3.17
28	27 85	2.93	27.83	3.05	27.82	3.17	27.81	3.29
29	28 84	3.03	28.83	3.16	28 81	3.28	28.80	3.41
30	29 84	3.14	29.82	3.27	29.81	3.40	19.79	3-53
31	30.83	3.24	30.82 31.81	3.37	30.80	3.51	30 79	3.64 3 76
32 33	31.82 32.82	3·34 3·45	32.80	3.48	31.79	3.74	31.78	3.88
34	3381	3.55	33.80	3.70	33.78	385	\$3.76	4.00
35	34.81	3.66	34-79	3 81	34 7 ⁸	3.96	34-76	4.11
36	35.80	3 76	35.79	3.92	\$5.77	4 08	35.75	4.23
37	36.80	3.87 3.97	36.78	4.03	36.76	4.19	36.74	4-35
38 39	37·79 38.79	4.08	37·77 38.77	4.14	37.76	4 30 4.41	37·74 38.73	4-47 4-58
40	39.78	4.18	39.76	4-35	39.74	4.53	39.72	4.70
41	40 78	4.29	40.76	4.46	40.74	4 64	40 72	482
42	41.77	4.39	41.75	4-57	41.73	4.75	41.71	4-94
43	42.76	4.49	42 74	4.68	42.72	4 87	42.70	5.05
44	43.76	4.60 4.70	43-74 44 73	4 79 4.90	43.72	4.98 5.09	43 70 44.69	5.17 5.29
46	45.75	4.81	45.73	5.01	45.70	5.21	45 68	5.41
47	46.74	491	46.72	5.12	45.70	5.32	46.67	5.52
48	47-74	5.02	47.7 I	5.23	47 69	5.43	47.67	5 64
49	48.73	5.12	48.71	5.33	48.69	5.55	48.66	5.76
50	49.73	5.23	49.70	5.44	49 68	5.66	49.65	5.88
51 52	50.73 51.72	5-33 5-44	50.70 51 69	5.55 5.66	50.67 51.67	5.77 5.89	50 65 51.64	5.99
53	52.71	5.54	52 69	5.77	52.66	6.00	52.63	6.23
54	53.70	5.64	53.68	5.88	53.65	6.11	53.63	6.35
55	54.70	5.75	54.67	5.99	54.65	6.23	54.62	6.46
56	55.69	5.85	55.67	6.10 6.21	55 64	6.34	55.61	6.58 6.70
57 58	56.69 57.68	5.96 6.06	56.66 57.66	6.31	56.63 57.63	6.45	56.60 57.60	6.82
59	58.68	6.17	58.65	6.42	58.62	6.68	58.59	6.93
60	59.67	6.27	59.64	6.53	59.61	6.79	59.58	7.05
ist.	Dep. Lat. Dep. Lat.			Dep.	Lat.	Dep.	Lat.	
A	0' 451				3(<i>jl</i>	15	'
	83 DF				CPRES			

6	DEGREES.	

ł	Dist	U	İ	15' 1		30' 1			4 /			
-	<u>.</u>	last	D-p	Lac	De	Lat.	D. p.	Lat.	1)			
	61	60.67	6.38	60.64	6.64	60.61	6.91	60.58	7.17			
	Ú2	61 66	6.48	61.63	6.75 6.86	61 60	7.02	61 57	7.29			
	63 64	62 65 63.65	6.59 6.69	62.63 63.62	6.97	62.60	7.13	63.56	7.40 7.52			
1	65	64.64	6.79	64.61	7 08	64.58	7 36	64.55	7.64			
1	66	65 64	6 90	65.61	7.19	65.58	7.47	65.54	7.76			
1	61	66.63 67.63	7.00	66.60 67.60	7.29	66.57 67.56	7.58 7-70	66 54 67.53	7.8 8 7.99			
1	68 69	68.62	7.11 7.21	68.59	7.40 7.51	68.56	7.81	68.52	8.11			
4	70	69.62	7.32	69.58	7.62	69 55	7.92	69.51	8.23			
1	71	70.61	7 42	70 58	7-73	70.54	8.04	70.51	8.35			
*	72	71.61 72.60	7·53 7.63	71.57 72.57	7 84 7.95	71.54 72.53	8.15 8.26	71.50	8.46 8.58			
4	73 -74	73.59	7.74	73.56	8.0 6	73.52	8.38	73.49	8.70			
	75	74-59	7.84	74.55	8.17	74.52	8 49	74.48	8.8:			
1	76.	75.58	7.94	75.55	8.27	75.51	8 60	75.47	8.93			
	77 78	76.58 7 7-5 7	8.05·	76.54 77.54	8.38 8.49	76.51 77.50	8.72 8.83	76.47 77.46	9.05 9.17			
*	79	78.57	8 26	78.53	8.60	78.49	8.94	78.45	9.29			
1	80	79.56	8.36	79 52	8.71	79 49	9.06	79.45	9 40			
1	81	80.56	8.47	80.52	8.82	80 48	9.17	80.44	9.52			
	82 83	81.55 82.55	8.57 8.68	81.51 82.51	9.04	81.47 82.47	9.28 9.40	81.43 82.42	9.64 9.76			
4	84	83.54	8.78	83.50	9 14	83 46	9.51	83.42	9.87			
4	85	84.53	8.88	84.49	9 25	84.45	9 62	84.41	9.99			
1	86	85.53	8.99	85.49	9.36	85.45	9.74	85.40	10 11			
	87 88	86.52 87.52	9.09 . 9.20	86 48 87.48	9.47 9.58	86.44 87 43	9.85 9.96	86.40 87.39	10.23			
	89	88.51	9.30	88.47	9.69	88.43	80.01	88.38	10.46			
4	90	89.51	9.41	89.47	9.80	89.42	10.19	89 38	10.58			
-	91	90.50	9.51	90.46	9.91	90.42	10.30	90 37	10.70			
	92	91.50	9.62 9.72	91.45 92.45	10.02	91.41 92.40	10.41	91.36	10.93			
]	93 94	93.49	9.83	93.44	10.23	93 40	10.64	93.35	11.05			
	95	94.48	9.93	94-44	10 34	94-39	10.75	94.34_	11 17			
-	96	95.47	10.03	95.43	10 45	95.38	10.87	95.33	11.28			
-	97 98	96.47 97.46	10.14	96.42 97.42	10.56	96 38 97-37	10.98	96.33 97.32	11.40			
1	99	98.46	10 35	98.41	10.78	98.36	11.21	98.31	11.64			
-	100	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75			
	101	100.4	10.56	100.4	11.00	100.3	11.43	100.3	11.87			
1	102	101.4	10.66	101.4	11.21	101 3	11.66	102.3	12.11			
1	104	103 4	10.87	103.4	11.32	103.3	11.77	103.3	12.22			
	105	104.4	10.98	104.4	11.43	104.3	11.89	104.3	12.34			
į	106	105.4	81.11	105 4	11.54	105.3	12.00	105.3	12.46			
	107	106 4	11.29	107.4	11.76	107 3	12.23.	107.3	12.69			
	109	108.4	11.39	1084	11.87	108.3	12.34	108.2	12.81			
	110		11 50	109.3	11.98	109 3	12.45	109 2	12.93			
	111	1104	11.60	110.3 h	12.08	110.3	12.68	110 2	13.05 13.16			
•	113	112.4	11.81	112.3	12.30	112.3	12.79	112.2	13.28			
	114	113.4	11.92	113.3	1241	113.3	12.41	113.2	13.40			
	115	1144	12.02	114.3	12.52	1143	13.02	114.2	13.52			
1	116	115.4	12.13	116.3	1263	115.3	13.13	115.2	13.63			
1	118	117.4	12.33	117.3	12.85	117.2	13.36	117.2	13.87			
1	119	118.3	12.44	118.3	12.96	118.2	13.47	118.2	13.79			
•	120	1193	12.54	119.3	13 06	119.2	13.58	119.2	14.10 L.d.			
-	Dist	1) p	Lat	Dep '								
ł												
	-	83 DEGREES.										

F	0/		1 /		30/		45'	
3	Lat	Dep	Lat.	Dep.	Lat	Dep.	Lat	Dep.
	0.99	0.12	0.99	C. 13	0.99	0.13	0.99	0.13
1 :	1.99	0.24	1.98	0.25	1.98	0.16	1.98	0.17
1 3	3.98	0.37	3.97	9.38	3 97	0.52	2 97 3 96	0.54
5	4.96	0.61	4.96	0.63	4.96	0.65	4-95	0.67
6	5.96	0 73	5 95	0.76	5.95	0.78	5.95	0.81
1 7	7 94	0.85	7-94	0.88 1.0L	6.94 7.93	1.04	7-93	1.08
1 5	8.93	1 10	8.93	2.14	8 92	1.17	8.91	1.21
10	9 93	1.32	9 93	1.26	9.91	1.31	9.91	1.35
1 !!	10 93	1.14	10.91	1 39	10.91	1.44	10.00	1.48
13	11.91	1.46 1.58	11.90	1.57	11.90	1.57	11.89	1.61
14	13.90	1.71	13.89	1.77	13.88	1.83	13.87	1.89
15	14.89	1 83	74.88	1.89	14.87	1.96	14.86	2.01
16	15.88 16.87	1.95	16.87	2.02	15.86	2.09	15.85	3-16 3-29
17	17.87	1.19	17.86	3.27	17 85	235	17.84	1.43
19	12.86	2.32	18.85	8.40	18.84	1.48	18 83	2-56
\$0	19.85	3.44	19.84	2.52	19.83	2.61	19.82	3.70
31,	30.84 21.84	2.55	20.83	2 65 2.78	20.82	2.74	20.8;	2.83
1 55	22.83	2.50	11.81	2.90	22,80	3.00	22.79	3.10
14	23 82	3.92	23.81	3.03	23.79	3.13	23.78	3.34
35	24 51	3.05	24.80	3.16	24.79	3.26	24 77	3-37
26 37	26.80	3.17	25.79	3.41	25.78	3 39 3 52	25.76	3.51 3.64
28	27.79	3-41	27.78	3-53	27.76	3.65	17-74	3 78
29	28.78	3.53	28.77	3.66	28 75	3-79	28.74	3-91
30	29.78	3 66	39.76	3.79	29.74	3 92	29.73	4-05
31	30.77 31.76	3.78	30.75	391	30 73 31.73	4.05	30.72	4.18
33	32.75	4-03	34.74	4.16	32.72	4-31	32.70	4-45
34	33-75	4-14	33.73	4-29 4-42	33.71	4 44	33.69 34.68	4.58
35	35.73	4-39	35-71	4 54	34.70	4-57	35.67	4.85
37	30.73	4.51	36 70	4.67	36.68	4.83	36.66	4-99
38	37-74	4-63	37-70	4.60	37.67	4.98	37.65	5.12
39 40	38.71 39.70	4-75 4-87	39.68	4 9 2 5 0 5	38.67 39.66	5.09	38.64 39.63	5.36 5.39
41	40.69	5 00	40.67	5.17	40.65	5-35	40.61	5-53
42	41.69	5.12	41-66	5.30	41 64	5.48	41.62	5.66
150	42.68 43 67	5-24	42.66	5-43	42 63	5.61	42.61	5.B0
44 45	44 66	5.48	43.65 44.64	5.55 5.68	43.62 44.62	5-74 5-87	43.60 44-59	§ 93 6.07
46	45.66	5 61	45.63	5.81	45 61	6 20	45.58	6.20
47	46 65	5-73	46 62	5.93	46.60	6.13	46.97	6.34
4 ⁸ 49	47.64 48.63	5 8g	47.62 48.61	6.06	47.59 48.58	6.27 6.40	47-56 48-55	6.47 6.6t
50	49.63	6.09	49.60	6.31	49-57	6.53	49-54	6 74
51	50.62	6.22	50.59	6.44	50.56	8.50	50.53	6.88
52	51.6t 52.60	6.34	\$1.58	6.56	51.56	6.79	51.53	7.01
53 54	53.60	6.46 6.58	52.58 53.57	6.69	52-55 53-54	6.93 7.05	52.52 53.51	7-15 7-28
33	54-59	6.70	54.56	6.94	54-53	7.18	54.50	7 43
56	55.58	6.81	55-55	7.07	59.52	7-31	55-49	7-55
57	56.58	6.95	\$6.54	7.19	56.51	7-44	55.48	7.69
58 59	57.57 58.56	7.07	57-54 58.53	7 32 7-45	57.50	7-57	57-47 58.46	7.8a 7.96
60	59-55	7.31	59.52	7.57	59-49	7.83	59-45	8.00
Dart	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	Dep.	Lat.
i a	6'		45'		30/		15'	

& DEGREEA.

Dist	- 0	1	11.5	5/	• 3	0'	4.5	
£ .	Lat.	Dep.	Lat.	Dep.	Lat	D n	lat	Dep.
61	60 55	7-43	60.51	7-70	60.48	7.96	60.44	8.23
61	61.54	7.56	61.50	7.82	61.47	8.0g	61.43	1.36
63	61.53	7.68	62.50	7-95	61.46 61.45	8.22	6141	8.50 8.63
64	63.52 64.52	7.92	64.48	8.20	64 44	8.45	64.41	8.77
66	65.51	\$.04	65.47	\$.33	65.44	8.61	65.40	8.90
67	66.50	8.17	66.46	8.46	66.43	\$75	66.39	9.04
68	67 49	8.39	67.46	8 58	67.43	8.88	67.38	9.17
6g 70	68.49 69.48	8.44 8.53	68.45 69.44	8.71 8.83	68.41 69.40	9.01	68,37 69.36	9.30 9.44
71		3.65	70.43	8.96	70.39	9-27	79.35	9-57
73	70.47 71.46	\$.77	7-43	9.09	71.38	9.40	71.34	9.71
71	72.46	8.90	71-44	9.21	72.38	9-53	72-33	9.84
74	73-45	9.02	73.41	9-34	73.37	9.66	73.33	9.98
75	74-44	9.14	74-40	9-46	74-36	9.79	7+3+	·——
76 77	75.43	9.16 9.38	75.39 76.38	9.59	75-35 76-34	10.02 6.43	75.31	10.15
78	77.42	9.51	77.38	9.84	77-33	10.18	77-29	10.51
79	78-41	9.63	78.37	9-97	78.32	10.31	78.58	10.65
85	79-40	9-75	79.36	10.10	79-32	10 44	79-17	10.79
31	80.40	9-87	\$0.35	10.33	80.31	10.57	80,16	10.93 11.06
81	\$1.39 \$1.38	9.99	\$1.34 ; \$2,34 ;	10.15	\$1.30 \$2.39	10.70	82.24	11.19
84	83.37	10.24	\$3.33	10.60	83.28	10.96	83.23	11.33
8 ç	84.37	10.36	84.32	10.73	84.27	11.09	84.22	11 46
86	\$5.36	10.48		10.85	85.26	11 23	85.21	11 60
87 88	86 35	10.60	\$6.30 \$7.30	10.98	86.26 87.25	11-49	\$6.21 \$7.20	11.73
89	\$7.34 \$8.34	10.85	18.29	11.23	\$\$ 24	11.63	\$8.19	11.00
90	\$9.33	10.97	\$9.28	11.36	\$9.23	11.75	\$9.18	18.14
91	90.32	[1.09	90.27	E1.48	90.13	11.88	90-17	12.27
93	91.31	11 34		18.61	91.81	13.01	91.16	12 41
93	92.31	11.45	93.15	11.74	92.20 93.20	12.14	92.15	12.54 12.68
94 95	93.30 94.39	11.58	94.14	71.99	94 19	13 40	94-13	12.81
96	95.28	11.70	95.33	12.12	95.18	18.53	95.12	1295
97	96.18	11.52	96.22	13.24	96.17	11.66	96.12	13.08
98	97.27	EF 94	97.22	12.37	97.16	12.79	97.10 98.10	13.32 13.35
100	98.26 94 15	13.49	98.21	13.49	98.15	13.05	99-09	13.49
toi	100.1	11.31	100.1	12.75	200,1	13.18	100.1	13.61
105	101.2	11.43	101.3	12.87	101.1	13.31	101.1	13.75
103	105.5	11.55	103,3	13.00	103-1	13-44	102.1	13.89
104	103 1	13.50	103.4	13.18 13.15	103.1 104.1	13.57	104.0	13.02 14.16
105 106		12.92	105.8	13.38	104.1	13.84		1429
107	105.2	13.04	106.1	13.50	106.1	13.97	106.0	14-43
108	107.1	13.16	107.1	13.63	107.1	14 10	107.0	14.56
109	2.801	13.28	1.801	13.76	100.1	14-35	108.0	1470
210	109.2	13.41	109.1			14-49	_	14 97
713	£.011	13-53 13 65	110.1 111.1	14-01	110-1	14.63	(11.0	15 10
113	173.3	13-77	E14-E	14.16	115.0	14.75	0.811	15-24
114	113.2	13.89	\$13.1	14-39	613.0	14.88	113.0	15-37
115	114.1	14.05	114.1	14.51	114.0	13:01	113.9	15 51
116	116.1	1414	216.1	14-54	#15.0 .	15.14	114.9 0 211	15 64 15 78
116	117.1	1438	117.1	14.89	117.0	15.40	116.9	15,91
119	rill,r	14.50	118.0	15.02	118.0	15.53	\$17.9	16 05
120	119.1	14.62	0.611	1514	119.0	15 60	118.9	16.18
.3	Dep.	Lat.	Dep.	Lit	D.p.	Lat	Dep.	h ak
13	0	#	43	/	30	, , , ,	11.	, ,

Lat Dep. Lat		0	,	15	/	30)1	45	;
2 1.98 0.28 1.93 0.29 1.93 0.30 1.93 0.30 1.93 0.30 1.93 0.30 1.93 0.30 1.93 0.30 1.93 0.30 1.93 0.93 0.93 0.93 0.95 0.50 0.57 0.96 0.57 0.96 0.59 0.59 0.59 0.59 0.91 0.96 0.59 0.93 0.97 0.93 1.00 0.92 1.03 0.92 0.91 0.96 0.93 1.00 0.92 1.03 0.92 0.91 0.96 0.93 1.00 0.92 1.03 0.92 1.06 0.93 1.00 0.92 1.03 0.92 1.06 0.93 1.03 0.99 0.91 1.25 0.90 1.43 0.90 1.33 0.90 1.43 0.90 1.93 0.90 1.43 0.90 1.93 0.90 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93	Dist.			Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
2 1.98 0.28 1.93 0.29 1.93 0.30 1.93 0.30 1.93 0.30 1.93 0.30 1.93 0.30 1.93 0.30 1.93 0.30 1.93 0.93 0.93 0.93 0.95 0.50 0.57 0.96 0.57 0.96 0.59 0.59 0.59 0.59 0.91 0.96 0.59 0.93 0.97 0.93 1.00 0.92 1.03 0.92 0.91 0.96 0.93 1.00 0.92 1.03 0.92 0.91 0.96 0.93 1.00 0.92 1.03 0.92 1.06 0.93 1.00 0.92 1.03 0.92 1.06 0.93 1.03 0.99 0.91 1.25 0.90 1.43 0.90 1.33 0.90 1.43 0.90 1.93 0.90 1.43 0.90 1.93 0.90 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93 0.90 1.93	18	0.99	0.14	0.99	0.14				_
\$\frac{3}{5} \frac{4}{.95} \cdot 0.56 3.96 0.56 4.95 0.77 4.95 0.76 4.95 0.77 4.95 0.77 4.95 0.77 4.95 0.77 4.95 0.77 4.95 0.77 4.95 0.77 6.93 1.06 6.93 1.06 6.93 1.06 6.93 1.06 6.93 1.06 6.93 1.06 6.93 1.06 6.93 1.06	`		j i	~	:	_			- 1
\$ 4.95. 0.70	Y		, , , , , , , , , , , , , , , , , , ,						
3 1-9-9- 0.84 5-94 0.86 5-93 0.89 1-93 0.91 6 5-94 0.84 5-94 0.86 5-93 0.89 1-93 0.91 1.06 8 7-92 1.15 7-91 1.29 8.90 1.33 8.90 1.37 10 9-90 1.39 9-90 1.43 9.89 1.48 9.88 11 10.89 1.53 10.89 1.58 1.08 1.65 10.85 1.62 12 11.88 1.67 11.88 1.72 11.87 1.77 1186 1.83 13 12.87 1.81 12.87 1.88 1.92 2.07 13.84 1.13 2.21 13.83 2.22 11.88 1.72 11.88 1.72 11.88 1.72 11.88 1.72 11.88 1.72 11.88 1.72 11.88 2.27 1.18 1.82 2.21 1.98 2.23 1.78 1.84				Ĭ					
7 6.93									0.41
8	1 1				•		•		
10 9.90 1.39 9.90 1.43 9.89 1.48 9.88 1.52		-		7.42	1.15		.		
11 10.89 1.53 10.89 1.58 10.88 1.63 10.87 1.67 12 11.88 1.67 11.88 1.72 11.87 12.87 12.87 12.87 12.87 12.87 12.87 12.87 12.87 12.87 12.85 1.92 12.85 1.93 13 12.87 1.81 12.87 12.87 12.85 1.92 12.85 1.93 13.86 1.95 13.86 2.01 13.85 1.92 12.83 1.93 15.14.85 2.09 14.84 2.15 14.83 2.22 14.83 2.28 14.83 2.28 16 15.84 2.33 15.83 2.30 15.82 2.37 15.81 2.43 17. 16.83 2.37 16.82 2.44 16.81 2.51 16.80 2.59 18 17.82 2.51 17.81 2.58 17.80 2.66 17.79 2.74 19 18.82 2.64 18.80 2.73 18.79 2.86 17.79 2.74 2.01 19 18.82 2.64 18.80 2.73 18.79 2.81 18.78 2.89 2.01 19.81 2.78 19.79 2.87 19.78 2.96 19.77 3.04 22 21.79 3.06 21.77 3.16 20.77 3.10 20.76 3.19 21 20.80 2.92 20.78 3.01 20.77 3.10 20.76 3.19 21 20.80 2.92 20.78 3.01 20.77 3.10 20.76 3.19 21 20.80 2.92 20.78 3.01 20.77 3.02 2.77 3.55 22.78 3.20 22.76 3.30 22.75 3.40 22.73 3.50 22.76 3.30 22.75 3.40 22.73 3.50 22.76 3.30 22.75 3.40 22.73 3.50 22.76 3.30 22.75 3.40 22.73 3.50 22.76 3.30 22.75 3.40 22.73 3.50 22.76 3.70 2.77 1.00 20.76 3.19 20.77 1.00 20.76 3.19 20.77 3.10 20.76 3.19 20.77 3.10 20.76 3.19 20.77 3.10 20.76 3.19 20.77 3.10 20.76 3.19 20.77 3.10 20.76 3.19 20.77 3.10 20.76 3.19 20.77 3.70 22.77 3.70 2	_								•
12 11.88 1.67 11.88 1.72 11.87 1.77 11.86 1.82 13.81 12.87 1.87 12.86 1.92 12.85 1.98 1.98 1.98 1.98 1.98 1.98 1.98 1.98	10				-			-	
13 12 87 1.81 12.87 1.87 12.86 1.92 12.85 1.98 14.91 13.86 1.95 13.86 2.01 13.85 2.07 13.84 2.13 15 14.85 2.09 14.84 2.15 14.84 2.22 14.83 2.28 16.83 2.37 16.82 2.44 16.81 2.51 16.80 2.59 18 17.82 2.51 17.81 2.58 17.80 2.66 17.79 2.74 19 28.82 2.64 18 80 2.73 18.79 2.81 18.78 2.89 20 19.81 2.78 19.79 2.87 19.78 2.66 17.79 3.04 22 21.79 3.06 21.77 3.16 21.76 3.25 21.74 3.35 22 24.79 3.06 21.77 3.16 21.76 3.25 21.74 3.35 22 24.79 3.04 22.75 3.44 23.74 3.55 21.74 3.35 22.52 24.76 3.48 24.74 3.59 24.73 3.70 24.71 3.80 2.57 3.94 23.75 3.44 23.74 3.55 23.72 3.65 24.76 3.48 24.74 3.59 24.73 3.70 24.71 3.80 2.57 3.60 29.71 4.18 29.69 4.30 29.67 4.43 29.66 4.41 29.67 4.26 28.72 4.04 28.70 4.16 28.68 4.29 28.66 4.41 29.69 4.30 29.71 4.18 29.69 4.30 29.67 4.43 29.65 4.56 31 30.68 4.55 31.69 4		-					_		
14	1						•		. = 1
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56 55.46 7.79 55.42 8 04 55.38 8.28 55.35 8.52 57 56.45 7.93 56 41 8.18 56.37 8.43 56.34 8.67 58 57 44 8.07 57.40 8.32 57.36 8.57 57.33 8.82 59 38.43 8.21 58.39 8.47 58.35 8.72 58.31 8.98 60 59.42 8.35 59.38 8.61 59.34 8.87 59.30 9.13 Dep. Lat. Dep. Lat. Dep. Lat.	54	53.47	7.52				7.98	53.37	
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Die.	Lat.	Dep		, Dep	Lut.	Dep.	Lat.	Dep.		
61	60.41	8.49	60.37	8.75	60.33	9 02	60.29	9.28		
62	61.40	8.63	61.36	8.90	61.32	9.16	61.28	9.43		
63 64	62.39	8.77 8.91	62.35	9.04	62.31	9.31	62.27 63.26			
65	64.37	9.05	64.33	9.33	64.29	961	64.24	9.89		
66	65.36	9.19	65.32	9 47	65.28	9.76	65.23	10.04		
67	66.35	9.32	66.31	9.61	66.26	9.90	66.23	10.19		
68	67.34	9.46	67.30		67 25	10.05	67.21	10.34		
70	68.33 69.32	9.60	68.29 69.28	9.90	68.24	10.20	68.20	10.50		
71	70.31	9.88	70.27	10.19	70.22	10.49	70.17	10.80		
72	71.30	10.02	71.25	10.33	71.21	10.64	71.16	10.95		
73	72.29	10.16	72.24	10.48	72.20	10.79	72.15	11.11		
74	73.28	10.30	73.23	10.62	73.19	11.09	73-14	11.26		
75	74.27	10.44	74.22	10.91	74.18	1	74.13	11.41		
76	75.26	10.58	75.21	11.05	75:17	11.25	75.12	11.56		
78	77-24	10.86	77.19	11.19	77.14	11.53	77.09	11.87		
79	78.23	10.99	78.18	11.34	78.13	11.68	78.08	12.02		
80	79 22	11.13	79.17	11.48	79-12	11.82	79-07	12.17		
81	80.21	11.27	80.16	11.62	81.10	11.97	80 06	12.32		
83	82.19	11.55	82.14	11.91	82,09	12.27	82 03	12.63		
84	83.18	1 r.69	83.13	12.05	83 08	12.42	83.02	12.78		
85	84.17	11.83	84.12	12.20	84 07	12.56	84.01	12.93		
86	85.16	11.97	85.11	12.34	85.06	12.71	85.00	13.08		
87 88	86.15	12.11	86.10 87.09	12.48	86.04	12.86	85.99	13.23		
89	88.13	12 39	88.08	12.77	88.02	13.16	87.96	13.54		
90	89.12	12.53	89.07	1291	89.01	13.30	88 95	13.69		
91	90.11	12.66	90.06	13.06	90.00	13.45	89 94	13.84		
92	91.10	12.80	91.05	13.20	90.99	13.60	90.93	14 00		
93	92.09	12.94	92.04	13.34	91.93	13.75	91.92	14.15		
95	94.08	13.22	94.02	13.63	93 96	14.04	93.89	14.45		
96	95.07	13.36	95.01	13.78	94.95	14.19	94 88	14.60		
97	96.06	13.50	96.00	13.92	95.93	14 34	95.87	14.76		
98 99	97.05	13.64	96.99 97.98	14.06	96.92	14.49	96 86 97.85	14.91 15.06		
100	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.28		
101	100.0	14.06	99.95	14.49	99 89	14.93	99.82	15.36		
102	101.0	14.20	100.9	14.64	100.9	15.08	100.8	15.52		
103	102.0	14.33	101.9	14.78	101.9	15.22	101.8	15.8%		
104	103.0	14.47	102.9	14.92	103.8	15.37 15.52	103.8	15.97		
106	105.0	14.75	104.9	15.21	104.8	15.67	104.8	16.13		
107	106.0	14.89	105.9	15.35	105.8	15.82	105.8	16.28		
108	106.9	15.03	106.9	15.50	8.801	15.96	106.7	16.43		
109	107.9	15.17	107.9	15.78	107.8	16.11 16.26	107.7	16.58 16.73		
111								16.89		
712	109.9	15.45 15.59	109.9	15.93 16.07	8.011	16.41	109.7	17.04		
113	111.9	15.73	8.111	16.21	8.11.8	16.70	111.7	17.19		
114	112.9	15.87	112.8	16.36	112-7	16.85	112.7	17.34		
115	113.9	16.00	113.8	16.50	113.7	17.00	113.7	17-49		
116	114.9 115.9 -	16.14 16.28	114.8 115.8	16.65 16.79	114.7	17.15	1147	17.64 17.80		
118	116.9	16.42	116.8	16.93	116.7	17.44	116.6	17.95		
911	117.8	16.56	117.8	17.08	117.7	17.59	117.6	18.10		
120	118.8	16.70	118.8	17.22		17,74	1,18.6	18.25		
ist.	Dep.	Lat.	De p.	Lat.	Dep	Lat.	Dep.	Lati		
<u>a</u>	L		45	-	30		15			
	91 DEGREES.									

Dist	0/		15	,	30		45	1
7	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lut.	Dep.
1	0.99	0.16	0.99	0.16	0.99	0.17	0.99	0.17
2	1.98	0.31	1.97	0.32 0.48	1.97	0.50	1.97 2.96	0.34
3 4	2.96 3.95	0.47	2.96 3.95	0.64	3.95	0.66	3.94	0.68
5	4-94	0.78	4 94	0.80	• 4 93	- 83	4.93	0.85
6	5.93	0.94	5.92	0.96	5.92	0.99	5.91	1.02
7 8	6.91	1.10	6.91 7.90	1.13	6.90 7. 8 9	1.16 1.32	6.90 7.88	1.19
9	7.90 8.89	1.25	8.88	1.45	8.88	1.49	8.87	1.52
10	9.88	1.56	9.87	1.61	9.86	1.65	9.86	1-69
11	10.86	1.72	10.86	1.77	10.85	1.82	10.84	1.86
12	11.85	1.88	11.84 12.83	1.93 2.09	11.84	1.98 2.15	11.83	2.03
13 14	12.84 13.83	2.03	13.82	2.25	13.81	2.31	13.80	2.37
15	14.82	2.35	14.80	2.41	14-79	2.48	14.78	2.54
16	15 80	2.50	15.79.	2.57	15.78	2.64	15.77	2.71
17	16 79	2.66	16.78	2.73	16.77	2,81	16.75 17.74	2.88 3.05
18	17.78	2.82 2.97	17.77	2.89 3.05	17.75	3.14	18.73	3.22
20	19.75	3.13	19.74	3.21	19.73	3.30	19.71	3.39
21	20.74	3.29	20.73	3-38	20.71	3.47	20.70	3.56
22	21 73	3.44	21.71	3.54	21.70	3.63 3.80	21.68 22.67	3.73
23 24	22.72 23.70	3.60 3.75	22.70 23.69	3.70 3.86	22.68 23.67	3.96	23.65	3.90 4.06
25	24.69	3.91	24-67	4.02	24.66	4.13	24.64	4.23
26	25.68	4.07	25.66	4.18	25.64	4.29	25.62	4.40
27	26.67	4.22	26.65	4-34	26.63	4.46	26.61	4-57
28 29	27.66 28.64	4.38 4.54	27.64 28.62	4.66	27.62 28.60	4.62	27.60 28.58	4.74 4.91
30	29.63	4.69	29.61	4.82	29.59	4.95	29.57	5.08
31	30.62	4.85	30 60	4.98	30.57	5.12	30.55	5.25
32	31.61	10.2	31.58	5.14	31.56	5.28	31.54	5.42
33	32-59	5.16	32:57 33.56	5.30 5.47	32.55	5.45 5.61	32.52 33.51	5.59 5.76
34 35	33.58 34.57	5.32 5.48	34-54	5.63	34.52	5.78	34-49	5 93
36	35.56	5.63	35-53	5.79	35.51	5.94	35.48	6.10
37	36.54	5-79	36.52	5.95	36.49	6.11	36.47	6.27
38 39	37·53 38.52	5.94 6.10	37.51 38.49	6.11	37.48 38.47	6.27 6.44	37-45 38.44	6.44 6.60
40	39.51	6.26	39.48	6.43	39-45	6.60	39.42	6.77
41	40.50	6.41	40.47	6.59	49 44	6.77	40,41	6.94
42	41.48	6.57	41.45	6.75	41.42	6.93	41.39	7.11
43 44	42.47	6.73 6.88	42.44	6.91 7.07	42.41 43.40	7.10 7.26	42.38 43.36	7.28 7.45
45	43.46 44.45	7.04	43.43	7.23	44-38	7-43	44-35	7.62
46	45.43	7.20	45.40	7.39	45-37	7.59	45-34	7.79
47	46.42	7.35	46.39	7.55	46.36	7.76	46.32	7.96
48	47.41	7.51 7.66	47.38 48-36	7.72	47·34 48·33	7.92 8.09	47.31 48.29	8.13 8.30
49 50	48.40	7.82	49-35	8.04	49.31	8.25	49.28	8.47
51	50.37	7.98	50.34	8.20	50.30	8.42	50.26	8.64
52	51.36	8.13	51.32	8.36	51.29	8.58	51.25	8.81
53	52.35	8.29	52.31	8.52 8.68	52.27	8.75 8.91	52.23 53.22	8.98 9-14
54 55	53-34 54-32	8.45 8.60	53.30 54.28	8.84	53.26 54.25	9.08	54.21	9.31
56	55.31	8.76	55.27	9.00	55.23	9.24	55.19	9.48
57	56.30	8.92	56.26	9.16	56.22	9.41	56.18	9.65
58	57.29	9.07	57.25	9.32	57.20	9-57	57.16	9.82
59 60	58.27 59.26	9.23 9.39	58.23 59.22	9.48 9.64	58 19	9.74 9.90	58.15	9.99 10.16
			Dep.	Lat	Dep	Lat	Dep	Lat.
Dist.	Dep. Lat.		45		30′		13	
		-			REES.			

Dist	0,		. 15/		3	0'	45	7
2	Lat	Dep.	Lat.	Dep	Lat	Dep.	Lat	Dep
61	60.25	9.54	60 21	9.81	60.16	10.07	60.12	10.33
62 63	61.24	9.70	61.19	9.97	61.15	10.23	61.10	10 50
64	63.21	10.01	62.18	10.13	62.14 63.12	10.40	62.09 63.08	10.67
65	64-20	10.17	64.15	10 45	64.11	10.73	64.06	11.01
66	65 19	10.32	05.14	10.61	65.09	10.89	65.05	11.18
67 68	66.18	10.48	66.13 67.12	10.77	66.08 67.07	11.06	66.03	11.35
69	68.15	10.79	68.10	11.09	68 05	11.39	67.02 68.00	11.52
70	69.14	10.95	69.09	11.25	69 04	11.55	68.99	11.85
71	70.13	11.11	70.08	11.41	70.03	11.72	69.97	12.02
72 73	71.11	11.26	71.06	11.57	71.01 72.00	11.88	70.96	12.19 12.36
74	73.09	11 58	73.04	11.90	72.99	12.21	71.95 72.93	12.53
75	74.08	11.73	74.02	12 06	73-97	12.38	73 92	12.70
76	75.06	11.89	75.01	12.22	74.96	12.54	74.90	12.87
77 78	76.05 77.04	12.05	76.00 76.99	12.38 12.54	75.94 76.93	12.71	75.89 76.87	13.04 13.21
79	78.03	12.36	77.97	12.70	77.92	13.04	77.86	13.38
80	79.02	12.51	78.96	12.86	78.90	13.20	78.84	13.55
81 82	80.00	12.67	79 95	13.02	79.89	13.37	79.83	13.72
83	80.99	12.83	80.93 81.92	13.18 13.34	80.88 81.86	13.53 13.70	80.82 81.80	13.89 14.06
84	82.97	13.14	82.91	13.50	82.85	13.86	82.79	14.23
85	83.95	13.30	83.89	13.66	83.83	14.03	83.77	14.39
86 87	84.94	13.45	84.88	13.82	84.82	14.19	84.76	14.56
88	85.93 86 [.] 92	13.61 13.77	85.87 86.86	13.98 14.15	85.81 86.79	14 36 14.52	85.74 86.73	14.73
89	87 90	13.92	87.84	14.31	87.78	14.69	87.71	15.07
90	88.89	14.08	88.83	14 47	88.77	14.85	88.70	15.24
91 92	89.88 90.87	14.24	89.82 90.80	14.63	89.75	15.02	89.69	15.41
93	91.86	14.39	91.79	14-79 14-95	90.74	15.18	90.67 91.66	15.58
94	92.84	14.70	92 78	15.11	92.71	15.51	92.64	15.92
95	93.83	14.86	93.76	15 27	93.70	15.68	93.63	16.09
96 97	94.82 95.81	15.02 15.17	94·75 95·74	15.43 15.59	94.68 95.67	15 84 16.01	94.61 95.60	16.26 16.43
98	96.79	15.33	96.73	15.75	96.66	16.17	96.58	16.60
99	97.78	15.49	97-71	15.91	97.64	16.34	97.57	16.77
101	98.77	15.64	98.70	16.07	98 63	16.50	98.56	16.94
102	99.76 100.7	15.96	99.69 300.7	16.40	99.61	16.67 16.83	99.54 100.5	17.10
103	101.7	16.11	101.7	16.56	101.6	17.00	101.5	17.44
104	102.7	16.27 16.43	102.6 103.6	16.72 16.88	102.6	17.17	102 5	17.61
106	104.7	16.58	104.6	17-04.	103.6	17.33	104.5	17.74
107	105.7	16.74	105.6	17 20	105.5	17.66	105.5	17.95 18.12
108	106.7	16.90	106.6	17.36	106.5	17.83	106.4	18.29
109	107.7	17.05	107.6	17.52	107.5	17.99 18.16	107.4	18.46
111	109.6	17.36	100.6	17.84	109.5	18.32	109.4	18.80
112	110.6	17.52	110.5	18.00	110.5	18.49	110.4	18.97
113	111.6	17.68	111.5	18.16	111.5	18.65	111.4	19.14
115	112.6	17.83	112.5	18.32 18 49	112.4	18.82 18.98	1124	19.31
116	114.6	18.15	114.5	18.65	114.4	19.15	114.3	19.6
117	115.6	18.30	115.5	18.81	115.4	19.31	115.3	19.8
1 18 1 19	116.5	18.46	116.5	18.97	116.4	19.48	116.3	19.9
120	118.5	18.77	117.5	' 19.13 119.29	117.4	19.64 119.80	117.3	20.
핖	Dep.	Let.	Dep.	Lat.	Dep.	Lat.	Dep.	L
Dist)′	45	<u> </u>	30		15	<u>'</u>
			-	DEGR				

90 Degrees.

1 5	0' 15'				30		45	
Diet	Lat.	Dep.	Lat	D n	Lat.	Dep.	Lat	Dep.
	0.98	0.17	0.98	0 18	0.98	0 18	0.98	0.19
1 4	1.97	0.35	1.97	0.36	1.97	0.36	1,95	0.37
3	295	0.52	2.95	0.53	3.95	0.55	2.95	0.56
4	3 94	0.69	3-94	0.71	3-93	0.73	3-93	0.75
5	4.93	0.87	4.92	0.89	492	0.91	4-91	0.93
6	5.91	1.04	5.90	1.07	5.90	1.0g	5.89	1.12
7 8	6.89 7.88	1.38	6.89 7.87	1.43	7.87	1.46	7.86	1.31 f.49
•	3.86	1.56	8.86	= -	8.89	1 64	8.84	2.68
10	9.85	1.74	9.84	1.78	9.83	1.81	9.82	2.87
11	10.83	1.91	10.82	1.96	10.82	2.00	10.81	1.05
13	11.82	2.08	11.81	MI4	11.80	3.19	21.79	2.24
13	12.80	2.26	12.79	2.31	12.78	2.37	18-77	2.42
14	13.79	2 43	13.78	2.49	13-77	2-55	13-75	3.61
15	14.77	2.60	14.76	2.67	_\$4-75	2.73	14-74	2.30
16	15 76	2.78	15.74	4.85	15 73	2.92	15.72	2.98 3.17
17	16.74	3.95	16.73	3.40	15.72	3.10	16.70	3.36
18	17.73	3.30	18 70	3.38	17.70	3.46	18.67	3-54
19	19.70	3.47	19 68	3.56	19 67	3.64	19,65	3.73
21	20.68	3.65	10.66	3.74	10.65	1 83	20 63	3.92
1 12	21.67	3 82	21.65	3 91	31.63	401	23.61	4-10
23	22.65	3.99	22.63	4-09	23.61	419	21 60	4-29
14	23 64	4.17	23.62	4-27	23.60	4-37	23.58	4.48 4.66
35	24.63	4-34	14.60	4-45	24.58	4.56	24.56	
26	25.61	4-51	25.59	4-63	25.56	4.74	25.54	4 85 504
27	26.59	4-69 4-86	26.57	4.80 4.98	26.55 27.53	4-92 5 to	26.53 27.51	5.22
28	27.57 28 56	5.04	27.55 28.54	5.16	28.51	5.28	28.49	5-41
30	19.54	5.21	29 52	5-34	39 50	5 47	19-47	5.60
31	30.53	5.38	30 51	5.52	30 48	5.65	30.46	\$ 78
32	31.51	1.56	31 49	1 5.69	31 46	5.83	31-44	5.97
33	32.50	5.73	33.47	, 587	32.45	10.0	32.42	6.16
34	33.48	5 90	33.46	6.05	33-43	6.20	33.40	6 34
35	34-47	6.08	34-44	6.13	34.41	6 38	34-39	6-53
36	35-45	6.43	35 43	6.41 6.58	35.40	6.56	35-37	6.71 6.90
37	36.44 37-43	6.60	36 41 37-39	6 76	37.36	6.92	36.35	7 09
38 39	38.41	6.77	38 38	6 94	38.35	7.11	38 32	- 27
40	39.39	6.95	39.36	7.12	39-33	7.29	39.30	2 40
41	40.38	7.13	40.15	7.30	40.31	7 47	40.28	7.05
42	41.36	7.29	41.33	7.47	41.30	7.65	41.36	7 83
43	43-35	7-47	42 31	765	42.18	7.84	42.35	8.01
44	43-33	7.64	43.20	7 83 8 Ot	43.26	\$.04 \$.50	43.11	8.39
45	44-31		44.28			8.38	44.21	8 58
46	45.30 46.29	7.99	45.27	3.36	45.21	8.57	45.19	8.77
47 48	47.27	1.34	47-23	8.54	47.20	8.75	47.16	8 95
49	48,16	8.5 E	48.22	\$.72	48.18	8.93	48 14	9-14
50	49.34	8.68	49.10	8.90	49.16	9.11	49.12	9-33
51	50.13	8.86	50.19	9.08	50.15	9.29	60-11	9.51
52	51.21	9.03	\$1.17	9.25	51.13	9-48	5109	9.70
53	52.19	9.20	52.15	9.43	52,11	9.66 9.84	\$2.07	9 89
54	53,18 54,16	9.38	53.14	9.61	54.08	70.02	53.05	10.26
55		9.55	54 12		55.06	10.21		10.45
56	\$5.15 \$6.13	9.72	55.11	y.96 10.14	56.05	10.39	56,00	10.63
57 58	57.13	10.37	57.07	10.32	57.03	10.57	56 98	1Q 82
59	58.10	10.25		10.50	58.01	10.75	57.96	1100
66	59.09	10.43	59.04	10.68	59.00	10.93	58.95	11 19
1	Dep.	Lat	Dep.	Lat	Hep.	Lat	Dep.	Lut
Dist	0		45	51	SC) , —	1:	5,
1	DI U		70	DECE				

f	8) ¹	1.5	j'	30) 1	4	<u> </u>	
1	Dist.	La.	Dep.	Lat.	Dep	La	Dep	L.	Dep.	
1	61	00.07	10 59	60.03	10.85	59.98	1112	59.93	11.38	
į	63	6100	10.77	61 01	11.03	60 46	11.30	60.91	11.56	
	63	52.04	10 94	61.09	11 24	61.95	11.48	61 89	11.75	
1	64 65	63.33	11.11	62.98 63.96	11.39 11.57	62.93 63 91	11.66	62.88	11.94	
1	66	65.00	11.46	64.95	11.74	64.89	12.03	64.54	12.31	
Ì	67	65.98	11.63	65.93	11.92	65.88	12 21	65.82	12.50	
1	68	66.97	11.81	66.91	12.10	66.86	12.39	66 81	12.68	
1	69	67.95	11.98	67.90 68 88	12.28	67 84 68.83	12.57	67.79 68.77	12.87	
1	70	68.94			1 2.46		12.76	-	13.06	
I	71 72	6y.92 7~91	12 33	69.87	12.63	69.81 70.79	12.94	69.75	13.24	
ł	73	7184	12.68	71.84	12.99	7178	13.30	71.72	13.62	
ł	74	72.88	12.85	72.82	13.17	72.76	13.49	72.70	13.80	
\$	75	73.86	13.02	73.80	13.35	73 74	13.67	73.68	13 90	
I	76	74.85 75.83	13.20	74·79 75 77	i 3 52 13 70	74-73 75.71	13.85	74 67 75.65	14.36	
I	77	76.82	13.54	76.76	13.86	76.6y	14.21	76.63	14 55	
ł	79	77.80	13.72	77-74	14.06	77.68	14.40	77.61	14.74	
İ	80	78.78	13.89	78.72	14.24	78 66	1458	78.60	14.92	
	81	79-77	14.07	79.71	14.41	79.64	14.76	79.58	45.41	
•	82 83	80 75	14.24	80.69 81.68	14.59	80.63 81.61	14.94	80.56 81.54	15.30	
ı	· 84	82.72	14.59	82.66	14.95	82.59	1531	82.53	15.67	
ł	85	83.71	14.76	83.64	15.13	83.58	15.49	83.51	15.85	
Ì	86	84.69	14 93	84.63	15.30	84 56	15.67	84.49	16.04	
ł	87	85.68 8 6. 66	15.11	85.61 86.60	15.48	85-54 85.53	15.85	85.47 86 46	16.23 16.41	
I	88 89	87.65	15.28	87.58	15.66	87.51	16.22	87 44	16.60	
ł	90	88.63	15.63	88.56	1601	88:49	16.40	88.42	16.79	
I	91	89.62	15.80	89.55	16 19	89.48	16.58	89.40	16.97	
Ì	92	90.60	15.98	90.53	16.37	90.46	16.77	90.39	17.16	
ŧ	93	91.59	16.32	91.52	16.55	91.44 92.43	16.95	91 37 92.35	17.35	
ł	94 95	93.56	16.50	93.43	16 90	93 41	17.31	93 33	17.72	
İ	96	94.54	16.67	94-47	17.08	94.39	17.49	94-32	17.91	
I	97	95.53	16.84	95.45	17.26	95.38	17.68	95.30	18.09	
I	98	96.51	17.02	96 44	17.44	96.36	17 86 18.04	96.28	18.28	
1	100	97.50 98.48	17.19 17.36	97.42 98.40	17.62	97·34 98.33	18.22	97.26	18.63	
1	101	99.47	17-54	99.39	17.97	99.31	18 41	99.23	18.84	
	102	100.4	17.71	100.4	18.15	100.3	18.59	100.2	19.03	
	103	101.4	17.89	101.4	18.33	101.3	18.77	101.2	19.21	
Ŧ	104	102.4	18.06 18.23	102.3	18.51 18.68	102.3	18.95	102.2	19.40	
1	106	104.4	18.41	104.3	18.86	104.2	19.32	104.1	19.77	
•	107	105.4	18.58	105 3	19.04	105.2	19.50	105.1	1906	
I	108	106.4	18.75	106.3	19 22	106 2	19.68	106.1	20;14	
	109 110	107.3	18 93	107.3	19.40	107.2	19 86 20.05	107.1	20.32 20.52	
ŀ	111		19.10		19.57	109.1	20.23	109.1	20.70	
- 1	112	109 3	19.28	109.2	19.75	110.1	20.41	110.0	20.70	
ľ	113	111.3	19.62	111.2	20 11	111.1	20.59	111.0	21.05	
1	114	112.3	19.80	112.2	20.29	1121	20.77	112.0	21.26	
•	115	113.3	19.97	113.2	20.46	113.1	20.96	1130	21.45	
- 1	116	114.2	20.14	114.1	20.64	114.1	21 14	114.0	21.60	
•	118	116.2	20.49	116.1	21.00	116.5	21.50	115.9	22.01	
•	119	117.2	20,66	117.1	21.18	117.0	21.69	116.9	22.20	
į.	120	118.2	20.84	118.1	21.35	118.0	21.87	117.9	22.38	
1	Dist	Den	Lat.	Dep	Lat.	Dep.	Lar.	Dep.	Lut.	
Ī	2	U		4			301	1	:1	
	79 DEGREES.									

Dist	07		15	7	30),	4	
7	Lat	Dep.	Lat.	Dep.	Lat	Dep.	Lat.	Dep
	0,98	0.19	0.98	0.20	0.98	0.20	0.98	0.20
2 4	1.96	0.38	1.96	0.39	1.96	0.40	1.96	0.41
3	2.94	0.57	2.94	0.59	2.94	0.60	2.94	0.61
4 5	3 93 4.91	0.76 0.95	3.92 4.90	0.78	3.92 4.90	1.00	3.92 4.90	1.03
6	5.89	1.14	5.88	1.17	5.88	1 20	5.87	1.22
7	6.87	1.34	6.87	1.37	6.86	1.40	6.85	1.43
8	7.85	1.53	7.85	1.56	7.84	1.59	7.83	1.63
9	8 83 9.82	1.72	8.83 9.81	1.76	8.82 9. 8 0	1.79	8.81	1.83
10		1.91		1.95		1.99	9.79	1.04
12	10.80	2.10 2.29	1 0 .79	2.15 2.34	10.78	2.19 2.39	10.77	2.24
13	12.76	2.48	12.75	2.54	12.74	2.59	12.73	2.65
14	13.74	2.67	13.73	2.73	13.72	2.79	13.71	2.85
15	14-72	2.86	14.71	2.93	14-70	2.99	144.9	3.05
16	15.71	3.05	15.69	3.12	15.68	3 19	15.66	3.26
17	16.69 17.67	3.24	16.67 17.65	3.32 3.51	16.6 6 17.64	3.39 3.59	16.64	3.46 3.67
19	18.65	3.63	18 63	3.71	18.62	3.79	18.60	3.89
20	19.63	3.82	19.62	3.90	19.60	3-99	19.58	4.07
21	20.61	4.01	20.60	4.10	20.58	4.19	20.56	4.28
32	21 60	4.20	21 58	4.29	21.56	4-39	21.54	4.48
23 24	22.58 23.56	4-39 4-58	22.56 23.54	4.49 4.68	22 54 23.52	4·59 4·78	32.52	4.68 4.89
25	24 54	4.77	24.52	4.88	24.50	4.98	23.50 24.48	5.09
26	25.52	4.96	25.50	5.07	25.48	5.18	25.46	5 29
27	26 50	5.15	26 48	5.27	26 .46	5.38	26.43	5.50
38	27-49	5-34	27.46	5 46	27.44	5.58	27.41	. 5.70
29	28.47 29.45	5-53	28.44 29.42	5.66 5.85	28.42	5.78 5.98	28.39 29.37	5.91
-	30.43		30 40	6.05	29.40 30.38	6.18		6.31
31 32	31.41	5.92	31.39	6.24	31.36	6.38	30.35 31.33	6.52
33	32.39	6.30	32.37	6.44	32 34	6.58	32 31	6.72
34	33.38	6.49	33.35	6.63	33.32	6.78	33.29	6.92
35	34 36	6.68	34-33	683	34.30	6.98	34.27	7.13
36 37	35·34 36.32	6.87 7.06	35.31 36.29	7.02 7.22	35.28 36.26	7.18 7.38	35.25 36.22	7.33
38	37.30	7.25	37.27	7.41	37.24	7 58	37.26	7·53 7·74
39	38.28	7-44	38 25	7.61	38.22	7.78	38 18	7.94
40	39.27	7.63	39.23	7.80	39.20	7-97	39.16	8.15
41	40.25	7.82	40.21	8.00	40.18	8.17	40. 14	8.35
42	41.23	8.01 8.20	41.19	8.19 8.39	41.16	8.37 8 57	4112 42.10	8.55 8.76
44	43.19	8.40	43.15	8.58	43.12	8.77	43.08	8.96
45	44-17	8.59	44-14	8.78	44.10	8.97	44.06	9.16
46	45.15	8.78	45.12	8.97	45.08	9.17	45 04	9.37
47	46.14	8.97	46.10	9.17	46.06	9.37	46.03	9.57
49	47.12	9.1 6 9.35	47.08 48.06	9.36 9.56	47.04 48 02	9·57 9·77	46 9 9 47-97	9.77
50	49.08	9.54	49.04	9.75	49.00	9.97	48.95	9.98 10.18
51	50.06	9.73	50.02	9.95	49.98	10.17	49.93	10.39
52	51.04	9.92	51.00	10.14	50.96	10.37	20.91	10.59
53	52.03	10.11	51.98	10.34	51.94	10.57	51.89	10.79
54 55	53.01	10.30	52.96 53.94	10.53	52.92 53.90	10.77	52.87 53.85	11.00 11.20
56	54.97	10.00	54.92	10.93	54.88	11 16	54.83	17.40
57	55.95	10.88	55 90	11.12	55 86	11.36	55.81	11.61
58	56.93	11.07	56.89	11.32	56.84	11.56	56 78	11,81
59	57.92	11.26	57.87 58.85	11.51	57.82	11.76	57.76	12.01
	58.90	11.45		11.71	58.80 Des	11.96	58.74	12.22
Dist	1)ep	Lat	-	Lat	Dep.	Lat.	Dep.	Lat.
10		/	4.5	/	30	1	15	'

-	9	-	1	37	. 3	91 .	454	,
1 1	Lat	Dep	Eat	Dep	Lat.	Dep.	Lat.	Dep.
61	59.88	11.64	59.81	11.90	59-78	12 16	59-72	12.45
62	60.\$6 61.\$4	11.83	60.81	12.10	60.76	12.36	60.70	12.63
63	61.81	12.21	62.77	12.49	62.72	12.76	88.90	13.03
66	63.8r	11.40	63.75	12.68	63.70	12.96	63.64	13.14
66	64.79	12.59	64-73	12 88	64.68	13.10	64 62	13-44
67	65.77 66.75	13.78	66.6g	13.07	65.66 66 63	13.3 6 13.56	65 63 66 58	13.64 : 13.85
69	67 73	13.17	67.67	13.46	67.61	:3 76	67.55	14.05
70	\$8.7 L	13.36	68.66	13.66	68.59	13.96	68.53	14 25
71	69.70	13 55	69.64	13 85	69.57	14-16	69.51	14 46
72 73	70 68 71.66	13.74	70,62	14-05	70.55	14-35 14-55	79 49	14 87
1 54	72.64	14.12	72.58	14-44	72 51	14-75	74-45	15.07
75	73.64	14:31	73 56	14-63	73-49	14-95	73-43	15.87
76	74.60	14 50	74-54	14 83	74-47	15.45	74-41	15 68
77	75.59	14.69 14.88	75,52	15 02	75.45	15.35 15.55	75 39 76 37	15.88
79	77-55	15.07	77-48	15 41	77-45	15-75	77-34	16.09
80	78 53	15.26	78 46	15-61	78 39	15.95	78.32	16 29
81	79-51	15.65 15.65	79-44 \$0.43	16.00	79-37 80 35	16.15 16.35	79-30 80.28	16.50
8;	\$0.49 \$1.48	15.84		16.19	\$1.33	16.55	81.26	16.90
84	\$4.46	16.03	\$2.34	16.30	\$2 31	16.75	82.24	17.46
8.	\$3-44	19.23	83-17	16.58	\$3 29	16.95	83 21	£7 31
87	84.43 85.40	16.41 16.60	\$4-35 \$5.33	16.78 10.97	\$4.27 \$5.45	17-35	84.20	17.51
88	\$6 38	16 79	\$6.31	17.17	\$6.23	17-54	26.16	17.92
84	\$7.36	16.98	\$7.29	17.36	\$7.21	17-74	87.14	18.11
93	\$8.35	17-17	\$8 27	17.56	\$8.19	17 94	11.68	18.33 18.53
91	9031	17.38	\$9 25 90.23	17 75 17 95	\$9.17 90.15	18.14 18.34	89.09 90.07	18.74
93	91-29	17.75	91.21	14.14	şt. iğ	18 54	91.05	18.94
94	92.27	17-94	92.19	! !! 34	92.11	18.74	9103	19.35
96	\$3.25	18,13	93.17	18.53	93.59	18.04	93.01	
96 97	94-24	18.32 18.51	94.10	16 73 18.92	94.07	19-14 19-34	93 99	19.75
98	96,20	18 70	96,12	19.12	96.03	19.54	95-95	19.96
99	97.18	18.89	97,10	19 31	97.01	19-74	96.93 97.90	20.16 20.36
100	y8.16	19.08		19 51	97-99	19.94	·yd.88	10-57
101	99-14	19.27 19.46	99.06	19.70	99-95	20.34	99.86	20.77
103	101-1	19 65	0.10	20.09	100.9	30 53	8.001	20.98
104	1.401	19 84 20.04	102.0	10.19 20.48	103.9	10.73 10.93	101.8	21 58
105	103.1	20.13	104 0	10.64	101 9	31 13	103.8	21.59
106	1941	20.42	104-9	20-87	104.9	21 33	104.\$	21.79
108	100.0	20.61	105.9	21-07	105.8	21.53	105.7	21 99
10g	108.0	20.80 20 99	106.9 107.9	21.26	106.8	21.93	106.7	21.40
411	0.001	21,18	108.0	31 66	108.8	21.13	108.7	11 60
113	419-9	21.37	159 8	at.85	109.8	22.33	109.7	22.81
in l	110.9	21.56	110.8	22.05	110.7	22 53	110.6	23.01
815	1119	21.75	112.8	22.24 22.44	1117	22 7J 22 93	1126	23.48
116	113.9	21.12	113.8	21.63	113.7	27 13	1436	23.02
617	1149	23 32	114-7	22 83	114 6	23.33	114.5	23 83
218	115.8	22.52	115.7	23.02	115.6	23.53	315.5 116.5	14.03
219 230	116.8	22.71	116.7	123.22 123.41	117.6	23 72	117-5	21 44
1-	Dep	Late	13e;	L:	Dep.	170	Ben,	Lak
180)/	-	;——	30		1	, -
والمساوري		7 9 2 4 9 9	MR	DEGE				-

Γ	Diet.	0/		15/		30	0'	451	
1	7	Lat	Dep.	Lat.	Dep.	Lat	Dep.	Lat.	Dep.
1	-	0.98	0.19	0.98	0.20	0.98	0.20	0.98	0.20
	2	1.96	0.38	1.96	0.39	1.96	0.40	4.96	0.41
Ī	3	2,94	0.57	2.94	0.59	2.94	0.50	2.94	0.61
ľ	4	3-93	0.76	3.92	0.78	3.92	0.80	3.92	0.81
L	5	4.91	0.95	4.90	0.98	4.90	1.00	4.90	
I	6	5.89 6.87	1.14	5.88 6.87	1.17	5.88 6.86	1 20	5.87 6.85	1.22
ı	7	7.85	1.34	7.85	1.37 1.56	7.84	1.40	7.83	1.43
ł	9	8 83	1.72	8.83	1.76	8.82	1.79	8.81	1.83
ł	10	9.82	1.91	9.81	1.95	9.80	1.99	9.79	2.04
1	11	10.80	2.10	10.79	2.15	10.78	2.19	10.77	2.24
I	12	11.78	2,29	11.77	2.34	11.76	2.39	21.75	2.44
1	13	12.76	2.48	12.75	2.54	12.74	2.59	12.73	2.65
1	14	13.74 14.72	2.67 2.86	13.73 14.71	2.73 2-93	13.72	2.79 2.99	13.78	2.85 3.05
-	15			15.69		15.68	-		3.26
ł	16 17	15.71	3.05 3.24	16.67	3.12 3.32	16.66	3 19 3.39	15.66	3.46
1	18	17.67	3.43	17.65	3.51	17.64	3.59	17.62	3.67
1	19	18.65	3.63	18 63	3.71	18.62	3.79	18.60	3.87
1	20	19.63	3.82	19.62	3.90	19.60	3.99	19.58	4.07
1	21	20.61	4.01	20,60	4.10	20.58	4.19	20.56	4.28
	22	21 60	4.20	21 58	4.29	21.56	4.39	21.54	4.48
4	23	22.58 23 56	4-39	22.56 23.54	4.49 4.68	22 54	4-59 4-78	32.52	4.68 4.89
1	25	24 54	4.58 4.77	24.52	4.88	23.52 24.50	4.98	23.50 24.48	5.09
-	25	25.52	4.96	25.50	5.07	25.48	5.18	25.46	5 29
ł	27	26 50	5.15	26 48	5.27	26 .46	5.38	26.43	5.50
ı	28	27.49	5-34	27.46	5 46	27.44	5,58	27.41	5.70
1	29	28.47	5.53	28.44	5.66	28.42	5.78	28.39	5.91
-	30	29.45	5 72	29.42	5.85	29.40	5.98	29.37	6 1 1
	31,	30.43	5.92	30.40	6.05	30.38	6.18	30.35	6.31
ł	32	31.41	6.11	31.39	6.24 6.44	31.36 32 34	6.38 6.58	31.33 32 31	6.52 6.72
I	33 34	33.38	6.49	33.35	6.63	32.34	6.78	33.29	6.92
I	35	34 36	6.68	34-33	6.83	34.30	6.98	34.27	7.13
1	36	35.34	6.87	35.31	7.02	35.28	7.18	35.25	7.33
1	37	36.32	706	36.29	7.22	36.2 6	7.38	36.22	7-53
}	38	37.30	7-25	37.27	7.41	37-24	7 58	37.26	7-74
ł	39 40	38.28	7.44	38 25	7.61	38.22	7.78	38 18 39.16	7-94 8.15
ŀ						39.20	7.97		
	41 42	40.25	7.82	40.21	8.00	40.18	8.17 8.37	40. F4 41.12	8.35 8.55
	43	42.21	8.20	42.17	8.39	42.14	8.57	42.10	8.76
}	44	43.19	8.40	43.15	8.58	43.12	8.77	43:08	8.96
Ŀ	45	44-17	8.59	44-14	8.78	44.10	8.97	44.06	9.16
Į	46	45.15	8.78	45.12	8.97	45.08	9.17	45.04	9.37
ł	47 48	46.14	8.97	46.10	9.17	46.06	9:37	46.02	9-57
	49	47.12	9.1 6 9.35	47.08 48.06	9.36 9.56	47.04 48.02	9·57 9·77	46 9 9 47-97	9-77
ł	50	49.08	9.54	49.04	9.75	49.00	9.97	48.95	9.98 10.18
ľ	51	50.06	4.73	50.02	9.95	49.98	10.17	49.93	10.39
	52	51.04	9.92	51.00	10.14	50.96	10.37	20.91	10.59
ł	53	52.03	10.11	51.98	10.34	51.94	10.57	51.89	10.79
I	54	53.01	10.30	52.96	10.53	52.92	10.77	52.87	11.00
1-	55	53.99	10.49	53.94	10.73	53.90	10.97	53.85	11.20
	56	54.97	10.88	54.92	10.93	54.88	11 16	54.83	17.40
	57 58	55.95 56.93	11.07	55 90 56.8 9	11.12	55 86 56.84	11.36	55.81 56 78	11.61
Ĭ	59	57.92	11.26	57.87	11.51	57.82	11.76	57.76	18.01
L	60"	58.90	11.45	58.85	11.71	58.80	11.96	58.74	12.23
	ید	Dep	Lat	Dep.	Lat	Dep.	Lat.	Dep.	Lat.
	Dist	0	/	45		30		15	
1	-				DECL		يتكاف شدني		

1 =	Ü	υ/ 15/			30' 45'			
7	Lui.	Dep.	Lat.	13-p.	Lat.	D.p.	f.at.	Dep.
61	59.67	12.68	59.61	12.94	59.55	13.20	59.50	13.46
62	60.65	12.89	60.59	13.16	60.53	13.42	60.47	13.68
63	61.62	13.10	61.57	13.37	61.51	13.64	61.45	13.90
65	63.58	13.51	63.52	13.79	63.46	14.07	63.40	14.12
66	64.56	13.72	64.50	14.00	64 44	14.29	64.37	14-57
67	65.54	13.93	65.47	14.22	65.41	14.50	65.35	14.79
68	66 51	14.14	66.45	14.43	66.39	14.72	66.32	15.01
69	67.49 68.47	14 35	67.43 68.41	14.64	67.36 68.34	14.93	67.30 68.27	15.23
71	69.45	.4.76	69.38	15.06	69.32	15.37	69.25	15.67
72	70.43	14.97	70.36	15.28	70.29	15 58.	70.22	15.89
73	71.40	15.18	71.34	15.49	71.27	15.80	71.20	16.11
74	72.38 73.36	15.39	72.32	15.91	72 25	16.02	72.18	16.33 16.5 9
76	74.34	15,80	74:27	16.13	74.20	16.45	74.13	16.77
77	75.32	16.01	75.25	16.34	75-17	16.67	75.10	16.99
78	76.30	16.22	76.22	16.55	76.15	16.88	76.08	17.21
79 80	77 27 78.25	16.43	77.20 78.88	16.76 16.97	77.13	17.10	77. 0 5 78. 03	17.44
81		16.84	79:16		79.08	17 53		17.88
82	79.23	17.05	80.13	17.19	80.06	17.75	79.00 79.98	18.10
83	81.19	17.26	81.11	17.61	81.03	17.96.	80.95	18.32.
84	82 16	17 46	82.09	17.82	82.01	18.18	81.93	18.54
86	83.14	17.88	83.06	18.04	82.99	18.61	82.90	18.76
87	84.12	18.09	84 04 85,02	18.25	83.9 6 84.94	18.83	83.88 84.85	18.98 19.20
88	86 08	18.30	86.00	18.67	85.91	19.05	85.63	19.48
89	87.06	18.50	86.97	18.88	86.89	19.26	86.81	19.64
90	88 03	18.71	87.95	19.10	87.87	19.48	87.78	19.86
91	89.01 89.99	18.92 19 F3	88.93	19.31	88 84 89 82 -	19.91	88.76 89.73	20.08
93	90.97	19.34	90.88	19.73	90.80	20 13	90.71	20.52
94	91 95	19.54	91.86	19 94	91.77	20.35	91.68	20.75
95	92.92	19.75	92.84	20.16	92.75	20.56	92.66	20.97
96 97	93.90 94 88	19.96	94.79	20.37	93.72	20.78 20.99	93.63 94 61	21.19
98	95.86	20.38	95.77	20.79	95.68	21.21	95.58	21.63
99	96.84	20.58	96.75	21.01	96.65	21.43	96.56	21.85
107	97.81	20.79	97 72	21 22	97.63	21.64	97.53	22.07
101	98.79 99.77	21.00	98.70 99.68	21.43	99. 61	21.86	, 98.51 99.49	24.29 24.51
103	100.7	21.41	100.7	21.85	100.6	22.29	100.5	22.73
104	101.7	21.62	101.6	22 07	101.5	22.51	101.4	22.95
105	102.7	21.83	102.6	22.28	102 5	22.73	102.4	23 17
106	103.7	22.04 22.25	103.6	22 49	103 5	22.94 23.16	103.4.	23.39 23.61
108	105.6	22.45	105.5	22.92	105.4	23 38	105 3	23.84
109	106.6	22 66	106.5	23.13	106.4	23.59	106.3	24.06
110	107.6	22.87	107.5	23.34	107.4	23.81	107.3	24.28
1111	108.6	23.08	108.5	23.55 23.76	108.4	24.02	108.3	24.50
1112	109.6	23.29 23.49	109.4	,23.98	109.3	34.46	109.2	24.73 24.94
114	111.5	23 70	111.4	24.19	111.3	24 67	111.2	25.16
115	112.5	23.91	1124	24.40	112.3	24.89	112.2	25.38
1116	113.5	24 12	113.4	24.61 24.82	113.3	25.11	113.1	25.60 25.82
1117	1154	24 33 24 53	114.3	24.02	114.2	25.54	114.1	26.04
119	116.4	24 74	116.3	25.25	116.2	25.76	116.1	26.26
120	117.4	24 95	117.3	25.46	717.3	25.97	117.0	26 68
Dist.	Dep.	Lat	Dep	Lat	Dep.	Lat.	Dep.	Lat
	' 0	· ·	45	الكالة الأراب المرابع	30		15	1
			77	DEGH	KES.			~ ~ ~ ·

TE	0		1	1	30	7	43	
D.	Lat	Dep	Lat.	Dep.	Lut.	Den.	Lat	Dep.
-	0.97	0.23	0.97	0.23	0.97	0.13	0.97	0 24
2	1.95	0.45	1.95	0.46 0.6g	1.94	9.47 9.70	, 1.94 2.91	0.4 8 0.75
3 4	3.90	0.67	2.92 3.89	0.93	2.92 3.89	0.93	3,89	2.95
5	4.87	1.12	4.87	1.15	4.86	1.17	4.86	1.19
6	5.85	1.35	5.84	1.38	5.83	1.40	5.83	1.43
7 9	7 80	1.57	6.81	1.60	6.81 7.78	1.63	6.80 7.77	1.66
9	8.77	2.02	7-79 8.76	2.06	8 75	2.10	8.74	2.14
10	9.74	2.25	9.73	2.24	9.72	2.33	9:71	2.38
11	10.72	2.47	10.71	2.52	10.70	2-57	10.68	2.61
12 13	11.69	2.70	11.68	2.75 2.98	11.67	2.80 3.03	11.66	2.85 3.09
14	13.64	3.85	13.63	3.2T	13.61	3.27	13.60	3.33
25	14.62	3 37	14.60	3 44	14.59	3,0	14-57	3.57
1.6	15.59	3.60	45-57	3 67	15.56	3.74	15.54	3.80
17	16.56	3.82 4.05	16.55 17.52	3.90 4.13	16 53 17.50	8-97 4-20	16.51 17.48	4.04 4.28
19	18.51	4.27	18.49	4 35	18.48	4-44	18.46	4.52
20	19.49	4.50	19.47	4.58	19.45	4.67	19.43	4-75
21	20.46	4.72	10.44	4.81	20.42	4.90	20.40	4-99
23	21.44 22.41	4.95	21.41	5.04	11.39 12.36	5.14	21.37	5-43 5-47
34	23.38	5.40	23.36	5.50	23.34	5.60	23.31	5.70
25	24.36	5.62	24-33	5.73	24.31	5.84	24.28	5.94
26	25.33	5.85	25.31	5.96	25.28	607	25.25	6.18
27	26.33 27.28	6.07 6.30	26.28 27.25	6.39 6.42	26.25 27.23	6.30 6.54	26.23 27.20	6.66
29	18,26	6 58	28.23	6.65	28.20	6.77	28.17	6 8g
30	19.23	6.75	29.20	6.88	29.17	7.00	29.14	7.13
31	30.21	6.97	30.17	7.Ft	30.14	7.24	30.11	7-37
32	31.18	7.20	31.15	7 33 7.56	31.12	7 47	31.08	7.61
33 34	32.15	7.65	33.09	7.79	33.06	7.94	53.03	80.8
35	34.10	7.87	34-07	8.02	34.03	8.17	34.00	8.32
36	35.08	8.10	35.04	8.25	35.01	8.40	34-97	8.56
37 38	36.05 37.03	8.32 8.55	36.02 36.99	8.48 8.71	35.98 3 6.9 5	8.64 8.87	35.94 36.91	8.79 g.33
39	38.00	8.77	37.96	8.94	37-92	9.10	37.88	9.27
40	38.97	9.00	38.94	9.17	38.89	9.34	38.85	9.51
41	39.95	9.22	39.91	9.40	39.87	9.57	39.83	9.75
43	40.92	9.45	40.88 41.86	9.63 9.86	40.84	9.80 10.04	40.80 41.77	9.9 &
44	42.87	9.90	42.83	10.08	42 78	10.27	42.74	10.46
45	43.85	10.12	43.80	10.31	43.76	10.51	43.71	10 70
46	44 82	10 35	44.78	10.54	44.73	10.74	44.68	10.93
47	45.80	10.57	45.7 5 46 72	10.77	45.70	10.97	40.62	11.41
49	47.74	11.04	47.70	11.23	47.65	11.44	47.60	11.65
50	48.72	11.25	48.67	11.40	48.62	11.67		11.88
51	A	11.47	49.64 50.62	11.69 11.92	49-59	11.91	44.54 50.51	12.36
52 53	50.67	11.70	51.59	12.55	50.56 51.54	12.37	51 48	12.60
54	52.62	12.15	52.56	12.38	52.51	12.61	52.45	12.84
55	53.59	12.37	53.54	12.61	53.48	12.84	53.42	13.07
56	54.56	12.60		12.84	54-45	13.07	54.40	13.55
57 58	1 ///	13.05		13.29	55.43 56 4 6	13.31	55-37 56.34	13.79
59	57.49	13.37	57.43	13.52	57-37	113.77	57 31	14.02
60	.1 '	13.50		13.75	58.34	14.01	58.28	14.26
Dist	Dep	Lat.	Dep	Lat.	1)4 .	Lat	Dep.	Lat.
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I	Dist	Lat	Оср	Lut	Dep.	Lat.	Dep.	Let	Depar
Ţ	61	59 44	13.72	59.38	13 58	59.34	1424	59 25	1450
Į	62	60:41 61:39	13 95	60.95 61.38	14-31	61 26	14-71	60.13	44-74 44-97
t	64	62,36	14.40	61.30	14.67	62.23	14 94	62,17	15.21
J.	65	63.33	14.62	63.27	f4.40	68.20	15.27	63.44	45-45
ł	66	64.51	14.85	64.24	15.36	64.18	15.41 45.64	64.34 65.08	15.69
I	68	66.36	15.90	66.19	t 5-59	66.12	15.87	66 05	15 93 16.16
1	69	67.25	15-58	67.16	(5.8)	67.09	16.11	67.0a	16.40
ŀ	70	68.25	15-75	64.14	16.04	68.07	16.34	67-99	16.64
Į	71 73	69.18 70.44	15.97	69.11 70-08	16.47 16.50	70.01	16.57	68.97 69.94	16 88
I	73	71.43	16.42	71.06	16 73	7- 48	17.94	70.91	17-85
ı	24	78 10	16 65	76 03	16.96	7196	17 28	71.88	17-59
ł	75 76	73.08	16 87	73.00	17.19	72-93	17.51	73.85	18 06
1	77	74.05	17.10	73.98 74.95	17.48	73.90	17.74	73.82	18,30
1	78	76,00	17.55	75-92	17.88	75.84	18,81	75.76	18.54
ł	79 80	76.98	17 77	70.90	18.41 19 34	76.82	18 44 18.68	76.74	18,78
1	81	77-95	18.42	78.84	18.57	77.79	18.91	77-71	19.01
1	82	79.90	18.45	79-84	18.79	79 73	19.14	79.65	19.49
Ì	83	\$0.87	18.67	\$0.79	19 02	80.71	19.18	80.61	29.73
4	84	\$1.85 \$2.82	18.40	\$4.76 \$2.74	19.25 19.48	81.68	10.84	\$1.59 \$2.56	19.97
1	80	83.80	19-35	83.71	19/11	83.62	80.08	87-44	20.44
4	87	\$4.77	19.57	84.68	19.94	84.60	20.11	84.51	20.68
ı	88	85.74	19.80	85.66	20.17	85.67	20.54	85.48	20.92
Į	93	86.72 87.60	20.01	86.69 87.60	20.40 20.63	86,54 87 5 t	20.98	86.45 87.42	21.45
-1	91	88,67	20.47	B8.58	20.86	88.49	21.34	88.39	21,63
- 1	92	\$9.64	20.70	\$9.55	21.09	89.46	21.48	49.3 6	21.87
1	93	90.64	20.93 21.15	90.52	21.54	90.43	21.73	90,23	33.40 13.34
4	95_	98.57	21.37	91.47	21.77	92.38	22.18	91.38	22 58
-[96	93-54	21 60	32.44	22 00	93-35	22.41	93.25	22 82
4	98	94-51	21.81	94.42	22.63	94-13	22.64	94.53	23.06
4	99	95.49	22.05 11.37	95-39 96.36	21.40 21.69	95,29	23.11	95.19 95.19	23.29 23.53
1	100	97-44	22.50	97.34	32.92	97-24	13.34	97-13	23 77
- 1	101	98.41	32.72	98.31	23-45	98.21	23.58	98.11	34.01
	103	100.4	23.94	99.18	23 38 23.61	99.18	23.81 24.04	80.00	74.74 24.48
i	104	101.3	23.40	101 2	33.84	101-1	24 18	0.101	24.72
- 6	105	101.3	23.62	101.1	34-07	101.1	34-51	101.0	24.96
1	106	103-3	23.84	103.2	14 30	103.1	24.75	103.0	35.19
1	108	104.3	24.07 24.89	104-3	24.52 24.75	105.0	25.81	103 g 104.5	25.43 25.67
1	109	106.3	24.58	1,001	24.98	100.0	25-45	105.9	25.91
- 1	110	107.2	24-74	197.1	25 21	107.0	15 68	106 8	26.15
- 1	111	108,2	34.97 35.19	0.801	25.44	107.9	25.43 26.15	107 8	26.38 16 63
	£ 1 3	110-1	15.41	110.0	15 90	109 9	26 38	109 8	26.86
	114	rtt.t	15 64	111.0	26. t 3		26 61	110.7	27 10
- 1	116	112.1	25 87	611.0	26.36	111.8	26 85	111.7	27.33
4	117	113.0	26.09 26.32	113.9	26.59 26.83	112.8	127 0 8 127.31	113.7	27.57
ł	118	115.0	26.54	114-9	27.05	1147	27.59	114.6	28.05
ŀ	119	116.0	16.77 26.99	116.8	27 27	115.7	27.78 28.01	115.6	18 18
3		Dep.	Lat	Dep	Lat	Dep	126.01 Lud.	Dip	18 52 Lut.
1	Dist.		7	4 4			U/		-
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I D	1 0	,	15	?	30)'	4	,
Diet	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Liste	Dep.
I	0.97	0.24	0.97	0.25	0.97	0.25	0.97	9.25
1 2	1.94	0.48	1.94	0.49	1.94	0 50	1.93	0.51
3	2.91	0.73	2.91	0 74	2.90 3.87	1.00	2.90 3.87	0.76
1 4	3.88 4.85	0.97	3.88 4.85	0.98	4.84	1.25	4.84	1.27
5	5.82	1.45	5.82	1 48	5.81	1.50	5.80	1.53
7	6.79	1.69	6.78	1.72	6.78	1.75	6 77	1.78
8	7.76	1.94	7.75	1.97	7.75	2:00	7.74	2.04
9	8.73	2.18	8.72	2-22	8.71	2.25	8.70	2.29
10	9.70	2.42	9.69	2.46	9.68	2 50	9.67	2.55
11	10.67	2.66 2.90	10.66	2.71 2.95	10.65	2.75 3.00	10.64	3.06
12	1961	3.15	12.60	3.20	12.59	3.25	12.57	3.31
14	13.58	3.39	13.57	3.45	13.55	3.51	13.54	3.56
15	14.55	3.63	14.54	3.69	14.52	3.76	14.51	3.82
16	15.52	3.87	15.51	3.94	15.49	4.01	15.47	4-07
17	16.50	411	16.48 17.45	4.18 4-43	16 46 17.43	4.26 4.51	16.44	4-33 4-58
19	18.44	4.60	18 42	4.68	18.39	4.76	18.37	4 84
20	19.41	4.84	19.38	4.92	19.36	5.01	19.34	5.09
21	20.38	5.08	20.35	5-17	20.33	5.26	20.3 L	5-35
22	21.35	5.32	21 32	5.42	21.30	5 5	21.28	5.60
23	22 32	5.56 5.81	22.29	5 66	22.27 23.24	5.76 6.01	22.24	5.86 6.11
24 25	23.29 24.26	6.05	23.26 24.23	5.91 6.15	24 20	6 26	23.21 24.18	6.37
26	25.23	6 29	25 20	6 40	25.17	6.51	25.14	6.62
27	26.20	6 53	26.17	6.65	26.14	6.76	26.11	6.87
28	27.17	6.77	27.14	6.89	27.11	7.01	27.08	7-13
29	28.14	7.02	28.11	7 14	28.08	7.26	28.04	7.38 7.64
30	29.11	7.26	29.08	7.38	29.04	7.51	29.01	
31	30.08	7.50 7.74	30.05 31.02	7.63 7.88	30.98	7.76 8.01	29.98 30.95	7.89 8.15
32	31.05	7.98	31.98	8.12	31.95	8.26	31.91	8.40
34	32.99	8.23	32.95	8.37	32.93	8.51	32.88	8.66
35	33.96	8-47	33.92	8.62	33.89	8 76	33.85	8.91
36	34.93	8.71	34.89	8.86	34.85	9.01	34.81	9.17
37 38	35.90 36.87	8.93 9.19	35.86 36.83	9.11 9.35	35.82 36.79	9.26 9.51	35.78 36 .75	9.42 9.67
39	37.84	9.43	37.80	9.60	37-76	9.76	37.71	9.93
40	38.81	9.68	38.77	9.85	38.73	10.02	38.68	10.18
41	39.78	9 92	39.74	10.09	39.69	10.27	39.65	10.44
42	40.75	10.16	40.71	10,34	40.66	10 52	40.62	10.69
43	41.72	10.40	41.68	10.58	41.63	10.77	41 58	10.95
44	42.69 43.66	10.64	42 65	11.08	43.57	11.02	42.55 43.52	11.46
46	44.63	11.13	44.58	11.32	44.53	11.52	44 48	11.71
47	45.60	11.37	45.55	11.57	_	11.77	45.45	11.97
48	46.57	11.61	46.52	11.82	46 47	1202	46.42	12.22
49	47.54	11.85	47 49	12 06		12.27	47.39	12.48
50	48.51	12 10	48.46	12.31	48.41	12.52	48.35	12.73
51	49.49	12.34 12.58	49.43 50.40	12.55		12.77	49.32 50 2 9	12.98
53	50.46	12.82	51.37	13 05	51.31	13.27	51.25	13 49
54	52.40	13.06	52.34	13.29	52.28	13.52	52.22	13.75
55	53-37	13.31	53.31	13-54	53.25	3.77	53-19	14.00
56	54-34	13.55	54.28	13.78		14 02	54-15	14.26
57	55.31	13.79		14.03	55.18	14-27	55.12 56.09	14.51
58 59	56.28	14.03		14.28	57.12	14.52	57.06	15.02
60	58.20	14.52		14.77	58.09	15.02	58.02	15.28
1	Dep.	Lat.	Dep.	Lat	Dep	Lat.	Dep.	List.
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Dist.	Lat	Dep.	Lat.	Dep.	Lat.	D _i p.	Lat.	De
61 62	59.19 60.16	14.76	59.12 60.00	15.02	59 06 60.03	15.27	58.99 59.96	15.5
63	61.13	15.24	61.06	15.51	60.99	15 77	60.93	16.0
64	62.10	15.48	62:03	15.75	61.96	16.02	6189	16.2
65	63.07	15.72	63.00	16.25	62.93	16.53	$\frac{62.86}{63.83}$	16.8
67	65.01	15.97	64.94	16.49	64.87	16.78	64.79	17.0
68	65.98	16.45	65.91	16.74	65.83	17.03	65.76	. 17. 3
69 70	66.95 67.92	16.69 16 93	66.88 67 85	16.98	66.80 67.77	17.28	66.73 67.69	17.5
71	68.89	17.18	68.82	17.48	68.74	17.78	68.66	18.0
72	69.86	17.42	69.78	17.72	69.71	18.03	69.63	18.3
73 74	70.83	17.66	70.75	17.97 18.22	70.67 71.64	. 18.28 . 18.53	70.59 71 56	18.5
75	72-77	18.14	72.69	18.46	72.61	: 18.78	72-53	19.1
76	73.74	18.39	73.66	18.71	73.58	19.03	73 50	19.3
77 78	74.71 75.68	18.63 18.87	7.4.63 75.60	18.95 19.20	74·55 75·52	19.28	74.46 75.43	:19.6 :19.8
79	76.65	19.11	76.57	19.45	76.48	19.78	76.40	20.1
80	77.62	19.35	77-54	19.69	77.45	20.03	77.36	20.3
8 t 8 z	78.59 79.56	19.60	78.51 79 48	19.94 20 18	78.42 7 9 .39	20.28	78.33 79.30	120.8
83	80.53	20.08	80.45	20.43	80.36	20.78	80.26	21.1
84 85	81.50	20.32	81 42	20.68	81.32	21.03	81.23	21.3
86	82.48	20.56	82 38	20.92	82.29	21.28	83.17	21.6
87	84.42	21.05	84.32	21.42	84.23	21.78	84.13	22.1
88	85.39	21.29	85.29	21.66	85.20	22.03	85.10	22.4
89 90	86.36 87.33	21.53	86.26 87.23	21.91	86.17 87.13	22.28	86.07 87.03	22.6
91	88.30	22.01	88.20	22.40	88.10	22.78	88.00	23.1
92	89.27	12.26	89.17	22 65	89.07	23.04	88.97	23.4
93 94	90.24 91.21	22.50	90.13	22.89 23.14	90.04 91.01	23.29 23.54	89.94 90.90	23.t 23.g
95	92.18	22.98	92.08	23.38	91.97	23 79	91.87	24.1
96	93.15	23.22	93.05	23.63	92.94	24 04	92.84	24.4
97 9 8	94.12	23.47 23.71	94.02 94.98	23.88 24.12	93.91 94.88	24.29 24.54	93.80 94-77	24.7 24.9
99	96.06	23.95	95.95	24.37	95.85	24.79	95-74	25.2
100	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.4
101 102	98.20 98.97	24.43 24.68	97.89 9 8.86	24.86 25.11	97.78 98 75	25.29 25.54	97.67 98.64	25.7 25.9
103	99.94	24.92	99.83	25.35	99.72	25.79	99.61	26.2
104	100.9	25.16 25.40	100.8	25.60 25.85	100.7	26 04 26.29	100.6	26.4 26.7
106	102.9	25.64	102 7	26.09	102.6	26 54	102 5	26.c
107	103.8	25.89	103.7	26.34	103.6	26.79	103.5	27.2
109	1048	26.13 26.37	104.7	26 58 26.83	104.6	27.04 27.29	104.4 105.4	27.5
110	106.7	26.61	106.6	27.08	106.5	27.54	106.4	28.0
111	107.7	26.85	107.6	27.32	107.5	27.79	107.3	28.2
112	108.7	27.10 27.34	108.6	27.57 27.82	108.4	28.04 28.29	108.3	28.5
114	110.6	27.58	110.5	28.06	110.4	28.54	110.2	29.0
115	111.6	27 82	111.5	28.31	111.3	28.79	111.2	29.1
116	112.6	28.06 28.30	112.4	28.55 28.80	112.3	29.04	112.2	29.5
118	113.5	28.55	1144	29.05	113.3	29.29 29.54	114.1	29 ; 30.6
119	115.5	28.79	115.3	29.29	115.2	29.80	115.1	30.1
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43 41.53 11.13 41.49 12.31 41.44 11.49 41.39 11.67 44 42.50 11.39 42.45 11.57 42.40 11.76 42.35 11.94 45 43.47 11.65 43.42 17.84 43.36 12.03 43.31 12.21 46 44.43 11.91 44.38 12.10 44.33 12.29 44.27 12.49 47 45.40 12.16 45.35 12.36 45.29 12.56 45.24 12.76 48 46.36 12.42 46.31 12.63 46.25 12.83 46.20 13.03 49 47.38 18.68 47.27 12.89 47.22 13.09 47.16 13.39 50 48.30 12.94 48.24 13.15 48.18 13.36 48.12 13.57 51 49.26 13.20 49.20 13.41 49.15 13.63 49.09 13.84 52 50.23 13.46 50.17 13.68 50.11 13.90 50.05 14.11 53 51.19 13.72 51.13 13.94 51.07 14.16 51.01 14.39 54 52.16 13.98 52.10 14.20 52.04 14.43 51.97 14.66 55 53.13 14.24 53.06 14.47 53.00 14.70 52.94 14.93 56 54.09 14.49 54.03 14.73 53.96 14.97 53.90 15.20 57 55.06 14.75 54.99 14.99 54.93 15.23 54.86 15.47 58 56.02 15.01 55.96 15.26 55.89 15.50 55.82 15.74 59 57.99 15.27 56.92 15.52 56.85 15.77 56.78 16.02 60 57.96 15.53 57.89 15.78 16.03 57.75 16.29 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat.	41	39.60	1061	39.56	10.78	39-51	10.96	39.46	11.13
44 42.50 11.39 42.45 11.57 42.40 11.76 42.35 11.94 45 43.47 11.65 43.42 17.84 43.36 12.03 43.31 12.21 46 44.43 11.91 44.38 12.10 44.33 12.29 44.27 12.49 47 45.40 12.16 45.35 12.36 45.29 12.56 45.24 12.76 48 46.36 12.42 46.31 12.63 46.25 12.83 46.20 13.03 49 47.35 12.68 47.27 12.89 47.22 13.09 47.16 13.30 50 48.30 12.94 48.24 13.15 48.18 13.36 48.12 13.57 51 49.26 13.20 49.20 13.41 49.15 13.63 49.09 13.84 52 50.23 13.46 50.17 13.68 50.11 13.90 50.05 12.11 53 51.19 13.72 51.13 13.94 51.07 14.16 51.01 14.39 54 52.16 13.98 52.10 14.20 52.04 14.43 51.97 14.66 55 53.13 14.24 53.06 14.47 52.04 14.43 51.97 14.66 55 55.06 14.75 54.99 14.99 54.93 15.23 54.86 15.47 58 56.02 15.01 55.96 15.26 55.89 15.50 55.82 15.74 59 57.99 15.27 56.92 15.52 56.85 15.77 56.78 16.02 57 57.96 15.53 57.89 15.78 57.82 16.03 57.75 16.29 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat.		_	-		_				
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47 45.40 12.16 45.35 12.36 45.29 12.56 45.24 12.76 48 46.36 12.42 46.31 12.63 46.25 12.83 46.20 13.03 49 47.35 18.68 47.27 12.89 47.22 13.09 47.16 13.30 50 48.30 12.94 48.24 13.15 48.18 13.36 48.12 13.57 51 49.26 13.20 49.20 13.41 49.15 13.63 49.09 13.84 52 50.23 13.46 50.17 13.68 50.11 13.90 50.05 14.11 53 51.19 13.72 51.13 13.94 51.07 14.16 51.01 14.39 54 52.16 13.98 52.10 14.20 52.04 14.43 51.97 14.66 55 53.13 14.24 53.06 14.47 53.00 14.70 52.94 14.93 56 54.09 14.49 54.03 14.73 53.96 14.97 53.90 15.20 57 55.06 14.75 54.99 14.99 54.93 15.23 54.86 15.47 58 56.02 15.01 55.96 15.26 55.89 15.50 55.82 15.74 59 57.99 15.27 56.92 15.52 56.85 15.77 56.78 16.02 60 57.96 15.53 57.89 15.78 57.82 16.03 57.75 16.29 10ep. Lat. Dep. Lat. Dep. Lat. Dep. Lat.									
48 46.36 12.42 46.31 12.63 46.25 12.83 46.20 13.03 47.16 13.30 50 48.30 12.94 48.24 13.15 48.18 13.36 48.12 13.57 13.46 50.17 13.68 50.11 13.90 50.05 14.18 53 51.19 13.72 51.13 13.94 51.07 14.16 51.01 14.39 54 52.16 13.98 52.10 14.20 52.04 14.43 51.97 14.66 55 53.13 14.24 53.06 14.47 53.00 14.70 52.94 14.93 55 55.06 14.75 54.99 14.99 54.93 15.23 54.86 15.47 55 57.96 15.27 56.92 15.26 56.85 15.77 56.78 16.02 16.29 10.57					_		-		
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51 49.26 13.20 49.20 13.41 49.15 13.63 49.09 13.84 52 50.23 13.46 50.17 13.68 50.11 13.90 50.05 14.11 53 51.19 13.72 51.13 13.94 51.07 14.16 51.01 14.39 54 52.16 13.98 52.10 14.20 52.04 14.43 51.97 14.66 55 53.13 14.24 53.06 14.47 53.00 14.70 52.94 14.93 56 54.09 14.49 54.03 14.73 53.96 14.97 53.90 15.20 57 55.06 14.75 54.99 14.99 54.93 15.23 54.86 15.47 58 56.02 15.01 55.96 15.26 55.89 15.50 55.82 15.74 59 57.99 15.53 57.89 15.78 57.82 16.03 57.75 16.29 50 57.96 15.53 57.89 15.78 16.03 57.75 16.29 <		_		_					
52 50.23 13.46 50.17 13.68 50.11 13.90 50.05 14.18 53 51.19 13.72 51.13 13.94 51.07 14.16 51.01 14.39 54 52.16 13.98 52.10 14.20 52.04 14.43 51.97 14.66 55 53.13 14.24 53.06 14.47 53.00 14.70 52.94 14.93 56 54.09 14.49 54.03 14.73 53.96 14.97 53.90 15.20 57 55.06 14.75 54.99 14.99 54.93 15.23 54.86 15.47 58 56.02 15.01 55.96 15.26 55.89 15.50 55.82 15.74 59 57.99 15.27 56.92 15.78 57.82 16.03 57.75 16.02 60 57.96 15.53 57.89 15.78 57.82 16.03 57.75 16.29 10 10 15 15 15 15 15 15 15 <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td>-</td> <td></td> <td></td>						-	-		
53 51.19 13.72 51.13 13 94 51.07 14.16 51.01 14.39 54 52.16 13.98 52.10 14.20 52.04 14.43 51.97 14.66 55 53.13 14.24 53.06 14.47 53.00 14.70 52.94 14.93 56 54.09 14.49 54.03 14.73 53.96 14.97 53.90 15.20 57 55.06 14.75 54.99 14.99 54.93 15.23 54.86 15.47 58 56.02 15.01 55.96 15.26 55.89 15.50 55.82 15.74 59 57.99 15.27 56.92 15.52 56.85 15.77 56.78 16.02 60 57.96 15.53 57.89 15.78 57.82 16.03 57.75 16.29 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat.				-			, ,		
54 52.16 13.98 52.10 14.20 52.04 14.43 51.97 14.66 55 53.13 14.24 53.06 14.47 53.00 14.70 52.94 14.93 56 54.09 14.49 54.03 14.73 53.96 14.97 53.90 15.20 57 55.06 14.75 54.99 14.99 54.93 15.23 54.86 15.47 58 56.02 15.01 55.96 15.26 55.89 15.50 55.82 15.74 59 57.99 15.27 56.92 15.52 56.85 15.77 56.78 16.02 60 57.96 15.53 57.89 15.78 57.82 16.03 57.75 16.29 10 </td <td></td> <td>-</td> <td></td> <td></td> <td></td> <td>_</td> <td>_</td> <td></td> <td></td>		-				_	_		
55 53.13 14.24 53.06 14.47 53.00 14.70 52.94 14.93 56 54.09 14.49 54.03 14.73 53.96 14.97 53.90 15.20 57 55.06 14.75 54.99 14.99 54.93 15.23 54.86 15.47 58 56.02 15.01 55.96 15.26 55.89 15.50 55.82 15.74 59 57.99 15.27 56.92 15.52 56.85 15.77 56.78 16.02 60 57.96 15.53 57.89 15.78 57.82 16.03 57.75 16.29 15 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat.	-							_	
56 54.09 14.49 54.03 14.73 53.96 14.97 53.90 15.20 57 55.06 14.75 54.99 14.99 54.93 15.23 54.86 15.47 58 56.02 15.01 55.96 15.26 55.89 15.50 55.82 15.74 59 57.99 15.27 56.92 15.52 56.85 15.77 56.78 16.02 60 57.96 15.53 57.89 15.78 57.82 16.03 57.75 16.29 50 15.26 15.78 15.78 15.78 16.03 16.29 15 15 15 15 15 16.29 15 15 15 15 15 15 15 15					_			52.94	
57 55.06 14.75 54.99 14.99 54.93 15.23 54.86 15.47 15.88 56.02 15.01 55.96 15.26 55.89 15.50 55.82 15.74 16.02 16.02 15.53 57.96 15.53 57.89 15.78 57.82 16.03 57.75 16.29 16.29 16.02 16.29 16.02 16.29 16.02 16.29 16.02 16.29 16.			14.49	54 03	14-73	53.96	14.97		l .
59 57.99 15.27 56.92 15.52 56.85 15.77 56.78 16.02 15.53 57.89 15.78 57.82 16.03 57.75 16.29 19.00	57					54-93		54.86	
15.53 57.89 15.78 57.82 16.03 57.75 16.29 16.2			_		_				
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Dist	0		1:	51	3	01	4	57
57	Lat.	Drp.	Lat	Drp	Lat	Dep.	Lat.	
61 62	58.92	15 79	58.85	16.04	58 78	16.30	58.71	1
63	59.89 60.85	16.05 16.31	59.82 60.78	16.31 ' 16.57	59.75 60.71	16.57	59.67 60.63	: I
64	61.82	16.56	61.75	16.83	61.67	17 10	61.60	ļ
65	62.79	16.82	62.71	17.10	62.64	17.37	62.56	
66 67	63 75 64.72	17.08	63.68 64.6 4	17.36 17. 62	63.60 64.56	17.64 17.91	63.52 64.48	. I
68	65.68	17.60	65.61	17.89	65.53	18.17	65.45	1
69 70	66.65 67.61	17.8 6 18.12	66.59 67.54	18.15	66.49 67 45	18.44	66.41	, 1
71	68.58	18.38	68.50	18.68	68 42	18.97	68 33	-
72	69 55	18.64	69.46	18.94	69.38	19.24	69.30	13
73	70.51	18.89	70.43	19.20	70.35	19.51	70.26	1
74 . 75	71.48	19.15	71.39	19.46 19.73	71-31	19.78 20.04	71.22	2
76	73.41	19.67	73.32	19.99	73.24	20 31	73 15	2
77	74.38	19.93	74.29	20.25	74.20	20.58	74.11	2
78 79	75.34 76.31	20.45	75.25 76.22	20 52 20.78	75.16 76.13	20.84 21.11	75.07 75.03	2 2
80	77.27	20.71	77.18	21 04	77.09	21.38	77.00	2
18	78.24	20.96	78.45	21.31	78.05	21.65	77 46	2
82 83	79.21	21.22 21.48	79-11	21.57	79.02 79 98	21.91 22.18	78.92 79.88	2 2
64	81.14	21.74	81.04	22.09	8095	22 45	80 85	2
85	82.10	22.90	82.01	22.36	81.91	22.72	81.81	2
86 87	83.07 84.04	22.26 22.52	82.97	22.62 22.88	82.87 83.84	22.·)8 23.25	82 77 83.73	2
88	85.00	22.78	83.94 84.90	23.15	84.80	23.52	84.70	2
89	85.97	23.03	85.87	23.41	85,76	23.78	85.66	2
90	86.93	23.29	86.83	23.67	86 73	24.05	86.62	2
91	87.90 88.87	23.55 23.81	87.80 88.76	23.94 24.20	87.69 88.65	24.32 24.59	87.58 88.55	2 2
93	89.83	24-07	89.73	24.46	89.62	24.85	89.51	2
94 95	90.80	24.33 24.59	90.69 91.65	24.72 24 99	90.58 91.54	25.12 25.39	90.47	2 2
96	92.73	24.85	92.62	25.25	92.51	25.65	92 40	2
97	93.69	25.11	93.58	25 51	93 47	25.92	93.36	2
98 99	94-66 95-63	25.36	94.55	25.78 26.04	94 44	26.19 26.46	94 34 95.28	2 2
100	96 59	23.88	95.51 96.48	26.30	95.40 96.36	26.72	96.25	2
101	97-56	26.14	97 44	26.57	97-33	26.99	97.21	2
102	98.52	26.40	98.41	26.83	98.29	27.26	98.17	2 2
104	99.49	26.66 26.92	99-37	27.09 27.36	99 25 100.2	27.53	99.13	2
105	101.4	27.18	101.3	27.62	101.2	28.06	101.1	2
106	102.4	27.43	102.3	27.88	102.1	28.33	102.0	2
107	103.4	27.69 27.95	103.2	28.14 28.4.ſ	103.1	28.59 28.86	103.0	2 2
109	105-3	28.21	105.2	28.67	105.0	29.13	104.9	2
110	106.3	28 47	106.1	28.93	106.0	29.40	105.9	2
1112	107.2	28.73 28.99	107.1	29.20 29.46	107.0	29.66 29.93	106.8	3
413	109.1	29.25	109.0	29.72	108.9	30.20	108.8	3
214	1.011	29.51	110.0	29.99	109.9	30.47	109.7	3
115	1120	29.76 30 02	111.0	30.25	111.8	30 73	110.7	3
117	113.0	30.28	112.9	30.77	112.7	31.27	112.6	3
1118	114.0	30.54	113.8	31.04	113.7	31.53	113.6	3
119	115.9	30.80	114.8	31.30 31.56	114.7	31.80	114.5	3
1	Dep.	int.	Dep.	Lat.	Dep.	Lut.	Dep.	1=
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1		ان	•	1.5	51	30	1	45	, , ,		
	Dist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep	Lat.	Dep.		
1-]	0.96	0.28	0.96	0.28	0.96	0.28	0.96	0.29		
	2	1.92	0.55	1.92	0.56	1.92	0.57	1,92	0.58		
Ĭ	3	2.88	0.83	2.88	0 84	2.88	0.85	2.87	0.86		
ļ	4	3.85	1.10	3.84 4 00	1.12	3.84	1.14	3.83	1.15 1.44		
-	5	4.81	1.38		1.40	4.79	1.42	4.79			
1	6	5.77 6.73	1.65	5.76 6.72	1.68 1.96	5.75 6.71	1.70 1.99	5.75 6.70	1.73 2.02		
1	7 8	7.69	2.21	7.68	2.24	7.67	2.27	7.66	2.31		
1	9	8.65	2.48	8.64	2.52	8.63	2.56	8.62	2.59		
1_1	10	9.61	2.76	9.60	2.80	9.59	2.84	9.58	2.88		
•	11	10.57	3.03	10.56	3.08	10.55	3.12	10.53	3.17		
	12	11.54	3.31 3.58	11.52	3.36 3. 6 4	11.51	3 41 3.69	11.49	3.46 3.75		
•	13	12.50 13.46	3.86	13.44	3.92	13.42	3.98	13.41	4.03		
	15	14.42	4-13	14.40	4.20	14.38	4.26	14.36	4.32		
1	16	15.38	4.41	15.36	4.48	15.34	4.54	15.32	4-61		
•	7	16 34	4.69	16.32	4.76	16.30	4.83	16 28	4.90		
1	18	17.30	4.96	17.28	5.04	17.26 18.22	5.11	17.24	5.19 5.48		
	19	18.26 19.23	5.24 5.51	18.24 19 20	5.32 5.60	19.18	5.40 5.68	19.15	5.76		
				20.16	5.88	20.14		20.11	6.05		
1	22	20.19	5.79 6.0 6	21.12	6.16	21.09	5.96 6.25	21.07	6.34		
	23	22.11	6.34	22.08	6 44	22.05	6.53	22.02	6.63		
	24	23.07	6.62	23.04	6. 🖜	23.01	6.82	22.98	6.92		
{- -	25	24.03	6.89	24 00	7.00	23.97	7.10	23.94	7.20		
	26	24.99	7.17	24 .96	7.28	24.93	7.38	24.90	7.49		
4	27	25.95	7.44	25.92 26.88	7.56 7.84	25.89 26.85	7.67	25.85 26.81	7.78 8.07		
1	29	26.92 27.88	7.72 7.99	27.84	8.12	27.81	7·95 8·24	27.77	8-36		
	30	28.84	8.27	28.80	8.39	28.76	8.52	28 73	8.65		
1-	3 1	29.80	8.54	29.76	8.67	29.72	8.80	29.68	8.93		
	32	30.76	8.82	30.72	8.95	30.68	9.09	30.64	9.22		
_	33	31.72	9.10	31.68	9.23	31.64	9.37	31.60	9.51		
	34	32.68	9.37	32.64	9.51	32.60	9.66	32 56	9.80 10.09		
-	35	33 64	9 65	33.60	9.79	33 56	9.94	33.52	10.38		
•	36 37	34.61 35-57	9. 92 10.20	34.56 35.52	10.07	34.52 35.48	10.22	34·47 35·43	10.66		
	8	36.53	10.47	36.48	10.63	36.44	10.79	36.39	10.95		
	39	37-49	10.75	37.44	10.91	37.39	11.08	37-35	11.24		
14	10	38.45	1103	38.40	11.19.	38.35	11.36*	38.30	11.53		
	† 1	39.41	11.30	39.36	11.47	39.31	11.64	39.26	11.82		
4	12	40.37	11.58	40.32	11.75	49-27	11.93	40.22	12.10 12.39		
•	13 14	41.33	11.85	41.28 42.24	12.03	41.23	12.21	41.18	12.68		
	15	42.30 43.26	12.40	43.20	12.59	43.15	12.50	43.09	12.97		
1-	16	44.22	12.68	44.16	12.87	44.11	13.06	44.05	13.26		
4	17	45.18	12.96	45.12	13.15	45.06	13.35	45.01	13.55		
4	18	46.14	13.23	46.08	13.43	46.02	13.63	45.96	13.83		
4	19	47.10	13.51	47.04	13.71	46.98	13.92	46.92	14.12		
1-	0	48 06	13.78	48 00	13.99	47 94	14.20	47.88	14-41		
	2	49.02	14.06	48.96	14.27	48.90	14.48	48.84	14.70 14.99		
•	3	49.99 50.95	14.33 14.61	49.92 50.88	14.55 14.83	49.86 50.82	14·77 15.05	49·79 50.75	15.27		
	4	51.91	14.88		15.11	51.78	15.34	51.71	15.56		
5	5 5	52 87	15.16	54.80	15 39	52.74	15.62	52.67	15.85		
	56	53.83	15.44	53.76	15.67	53.69	15.90	53.62	16.14		
5	57	54.79	15.71	54.72	15.95	54.65	16 19	54 58	16.43		
•	8	55.75	15.99	55.68	16.23	55.61	16.47	55.54	16.72 17.00		
	9	56.71 57.68	16.26 16.54	56.64 57.60	16.51 16.79	56.57 57-53	16.76 17.04	56.50 57.45	17.29		
}	 ¦	Dep	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Lat.		
	Utst.						······································				
ئرا		U	0/		چىمىنىيە مىدىدىن ئىرىنىيىلىن بىرىنى بىرىنى بىرىنى بىرىنى بىرىنى بىرىنى بىرىنى بىرىنى بىرىنى بىرىنى بىرىنى بىرى		30/		15/		
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	15)′	1 1.	51	30)'	4	5'
	Dist.	Lat	Dep	Lat.	Dep.	Lat.	Dep.	Lat	Dep.
	61	58.64	16.81	58.56	17.07	58.49	17.32	58.41	17.58
	62	50.60	17.09	59.52	17.35	59.45	17.61	59-37	17.87
	63 64	61.52	17.37	60.48	17.63 17.91	60.41 61.36	17.89	60.33 61.28	18.16 18.44
	65	62 48	17.92	62.40	18.19	62.32	18.46	62.24	18.73
	66	63.44	18.19	63.36	18.47	63.28	18.75	63.20	19.02
•	67	64.40	18.47	64.32	18.75	64.24	19.03	64.16	19.31
	68 69	65.37 66.33	18.74	65.28	19.03 19 31	65.20 66.16	19.31	65.11 66.07	19.60
	70	67.29	19.29	67.20	19.59	67 12	19.88	67.03	20.17
	71	68.25	19.57	68.16	19.87	68.08	20.17	67.99	20.46
	72	69.21	1985	69.12	20 15	69.04	20.45	68.95	20 73
	73 74	70.17	20.12	70.08 71.04	20.43 20.71	69.99 70.95	20.73	69.90 70.86	21.04
	75	72.09	20 67	72.00	20.99	71.91	21.30	71.82	21.61
	76	73.06	20.95	72.96	21.27	72.87	21.59	72.78	21.90
	77	74 02	31 22	73.92	21.55	73.83	21.87	73-73	22.19
	78 79	74.98 75.94	21 50	74.88 75 84	21.83	74-79 75-75	22.15	74-69 75.65	22.48 22.77
	80	76.90	22-05	76.80	22.39	76.71	22.72	76.61	23.06
	81	77.86	22.33	77.76	22 67	77.66	23.01	77-56	23.34
	82	78.82	22.60	78.72	22.95	78 62	23.29	78.52	23.63
	83 84	79.78 80.75	22.88 23.15	79.68 80.64	23.23 23.51	79.58 80.54	23.57 23.86	79.48 80.44	23.92 24.21
	85	81.71	23.43	81.60	23.79	81.50		81.39	24.50
	86	82.67	23.70	82.56	24.07	82.46	24.43	82.35	24.78
	87	83.63	23.98	83 52	24.35	83.42	24.71	83.31	25.07
	88 89	84 59 85.55	24.26	84.48 85.44	24.63 24.90	84.38 85.34	24.99 25.28	84.27 85.22	25.36 25.65
	90	86.51	24.81	86.40	25.18	86.29	25.56	86.18	25.94
	91	87.47	25.08	87.36	25.46	87-25	25.85	87 14	26.23
	92	88.44	25.36	88.32	25.74	88.21	26.13 26.41	88.10	26.51
	93 94	89.40 90 36	25.63 25.91	89.28 90.24	26.30	89.17 90.13	26.70	90.01	26 80 27.09
	95	91.32	26.19	91.20	26.58	91.09	26.98	90.97	27.38
	96	92-28	26.46	92.16	26.86	92.05	27.27	91.93	27 67
	97 98	93.24 94 20	26.74 27.01	93.12 94.08	27.14 27.42	93.96	27.55 27.83	92.88 93.84	27.96 28.24
	99	95.16	27.29	95.04	27.70	64.92	28.12	94 80	28.53
	100	96.13	27.56	96.01	27.98	95.88	28.40	95.76	28.82
	101	97 09	27.84	90.97	28.26	96.84	28.09	96.71	29.11
	102	98.05 99.01	28.12 28.39	97 93 98.89	28.54 28.82	97.80 98.76	28.97 29.25	97.67 98.63	29.40 29.68
	104	99-97	28.67	99.85	29.10	99 72	29.54	99.59	29.97
	105	100.9	28.94	100.8	29.38	100.7	29 82	100.5	30.26
	106	101.9	29.22	101.8	29.66	101.6	30.11	101.5	30.55
	108	102.9 103.8	29.49	102.7	29.94 30.22	102.6 103.6	30.39 30.67	102.4	30.84
	109	104 2	30.04	104.6	30.50	104.5	30.96	104.4	31.41
	110		30.32	105 6	30.78	105 5	31.24	105.3	31.70
	111		30.60 30.87	106.6	31.06 31.34	106 4	31.53	106.3	31.99 32 28
	113	108.6	31.15	108.5	31.62	108.3	32.09	108.2	32.57
	114	109.6	31.42	109.4	31.90	109.3	32.38	109.2	32.85
	115		31.70	110.4	32.18	110.3	32.66	110.1	33.14
	116	•	31.97		32.46	111.2	32.95	111.1	33.43
	118	_	32.53	112.3	32.74 32.02		33.23 33.61	112.0	33.72 34.01
	1119	114.4	32.80	114.2	33 30	114.1	33.80	114.0	34.30
	120	115.4	33.08	115.2		115.1	34.08	1149	34.58
	Dist.	$\frac{\mathbf{D}_{c}\mathbf{p}}{\mathbf{D}_{c}}$	Lat.	Dep.	Lat.	Dep.	Lat	Dep.	Lat.
	12	0		4.		3() [.]	1	51
			•	73	DEGR	EES.			

101	0/		1:	5/	اد ا)/	4	51
Di at	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
	0.96	0.29	0.96	0.30	0.95	0.30	0.95	0.30
2	1.91 2.87	0.58 0.88	1.91 2.87	0.59	1.91 2.86	0.60	1.90 2.86	0.61
3 4	3.83	1.17	3.82	1.19	3.81	1.20	3.81	1.22
5	4.78	1.46	4.78	1.48	4-77	1 50	4.76	1.52
6	5.74 6.69	1.75 2.05	5.73 6.69	1.78	5.72	1.80	6.67	1.83
7	7.65	2.34	7.64	2-37	7.63	2.41	7.62	2.44
· 9	8 6 1 9-5 6	2.63 2.92	8 60 9·55	2.67	8.58 9.54	3.71 3.01	8.57 9.52	2.74 3.05
11	10.52	3.22	10.51	3.26	10.49	3.31	10.48	3.35
12	11.48	3.51	11.46	3.56	11.44	3.61	11.43	3.66
13 14	12.43	3.80 4.09	12.42	3.86	12.40	3.91 4.21	13.33	3.96 4.27
15	14-34	4-39	14.33	445	14-31	4.51	14.29	4-57
16	15.30	4.68	15.28	4-74	15.26	4.81	15.24	4.88
17	16.26	4-97 5. 26	16.24 17.19	5.34	16.21	5.11 5.41	16.19	5.18 5.49
19	18.17	5.56	18 45	5.63	18.12	5.71	18.10	5.79
20	19.13	5.85	19.10	5.93	19.07	6.01	19.05	6 10
21 22	20.08 21.04	6.14 6.43	20.06	6.23	20.98	6.31 6.62	20.95	6.40
23	22.00	6.72	21.97	6.82	21.94	6.92	21.91	7.01
24	22.95	7 02	23.92 23.88	7.12	22 89 23.84	7 22 7.52	22.86 23.81	7.32 7.62
25	2486	7.60	24.83	7.71	24.80	7.82	24.76	7.93
27	2582	7.89	25.79	8.01	25.75	8.12	25.71	8.23
28	26.78	8.19	26.74	8.30 8.60	26.70 27.66	8.42 8.72	26.67 27.62	8.54 8.84
29 30	27.73 28.69	8.48 8.77	28.65	8.90	28.61	9.03	28.57	9.25
31	29.65	9.06	29.61	9.19	29.57	9.32	29.52	9.45
32	30.60	9.36	30 56 31.52	9.49	30.52 31.47	9.62 9.92	30.48 31.43	9.76 10.06
33 34	31.56 32.51	9.65 9.94	32-47	10.08	32 43	10.22	32.38	10.37
35	33-47	10.23	33.43	10.38	33.38	10.52	33.33	10.67
36	34-43 35-38	10.53	34.38 35.34	10.68 10.97	34-33 35.29	10 83	34.29 35.24	10.98
37 38	36.34	11.11	36.29	11.27	36.24	11.43	36.19	11.58
39	37.30	11.40	37.25 38 20	11.57	37-20 38.15	11.73	37-14 38.10	11.89
40	38.25	11.69	39.16	12.16	39.10	12.33	39.05	12.19
42	40.16	12.28	40.11	12 45	40.06	12 63	40.00	12.80
43	41.12	12 57	41.07	12.75	41.01	12.93	40.95	13.11
44 45	42.08 43.03	12.86	42.98	13.05 13.34	41.96 42.92	13.23 13.53	41.91	13.72
46	43.99	13.45	43.93	13.64	43.87	13.83	43.81	14.02
47 48	44.95	13.74 14.03	44.89 45.84	13.94 14.23	44.82 45.78	14-13 14-43	44.76 45.72	14.33 14.63
49	45.90	14.33	46.80	14.53	46.73	14.73	46.67	14.94
50	47.82	14 62	47-75	14.83	47-69	15.04	47.62	15.24
51 52	48.77 49.73	14.91 15.20	48.71 49.66	15.12 15.42	48.64 49.59	15.34 15.64	48.57 49.52	15.55
53	50 68	15.50	50.62	15.72	50.55	15.94	50.48	16.16
54	51.64	15.79 16.08		16.31	51.50	16 24	51.43 52.38	16.46 16.77
55	52.60	16.37	-	16.61	52.45	16.54	53-33	17.07
57	54-51	16.67	54-44	16 90	54.36	17.14	54-29	17.38
58	55.47	16.96	55 39 56.35	17.20	55 32 56.27	17.44	55.24	17.68 17.99
59 60	56.42 57.38	17.25	57.30	17.50	57.22	17.74	57.14	18.29
نيد	Dep	Lut.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.
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1 9.1	0'		15'		30,		451	
Dist	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
61	58.33	17.83	58.26	18.09	58.18	18 34	58.10	18.60
62 63	59.29 60.25	18.13 18.42	59.21 60.17	18.39 18 68	59.13 60.08	18.64 18.94	59.05 60.00	18.90 19.21
64	61.20	18.71	61.12	18.98	61.04	19.25	60 95	19.51
65	62,16	19.00	62.08	19.28	61.99	19.55	61.91	19.82
66	63.12	19.30	63.03	19-57	62.95	19.85	62.86	20.12
67	64.07 65.03	19.59 19.88	63.99 64.94	19.87 20.16	63.90 64.85	20.15 20.45	63.81 64.76	20.43 20.73
69	65.99	20.17	65.90	20.46	65.81	20.75	65.72	21.04
70	66.94	20 47	66.85	20.76	66.76	21.05	66.67	21.34
71	67.90	20.76	67.81	21.05	67.71	21.35	67.62	21.65
72 73	68.85 69 81	21.05	68.76 69.72	21.35 21.65	68.67 69.62	21.65 21.95	68.57 69. 52	21.95 22.26
74	70.77	21.64	70.67	21.94	70.58	22.25	70.48	22.56
75	71.72	21.93	71.63	22.24	71.53	22.55	7:1.43	22 86
76	72 68	22.22	72 58	22.54 22.83	72.48	22.85	72.38	23.17
77	73.64 74.59	22.51 22.81	73·54 74·49	23.13	73-44 74-39	23.15 23.46	73·33 74·29	23.47 23.78
79	75.55	23.1Q	75.45	23.43	75.34	23.76	75.24	24.08
80	76.50	23.39	76.40	23.72	76.30	24.06	76.19	24.39
81 82	77.46	23.68	77.36 78.31	24.02	77.25	24. 36 24. 66	77.14	24.69 25.00
83	78.42 79·37	23.97 24.27	79.27	24.32 24.61	79.20	24.96	79.05	25.30
84	80.33	24.56	80.22	24.91	11.08	25.26	80.00	25.61
85	81.29	24.85	81.18	25.21	81.07	25.56	80.95	25.91
86	82.24 83 20	25.14	82.1 <u>3</u> 83.09	25.50 25.80	82.02 82.97	25.86 26.16	81.91 82.86	26.22 26.52
88	84.15	25.44 25.73	84.04	26.10	83 93	26.46	83-81	26.83
89	85.11	26.02	85.00	26.39	84.88	26.76	84.76	27.13
90	86.07	26.31	85.95	26.69	85.83	27.06	85.72	27.44
9 ¹	87.02 87.98	26.61 26.90	86.91 87.86	26:99 27.28	8 6. 79	27.36 27.66	86.67 87.62	27.74 28.05
93	88.94	27.19	88.82	27 58	88.70	27.97	88.57	28.35
94	89.89	27.48	89.77	27.87	89.65	28.27	89.53	28.66
95	90.85	27.78	90.73	28.17	90.60	28.57	90.48	28.96
96 97	91.81 92. 76	28.07 28.36	91.68 92.64	28.47 28.76	91.56 92.51	29.17	91.43 92.38	29.27 29.57
98	93.72	28.65	93.59	29.06	93.46	29-47	93.33	29.88
99	94.67	28.94	94-55	29.36 29.65	94.42	39.77 30.07	94.29	30.18 30.49
101	95.63	29.24	95.50	29.95	95.37	30.37	95.24	30.79
102	97.54	29.53 29.82	96.46 97.41	29.93 30.25	97.28	30.67	97.14	31.10
103	98.50	30.11	98.37	30.54	98.23	30.97	98.10	31.40
104	99.46 100.4	30.41	99.32	30.84 31.14	1.001	31.27	99.05	31.71 32.01
106	101.4	30.70	101.2	31 43	101.1	31.87	101.0	32.32
107	102.3	30.99 31.28	102.2	31.73	102.0	32.18	101.9	32.62
108	103.3	31.58	103.1	32.03	103.0	32.48	102.9	32.93
110	104.2	31.87 32 16	104-1	32.32 33.62	104.0	32.78 33.08	103.8	33.23 33.54
111	106.1	32.45	106.0	32.92	105.9	33.38	105.7	33.84
112	107.1	32.73	107.0	33.21	106.8	33.68	106.7	34.14
113	108.1	33.04	107.9	33.51 33.81	107.8	33.98 34.28	107 6	34·45 34·75
115	110.0	33·33 33.62	108.9 109.8	34.10	108.7	34.58	109.5	35.06
416	110.9	33.92	110.8	34-40	110.6	34.88	110.5	35.36
117	111.9	34.21	111.7	34.70	111.6	35.18	111.4	35.67
119	112.8	34.50	113.7	34-99 35.29	112.5	35.48 35.78	112.4	35.97 36.28
120	114.8	34-79 35.08	114.6	35.59	114.4	36.08	114.3	36 58
ند	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
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D.	0'		· 15	′	30)′	45	
Dist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.95	0.31	0.93	0.31	0.95	0.32	0.95	0.32
3	1 90	0.02	1.90	0.94	1.90 2.85	0.95	1.89 2.84	0.64 0.96
4	3.80	1.24	3.80	1.25	3.79	1.27	3-79	1.29
5	4.76	1.85	4-75	1.88	<u>4.74</u> 5.69	1.59	4.73 5.68	1.61
6	5.71 6.66	2.15	5.70 6.65	2.19	6.64	2.22	6 63	1.93 2.25
8	7.6 r	2.47	7.60	2.51 2.82	7.59	2 54 2.86	7.58	2.57
10	8.56 9.51	2.78 3.09	8.55 9.50	3.13	8.53 9.48	3.17	8.52 9.47	2.89 3.21
11	10.46	3.40	10.45	3.44	10.43	3 49	10.42	3.54
12	11.41	371	11.40	3.76 4.07	11.38	3.81 4.13	11.36	3.86 4.18
13	12.36	4.02 4.33	12.35 13.30	4.38,	13.28	4.44	13.26	4.50
15	14.27	4.64	14.25	4.70	14.22	4.76	14.20	4.82
16	15 22	4.94	15.20	5.01	15.17	5.08	15.15	5.14
17	16.17	5 2 5 5.56	16.14 17.09	5.32 5.64	16 12 17 07	5 39 5.71	16.10	5.46 5.79
19	18.07	5.87	18 04	5.95	18.02	6.03	17.99	6.11
20	19.02	6.18	18.99	6.26	18.97	6.66	18.94	6.43
21 22	19.97 20.92	6.80	19 94 20.89	6.58 6.89	19 9 I 20.86	6.98	19.89 20.83	6.75 7.07
23	21 87	7.11	21 84	7.20	2181	7.30	21.78	7-39
24	22 83	7.42 7.73	22. 79 23. 74	7.52 7.83	22.76 23.71	7.62 7.93	22 73 23.67	7.71 8.04
25 26	23.78	8.03	24.69	8.14	24 66	8.25	24.62	8.36
27	25.68	8.34	25 64	8.46	25.60	8.57	25.57	8.68
28	26.63	8.65 8.96	26 .59	8.77 9.08	26 .55 27 .50	8.88 9.20	26.51 27.46	9.00
29 30	27.58 28.53	9.27	27.54 28.49	9.39	28 45	9.52	28.41	9.64
31	29.48	9.58	29.44	9.71	29.40	9.84	29.35	9.96
32	30.43	9.89	30.39 31.34	10.02	30 35 31.29	10.15	30.30	10.61
33 34	31.38 32.34	10.51	32.29	10.65	32.24	10.79	32.20	10.93
35	33.29	10.82	33.24	10.96	33.19	11.11	33-14	11.25
36 27	34.24	11.12	34.19 35.34	11.27	34.14 35.09	11.42	34.09 35.04	11.57
37 38	35.19 36.14	11.74	36.09	11.90	36.04	12.06	35.98	12.21
39	37.09	1205	37.04	12.21	36.98	12.37	36.93 37.88	12.54
40	38.04	12.36	37-99 38.94	12.53	37 93	1301	38.82	13.18
41	39.94	12.98	39.89	13.15	39.83	13.33	39.77	13.50
43	40.90	13.29	40.84	13.47	40.78	13.64	40.72	13.82 14.14
44 45	41 85 42.80	13.60 13.91	41.79	13.78	41.73 42.67	14 28	42.61	14.46
46	43.75	14.21	43 69	14.41	43.62	14.60	43.56	14.79
47	44.70	14.52	44.64	14.72	44.57	14.91	44.51	15.11
48 49	45.65 46.60	14.83	45.59 46.54	15.03	45.52 46.47	15.23	45.45	15.43 15.75
50	47.55	15.45	47 49	15.66	47.42	15.87	47-35	16.07
51	48.50	15.76	48.43	15.97	48.36	16.18	48.29	16.39
52 53	49·45 50.41	16.07 16.38	49.38 50.33	16.28	49.31 50 26	16.50 16.82	49.24 50 19	16.71 17.04
54	51.36	16 69	51.28	1691	51.21	17 13	51.13	17.36
55	52.31	17.00	52.23	17.22	52.16	17.45	52.08	17.68
56 57	53.26 54.21	17.31	53.18 54.13	17.54	53.11 54.05	17.77 18.09	53.03 53.98	18.32
58	55.16	17.92	55.08	18.16	55.00	18.40	54.92	18.64
59 60	56.11 57.06	18.23 18.54	56 03 56.98	18.48 18.79	55.95 56.90	18.73	55.87 56.82	18.96 19.29
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
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=	Lat.	Dep.	Lat.	Dep.	Lat.	Dep	Lat	D
61	58.01	18.85	57 93	19.10	57.85	19.36	57.76	19.
63	58.97	19.16	58.88	19.42	58.80	19 67	· 58.71	19.
64	60.87	19.78	60.78	20.04	60.69	20.31	60.60	10.
65	61.82	20.09	61.73	20.36	61.64	20.62	61.55	20.
66	62.77	20.40	62.68	20 67	62.59	20.94	62 50	21.
68	63.72	20.70	63.63	20.98	63.54	21.26	63.44 64. 3 9	21.
69	65.62	21.32	65.53	2161	65 43	21.89	65.34	22.
70	66 57	21.63	66.48	21.92	66.38	22.21	66.29	22.
71	67.52	21.94	67.43	22 23	67.33	22.53	67.23	22.
72 73	68.48 69.43	22.25	68.38 69.33	22.55	68.28	22.85	68.18	23.4
74	70.38	22.87	70.28	23.17	70.18	23 48	79.07	23.
75	71.33	23.18	71 23	23.49	71.12	23.80	71.02	24.
76	72.28	23.49	72.18	23.80	72.07	24.12	71.97	24.4
77 78	73.23	23 79 24.10	73.13	24.11 24.43	73.02	24 43 24.75	7 3 .86	24.
79	75.13	24.41	75.03	24.74	74-92	25.07	7481	25.
80	76.08	24.72	75.98	25.05	75.87	25.38	75-75	25.
81	77.04	25.03	76.93	25.37	76.81	25.70	76.70	26.0
82 83	77 99 78.94	25 34 25.65	77.88	25.68	77.76	26 02 26.34	77 65	26. 26 6
84	79.89	25.96	79.77	25.99 26.31	78.71 79.66	26.65	78.60 79-54	27.0
85	80.84	26.27	80.72	26 62	80.61	26 97	80.49	27 3
86	81.79	26.58	81.67	26.93	81.56	27.29	81 44	27.6
8 ₇ 88	82 74	26.88	82.62	27.25	82 50	27.61	82.38	27.9
89	83.69 84. 6 4	27.19 27.50	83.57 84 52	27.56 27.87	83.45 84.40	27.92 28.24	83.33 84.28	28.1
90	85.60	27.81	85.47	28 18	85.35	8 56	8g.22	28.9
91	86 55	28 12	85.42	28.50	86.30	28.87	86.17	29.2
92	87.50	28.43	87.37	28 81	87.25	29.19	87.12	29.5
93 94	88 45 89.40	28.74 29.05	88.32 89.27	29.12	88 19 89.14	29.51 29.83	88.06	29.8 30.1
99	90.35	29.36	90.22	29.75	90.09	30.14	89 y6	30.5
96	91 30	29.67	91.17	30.06	91.04	30.46	90.91	30.8
97	92.25	29.97	92.12	30.38	91.99	30.78	91.85	31.1
98 99	93.20	30.28 30 59	93.07 94.02	30.69	92.44	31.10	92.80	31.8
100	95.11	30.90	9+97	31.32	94.83	31 73	94 69	3.2.1
101	96.06	31.21	95.92	31.63	95.78	32.05	95.64	32.4
102	97.01	31.52	96.87	31.94	96.73	32.36	96.59	32.7
103	97.96 98.91	31.83 32.14	97.82 98.77	32.26 32.57	97.68 98.63	32 68 33.00	97·53 98.48	33 F
105	99.86	32.45	99.72	32.88	99 57	33.32	99.43	33.4 33.7
106	100.8	32.76	100.7	33.20	100.5	33.63	100.4	34.0
107	8.101	33.06	301.6	33.51	101.5	33.95	101.3	34.3
108	102.7	33·37 33·68	102.6	33.82	102.4	34 27	102.3	34.7
110	104.6	33.99	103.5 104.5	34.1 3 34.45	103 4	34 59 34 99	103.2 104.2	35.Q 35 3
111	105.6	34-30	105.4	34.76	105.3	35.22	105.1	35.4
112	106.5	34.61	106.4	35.07	106.2	35.54	106.1	30. g
113	107.5	34.92	107.3	35.39	107.2	35.86	107.0	36.3
114	108.4	35.23 35.54	108.3	35.70 36.01	108.1	36.17 36.49	108.0	36. 4 36. 9
116	110.3	35.85	110.2	36.33	110.0	36.81	109.8	37.2
117	111.3	36.16	111.1	36.64	111.0	37.12	110.8	37.
118	112.2	36.46	112.1	36.95	111.9	37-44	111.7	37.
119	113.2	36.77 37.08	113.0	37.27 37.58	112.9	37.76 38. 08	112.7	38 4
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5	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.95	0.33	0.94	0.33	0.94	0.33	0.94	0.34
3	1.89 2.84	0.65	1.89 2.83	0. 66 0.99	1.89 2.83	0.67	1.88 2.82	0.68
4	3.78	0.98	3.78	1.32	3 77	1.34	3.7.6	1.35
_ 5	4-73	1.63	4-72	1.65	4-71	1.67	4-71	1.69
6	5 67	1.95	5.66	1.98	5.06	2.00	5.65	2.03
7 8	6.62	2.28 2.60	6.6t	2.31 2.64	6.60	2-34 2.67	6.59	2.37
9	7.5 6 8.51	2.93	7.55 8.50	2.97	7·54 8.48	3.00	7·53 8. 47	2.70 3.04
10	9.46	3.26	9.44	3.30	9.43	3 34	9.41	3.38
11	10.40	3.58	10 39	3.63	10.37	3.67	10.35	3.72
12	11.35	3.91	11.33	3.96	11.31	4.01	11.29	4.06
13 14	12.29 13.24	4.23 4.56	12.27	4.29 4.62	12.25	4-34 4-67	12.24	4-39 4-73
15	14.18	4.88	14.16	4 95	14.14	5.01	14.12	5.07
16	15.13	5.21	15.11	5.28	15.08	5.34	15.06	5-41
17	16 07	5.53	16.05	5.60	16.02	5.67	16.00	5.74
18	17.0 2 17.96	6.19	16.99 17.94	5.93 6. 26	16.97 17 91	6.01	16.94	6.08 6.42
20	18.91	6.51	18 88	6.59	18.85	6.68	18.82	6.76
21.	19.86	6 84	1983	6.92	19.80	7.01	19.76	7.10
22	20.80	≈ 7⋅16	20.77	7.25	20.74	7.34	20.71	7-43
23 24	21.75	7.49	21.71 22.66	7.58	21.65	7.68 8.01	21.64	7.77
25	22.69 23.64	7.81° 8.14	23.60	7.91 8.24	23.57	8.35	23.53	8.45
26	24.58	8.46	24-55	8.57	24-58	8.66	34.47	8.79
27	25.53	8.79	25.49	8.90	25.45	9.01	25.41	9.12
28	26.47	9.12	26.43	9.23	26.39	9.35	26.35	9.46
29 30	27.42 28.37	9.44	27.38 28.32	9.56 9.89	27.34 28.38	9.68	27.29 28.24	9.80
31	29.31	10.09	29.27	10.22	29.22	10-35	29.18	10.48
32	30.26	10.42	30.21	10.55	30.16	10.68	30.12	18.01
33	31.20	10.74	31.15	10.88	31.11	11.02	31.06	11.15
34	32.15 33.09	11.07	32.10 33.04	11.21	32.05 32.99	11.35	32.00	11.83
35	34.04	11.72	33 99	11.87	33.94	12,02	32-94 33.88	12.17
37	34.98	12.05	34-93	12.20	34.88	14.35	34.82	12.50
38	35.93	12.37	35.88	12.53	35.82	12.68	35.76	23.84
39 40	36.88 37.82	12.70	36.82 37.76	12.86	3 6 .76	13.02	30.7K	13.18
41	38.77	13.02	38.71	13.19	37.71	13.35	37.65	13.52
42	39.71	13-35 13.67	39.65	13.85	39-59	13.69	39-53	13.85
43	40.66	14.00	40.60	14.18	40.53	14.35	40.47	14-53
44	41.60	14.33	41.54	14.51	41.48	14 69	41.41	14.87
45	42.55	14.65	43.48	14.84	43.42	15.02	48.35	15.21
47	43-49 4 4- 44	14.98	43·43 44·37	15.17	43.36	15.36 15.69	*43.29 44.24	15.54 15.88
48	45.38	15.63	45.32	15.83	45.25	16.02	45.18	16.22
49	46.33	15.95	46.26	16.15	46.19	16.36	46.72	16.56
50	47.28	16.23	47.20	16.48	47.13	16.69	47.00	16.90
51 52	49.17	16 93	49.09	17.14	48.07 49.02	17.02 17.36	48.94	17.43 17.57
53	50.11	17.26	50.04	17.47	49.96	17.69	49.88	17.91
54	51.06	17.58	50.98	17.80	50.90	18.03	50.82	18.25
55	52.00	17.91	51.92	18.13	51.85	18.36	51.76	18.59
56 57	52.95 53.89	18.23 18.56	52.87 53.81	18.46 18.79	52-79 53-73	18.69	53.65	18.92 19.26
58	54.84	18.88	54.76	19.12	54.67	19.36	54.59	19.60
59	55.79	19.21	55.70	19.45	55.62	19.69	55.53	19.94
60	56.73	19.53	56.65	19.78	56.56	20.03	56-47	20.28
Dist.	Dep.	Lat	1)ep	Lat.	Dep.	Lat	Dep.	Lat
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1	Dia.	Lat	Пер	Lat	Dep	Late	Dep.	Lat	Dep
ł	61	57.68	19 \$6	\$7-59	20.11	57-50	90.36	57-41	20 61
í	6a	58.62 59-57	20.51	58-53 59-48	80.44 90.77	58.44 59.39	21.03	58.35	21 19
ŧ	64	60,51	30.84	60.43	81.10	60.33	21 35	60 24	21.53
ı	65	61 46	81.16	61.37	11.43	61.37	31 70	61.18	21.96
ľ	66	6140	31.49	62.31	11.76	61.16	32.03	63.06	22.30
1	67 68	63.35	91.81 93.64	63.25 64.30	11.09 11.41	64.10	83.37 93.70	64 00	22.98
ł	69	65.24	44 46	65 14	22.75	65.04	25.03	64 94	23 32
ŧ	70	66.19	32.79	66.09	13.08	65 98	23.37	65 88	23 65
ł	71	67 13	13.12	67.03 67.97	23 41	66.93 67 87	23.70 24.03	67.76	23.99 24.33
ł	72 73	65.08	93.44 93.77	61.92	24.07	65.81	24-37	68.71	24.67
1	74	69.97	24 09	6g_86	34 40	69-76	24 70	69.65	8501
1	75	70 91	34.43	70.81	24-73	70.70	25.04	70 59	15.34
ł	76	71.86	\$4.74 \$4.07	71.75	25.06 25.39	71 64 73-58	25.37	71-53	95.68 86 02
ł	77	73.75	45 39	71 64	25 72	73-53	10.01	73-41	£6.36
ı	79 ID	7470	45.13	74-58	26.05	74 47	26.37	74-35	16.73
1		75.64	46 05	75-53	26 38	75-42	26 70	75 29 76 24	87-03
1	\$1 \$2	76.59 77-53	16.70	75.47 77.43	26.70 27.03	76.35 77.30	27.04 27.37	77-18	37-37 37 71
ł	13	78.48	37.04	78-36	17 36	78.24	47 71	78.13	28.05
ţ	14	79.43	37 35	79-30	27 69	79 18	18.04	79.06 80 00	18.39 18.72
Į	35	80.37	27 67	10.35	28.02	80.12	38 71	B0.94	20.06
ı	\$6 \$7	\$1.31 \$2.26	28.00 28.11	\$1.19 \$5.14	38 35 38 68	\$1.07 \$1.01	19.04	81,88	19.40
۱	31	\$3.21	28 6g	\$3.0\$	10.08	\$2 95	19-37	81.82	19.74
١	39	84-15	2.4	84.03	29.34	\$3.90 \$4.84	19.7 f 30 04	83.76 84.71	\$0.07 \$0.41
ŀ	90	85.10	*9. D	84.97	30.00	85.78	30.38	85 65	30 75
l	91 93	\$6.04 \$6.99	29.63 29.85	\$5 gt \$6.86	30.33	86.72	30 71	86.59	31.09
Ĭ	93	\$7.93	30.18	\$7.80	30.66	87 67	\$1.04	87.53	31-43
1	94	22.22	37.60	23.74 89 69	30.00	\$9.55	31.38	\$8.47 \$9.41	31.76
ł	95	8g.8s	3D.03 31.25	90.61	31.65	90.49	1105	92 35	\$4.44
1	96 87	9677	fr.5	91.5	\$1.08	91 44	32.38	91 29	32.78
1	98	91.66	31.91	91.51	39.3 1	91.31	32.71	93 24	13.13
1	100 100	91.61	32.55	93.46	37 64 32 97	93 38 94-16	33 O5 13.38	93 18	33-45
•	101	9455	30.88	95-35	33.10	95 21	33.71	95.06	34-13
	102	96.44	23.31	96.30	33.61	96 rş	34.05	90.00	34-47
I	103	97-39	33-53	97.24	33.96	97.09	34-38	96 94 97 88	34-84
-	104 105	98.33	33.86 34-18	98.19	34 29 34.62	98 98	35.05	98 82	1,.48
	106	100.1	34-51	Y00. L	34 95	99.92	35 38		35 82
ŀ	107	tor.2	34 84	101.0	35 28	100.9	35.72	100.7	36.16
	108	102, t	35-16	102.0	35.61 35.94	101.5	36.05 36.38	701.6	36.49 36.83
•	109	1014	35.49 35.81	103.8	30 27	103.7	36.72	101.5	37.17
4		105.0	36.14	104.8	36.60	104.6	37.05	104 5	37.58
k	162	105 9	35.46	109.7	36 93	105.6	37-39	105.4	37.85 58.18
		105.8	36 79 37.11	107.6	37.26 37.58	306.5 807.5	37.73 38.05	106.4	38.52
	1	108.7	37-44		37 91	108.4	38.79	108.2	38.86
- 111	116	100-7	37-77	139.5	38.84	109.3	38.72		39.20
	117	110,6	38 09	\$10.5	38.57	£ 10.3	39 06	110.1	39-54 39-87
-	1 2 8 1 4 9	111.6 112.5	38.48 38.74	113.3	38.90 39.13	111.1	39.39 39.73	J110	40.36
	130	113.5	39.07	113.3	39 56	113.1	40 06	118.9	40.55
1	4	Dep.	Lat.	Dep	Lat.	Dep.	Lat	Dep.	Let
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-	0.94	0.34	0.94	0.35	0.94	0.35	0.94	0.35
2	1.8 8 2.83	0.68	1.88 2.81	0.69	1.87 2.81	0.70	1.87 2.81	2.71 1.06
3 4	3.76	1.03	3.75	1.38	3.75	1.40	3.74	1.42
5	4.70	1.71	4.69	1.73	4:68	1.75	4.68	1.77
6	5.64	2.05	5.63	2.08	5.62	2.10	5.61	2.13
7	6.58	2.39	6.57	2.42	6.56	2.45 2.80	6 .55 7.48	2.48 2.83
9	7 52 8.46	2.74 3.08	7.51 8.44	2.77 3.12	7·49 8 43	3 15	8.43	3.19
10	9.40	3 42	9.38	3.46	9-37	3.50	9.35	3.54
11	10.34	3.76	10.32	3.81	10.30	3.85	10.29	3.90
12	11.28	4.10 4.45	11.26	4.50	11.24	4-20 4-55	11.22	4-25 4-61
13 14	13.16	4.79	13.13	4.85	13.11	4-90	13.09	4.96
15	14-10	5.13	14-07	5.19	14.05	5.25	14.03	:5.31
16	15.04	5.47	15.01	5.54	14.99	5.60	14 96	5.67
17.	15.97	5.81	15.95 16.89	5.88 6.23	15.92 16.86	5.95 6.30	15.90 1 6. 83	6.02 6.38
19	17.85	6.50	17.83	6.58	17.80	6.65	17.77	6.73
20	18.79	6 84	18.76	6.92	18.73	7.00	18.70	7.09
21	19.73	7.18	19.70	7 27	19.67	7 35	19.64	7.44
22	20.67 21.61	7.52 7.87	20.64 21.58	7.61	20.61	7.70 8.05	20.57 21.51	7.79 8.15
23	22.55	8.21	23.52	7.96 8.31	21.54	8.40	22.44	8.50
25	23.49	8.55	23.45	8.65	23.42	8.76	23.38	8.86
26	24 43	8.89	24.39	9.00	24.35	9.11	24 31	9.21
27 28	25.37 26.31	9.23 9.58	25.33 26.27	9.35 9.69	25.29 26.23	9.46 9.81	25.25 26.18	9·57 9·92
29	27.25	992	27.27	10.04	27.16	10.16	27.12	10.27
30	28.19	10.26	28.15	10.38	28 10	10.51	28.05	10.63
31	29.13	10.60	29.08	10.73	29.04	10.86	28.99	10.98
33	30.07 31.01	10.94 11.29	30.02 30.96	11.08	29.97 30 9 I	11.21	29.92 30.86	11.34
33 34	31 95	11.63	31.90	11.77	31.85	11.91	31.79	12.05
35	32.89	11.97	32.84	12.11	32.78	12.25	32.73	12.40
36	33.83	12.31	33.77	12.46	33.72	12.61	33.66	12.75
37 38	34-77. 35-71	12.65 13.00	34.71 35.65	12.81	34.66 35.59	12.96 13.31	34.60 35.54	13.11 13.46
39	36.65	13.34	36.59	13.50	36.53	13.66	36.47	13.82
40	37-59	13.68	37.53	13.84	37.47	14.01	37-41	14-17
41	38.53	14.02 14.36	38.47	14.19	38.40	14.36	38.34	14-53
42 43	39.47 40.41	14.71	39.40 40.34	14.54 14.88	39-34 40-28	14.71	39.28 40.21	14.88
44	41.35	1505	41.28	15.23	41 21	15.41	41.15	15.59
45	42.29	15.39	42.22	15 58	42-15	1576	42.08	15.94
46	43 23 44.17	15.73 16 07	43.16	15.92 16.27	43.09	16.11 16.46	43.02	16.30 16.65
47 48	45.11	16.42	44.09 45.03	16.61	44.02 44.96	16.81	43.95	17.01
49	46.04	16.76	45.97	16.96	45.90	17.16	45.82	17.36
50	46.98	17.10	46.91	17.31	46.83	17.51	46.76	17.71
51	47 92 48.86	17-44 17-79	47.85 48.79	17.65	47-77 48.71	17.86 18.21	47.69 48.63	18.07 18.42
52 53	49.80	18.13	49-73	18.34	49.64	18.36	49.56	18.78
54	50.74	18.47	50.66	18.69	50.58	16.81	50.50	19.13
55	51.68	18.81	51.60	19.04	51.52	19 26	51 43	19.49
56	52.62 53.56	19.15 19.50	52.54° 53.48	19 38	52.45	19.61 19.96	52.37	19.84 20.19
57 58	54.50	19.84	54.42	20.07	53·39 54·33	20.31	53.30 54.24	20.19
59	55.44	20.18	55.35	20 42	55.26	20 66	55:17	20.90
60	56.38 Den	20.52	56.29	20.77	56.20	21.01	56.11	21 26
Dist	Dep O'	Lat	Dep	Lat.	Dep.	Lat	Dep.	Lith
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Dist	0)	1:	5'	3	0'	45	,			
155	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.			
61	57-32	25.86	57-23	21.11	57.14	21.36	57.04	21.61			
62	58.26	21.21	58.17	21.46	58.07	21.71	57.98	21.97 22.32			
64	60.14	21.89	60.04	22.15	59.95	22.41	59.85	24.67			
65	61.08	22.13	60.98	22.50	60.88	22.76	60.78	23.03			
66	62.02	22.57	61.92	22.84	61,82	23.11	61.72	23.38			
67	62.96 63.90	22.92	62.86, 63.30	23.19 23.54	62.7 6 63.69	23.46 23.81	62.65 63.59	23.7,4 24.09			
69	64.84	23.60	64.74	23.88	64.63	24.16	64.52	24.45			
70	65.78	23.94	65.67	24.23	65.57	24.51	65.46	24.80			
71	66.72	24.28	66.61	24.57	66.50	24.86	66.39	25.15			
72 73	67.66 68.60	24.63 24.97	67.55 68.49	24.92 25.27	67.44 68.38	25.31 25.57	67.33 68 26	25.51 25.86			
74	69 54	25.31	69.43	25 61	69.31	25.92	69.20	26.42			
75	70.48	25.65	70.36	25.96	70.25	26.17	70.14	26 57			
76	71.42	25.99	71.30	26.30	71.19	26 62	71.07	26.43			
77 78	73.36	26.34 26.68	72.24	26.65 27.00	72.12	26.97 27.32	72.01 72.94	27.28 27.62			
79	74.24	27.02	74.12	27.34	74.00	27.67	73.88	27.99			
80	75.18	27 36	75.06	27.69	74.93	28 02	74.81	28.34			
81	76.12	27.70	75 99	28.04	75.87	28.37 28.72	75.75	28 70			
82 83	77.05	28.05 28.39	76.93 77-87	28.38 28.73	76.81 77.74	19 07	76.68 77.62	29.05 29 41			
84	78.93	28.73	78.81	29.07	78.68	29.41	78.55	29.76			
85	79-87.	29.07	79-75	29 42	79.62	29.77	79.49	30.11			
86 87	\$0 81 \$1.75	29.41 29.76	80.68 81.62	29.77 30.61	80.55 81.49	30 12 30.47	80 42 81.36	30.47 30.82			
88	82.60	30 10	82:56	30.46	8243	30.82	82 29	31.18			
89	83.63	30.44	83.50	30.80	83 36	31.17	83:23	31.53			
90	84.57	30.78	84.44	31.15	84 30	31.52	84.16	31.89			
91	85.51 86.45	31.12	85.38 86.31	31.50	85.24 86.17	31.87 32.22	85.10 86.03	32.24 32.59			
92 93	87.39	31.84	87.25	32.19	87.11	32.57	86 97	32.95			
94	88.33	32.15	88.19	32.54	88.05	32.92	87.90	3,.30			
95	89.27	32.49	89.13	32.88	88.98	33.27	88 84	33.66			
96 97	90.21	32.83	90.07	33. 23 33.57	89.92 90.86	33.62 33.97	89.77 90.71	34.0.5 3+ 37			
98	92.09	33.52	91.94	33.92	91.79	34-32	9164	34-72			
99	93.03	33.86	92.88	34.27	92.73	34.67	92 58	35.07			
100	93.97	34.20	93.82	34.61	93 67	35.02	93.51	35.43 35.78			
101	94.91	34.54 34.89	94.76 95.70	35.30	95.54	35.37 35 72	94 45 95.38	36.14			
103	96.79	35.23	96.63	35.65	96.48	36.07	96 32	36.49			
104	97·73 98.67	35.57	97 57 98.51	36.00 36.34	97.41 98.35	36.42 36.77	97.25 98.19	36.85 37.20			
105	99.61	35 91 36.25	99.45	36.69	99 29	37.12	99-12	37.55			
107	100.5	36.60	100 4	37.03	100.2	37.47	100.1	37.91			
108	101.5	36.94	101.3	37.38	101.2	37.82	101.0	38.26			
011	102.4	37.28 37.62	102.3	37·73 38.07	103.0	38.17 38.52	101 9	38.62 38.97			
111	104.3	37 96	104.1	38.42	104 0	38.87	103.8	39-33			
112	105.2	38.31	105.1	38.77	104.9	39.22	104.7	39.68			
113	106.2	38.65	106.0	39.11	105.8	39.57	105.7 106.6	40.03			
114	107.1	38.99 39.33	107.0	39.46 39.80	107.7	39.92 40 27	107.5	40.39			
116	109.0	39.67	108.8	40.15	108.7	40.62	108.5	41.10			
117	109.9	40.02	109.8	40.50	109.6	40.97	109.4	41.45			
811	110.9	40.70	110.7	40.84	110.5	41.52 41.67	110.3	41.81			
119	112.8	41.04	111.6	41.53	1124	42.02	112.2	42.52			
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1	0.93	0.36	0.9 (0.36	0.93	0.37	0.91	0.37
	1.87	0.71	1 80	072	1.86	0.73	1.86	0.74
3	2.8 3	108	2.80	1 09	2.79	1 10	1.79	1.12
4	3.73	1 43	3.73	145	3.73	47	3-73 4-64	t.48 t.85
5	467	1 7q	4.66	181	4.65	183		
6	5 60	2.15	5-59	2.17	5 58	2.23	5-57	1.13
7	6 54	2.51	6.52	2.54	6.51	2.57	6.50	2.59
8	7-47	2.87	7 46	2 90	7.44	2.93	7 43	2.96
9	8.40	\$ 13	8.39	3 26 3 6 2	8.37	3 50	8.36 9.29	3 34 3.7£
10	9-34	3 /8	9 32		9 30			4.08
11	10.27	3 94	10.21	3 49	10.23	4 93	10.92	4.45
12	11 20	4.30	11.18	4-15 4-71	11.17	4.76	12.07	7 82
23	12-14	5 02	12.12	5 07	13 03	5 13	13.00	5.19
15	14.00	5 38	13.98	5 44	13 96	5 50	1393	5.56
1				5 80	14.89	5 86	14.86	5.93
16	14.94	5.73 6.0g	14.84	6 16	1582	6 23	15.79	6 30
17	16.85	6.45	16.78	6 52	16.75	6.60	16 73	6.67
19	17,74	6.81	17.74	6 89	168	6 96	47 65	7.04
10	18 67	7 17	18 64	7 35	18.61	7 33	18.58	7-41
2.0	1961	7 53	19 57	761	19 54	7 70	19.5t	7-78
11	10.54	7 88	20 50	7 97	20.47	8.06	20-43	8 15
73	21.47	8, 24	21 41	8 34	21.40	8 43	21,36	8.52
14	12,41	8 60	22.37	8 70	22.33	8.80	22 29	8.89
25	23 34	8.96	27.30	9 06	23 26	9.16	23,32	9. 26
26	24.27	9.32	24.23	9 42	24-19	9 53	84-15	9.63
27	35.24	9 68	25.16	9.79	25 12	9 90	25.08	10.01
18	26.14	10.03	26,10	10 15	16.05	10 26	16 01	10.38
19	17.07	10.39	\$7.03	10.51	26.98	10.63	26-94	10 75
3.5	18 Q L	10 75	27 96	10 87	27 91	11 00	27 86	11 18
3+	28 94	11.11	18 13	11 24	£8 84	11.36	28.79	1 6.49
32	29 87	11.47		111,60	39 77	11 73	19.72	14 86
33	35.81	11.83	30 76	11 96	30 70	11 09	30.65	13.23
34	3174	13 18	31.69	12 72	3 6 6 3	12.46-	3158	12.97
35	32 68	12 54	1262	11 69	31 56			
36	33 61	12 90	33 15	130,	33 50	13 19	33-44	13.34
37	34 54	13 10	34.48	14 51	3+43	13 56	34-37	13.71 14.08
33	35 48	13 98	35 42	13 77	35 36	13 93	35.39	14 45
39	36 41	14-33	37 28	14 50	17 22	14 66	37 15	14 82
40		1					38 C8	15.19
41	38 28	14.69	38 21	14 86	38 15	15 03	39.01	15.56
42	39 21	15.41	39 14 40.08	15 58	40.01	15 76	39.94	15 93
43	41 08	15 77	41.01	1595	40.94	16 13	40.87	16.30
44	4201	16.13	41 94	1631	41 87	16 49	41.80	16 68
	41 94	16 48	4287	16 67	42 80	16.86	42 73	17-05
46 47	43 88	16.84	43.80	17.03	43 73	17 23	43 65	17.42
48	44.81	17 20	44.74	17.40	4+66	17 59	44.59	17.79
49	45.75	17 56	45 67	17.76	45 59	17 96	45 51	18.16
50	46 68	17.92	46.60	18 13	46 52	18 33	46 44	18.53
51	4-61	18,28	47 53	18 48	47 45	18 69	47 37	18.90
52	48 55	18 64	48 46	18.85		(tg.Q6	48 30	19.27
53	49 48	18.99	49 40	19.21	49 31	119.48	49 23	19.64
54	50 41	1935	50 33	19.57	50.14	19.79	50.16	20.01
55	51 35	1971	51 26	1992	51 17	20 16	51.08	30.38
56	52.28	25.07	52.19	20 30	52,10	20.53	52.01	20.75
57	53 21	20.43	53.13	20 66	# - T	20,89	52.94	21.72
58	54.15	20.79	54 06	21.03	53 96	21.26	53 87	31-49
59	55.08	21 14	54-99	21.38	54.89	21.62		21.86 22.23
60	56.01	21 50	55 91	21 75	55.83	21 99	55-73	
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I	62	57.88	22 22	57 78	22 47	57 69	2 72	57 59	41.97
ı	61	58 82	22.58	58.72	22 83	58 62	23 09	58.52	23 35
ı	64	59-75	22.94	59.65	23 20	59.55	23 46	59-44	23.72
Į.	65	60.68	23 19	60 58	23 56	60 48	13 82	60.37	24 09
ì	66	61.62	23 65	6151	23 92	61 41	24-19	61.30	24.46
ı	68	63.48	24.01 24.37	62 44	24 65	62.34	124.56	62.16	24.83 25.20
ł	69	64.48	24.73	64.31	25.06	64.20	25 29	64.09	25 57
ŧ	70	65.35	25 09	69 24	25 37	65.13	2, 66	65.60	11 94
ľ	71	66.18	2 44	66 17	25 73	65.06	26 -2	05.95	26 31
ł	72	67 22	2, 80	67 10	26 10	66.99	26 39	66 ×7	26.68
ŧ	73	68.49	26.16	68 04	26 46	67 92	26.75	67.80	27:05
ł	74	69.08	16 52 26 88	68 97	26 82	68.85	27 12	68.73	27 42
ŀ	75	70.01		69 90	27 (8	69.78	27-49	69.66	27-79
1	76	70.95	37.24	70 83	27 55	70.71	27 85	70 59	28 16
ı	78	71.89	27 59 27 95	71 6	27 91	72.57	28 59	71 52	28.90
ı	79	73 75	28.31	73 63	28 63	73.50	28 95	73 38	29.27
ı	80	74 69	18 67	74 56	29.00	74-43	19.32	74-30	29 64
ľ	81	~562	29 03	75 49	29 36	75.36	29.69	75.23	30.01
1	82	76.55	29 39	76.42	29 72	75 29	30.05	75.16	30 39
1	83	77 49	29 74	77 36	30 08	78.16	30 42	77.09	30.76
1	84	78 42	30.10	78 29 79.22	30 95	79.09	30.79	78.02	31.13
ł	86	79.35	30 82		-	80.02		79 88	31.87
Į.	87	80.29 81.32	31.18	80.15	36.17	80 95	31.53 31.8g	80.81	32.24
1	88	\$2.16	31 54	82.02	31 89	81 88	32.25	81 74	32.61
1	89	83.09	31 89	82.95	32 26	83.81	32.62	82.66	32.98
Į.	90	84 02	32 25	83 88	32.61	83-74	32 99	85.59	33 35
ł	91	84.96	32.01	8481	3298	84 67	33 35	8+52	37,22
1	92	85.89	32.97		33-34	85.60	33 72	85 45	34 09
ł	93	86.82 87.76	33.33	\$6.68 \$7.61	33 71	86.53	34.08	26.38 27.31	34.46
1	95	\$8 6g	34.04	88.54	34 43	88.39	34 82	88.24	35.20
t	96	89.62	34-40	89.47	34-79	89.32	35 18	89.17	35 57
ł	97	90.56	34-76	90.40	35 16	90.25	35 55	90.09	35 94
ł	98	91.49	35 22	91.34	35.52	91.18	35.92	91.01	36.31
ł	99	92 42	35-48	92.27	35.88	91.11	36.28	91 95	36,69
-	100	93 36	35 84	93.20	36.24	93 04	36 65	92.88	37 06
	101	94 19	36 20	94-13	30 61	93-97	37 02	93.81	37 43 37 80
-	103	95 23 96.16	36.55 36 98	95.00	36.97 37.33	94.90	37 38 37 75	94 74	38.17
	104	97.09	37 27	96 93	37 69	96.76	38.12	96.60	35.54
	ιος	9803	37 63	97 86	38 06	97 69	38 48	97-53	38 91
	106	98.96	37 99	98.79	38.42	98.62	38 85	98.45	19 28
	707	99.89	38.35	99.72	38.78	99-55	39.22	99.38	39.65
	108	100.8	38 70	100.7	39-14	100 5	39.58	100.3	45.02
-	100	101.8	39.06 39.43	101.6	39.51	101-4	39.95	101.2	40.39
	111		39.78	-			40 68		41.13
	12	103.6	40 14	103 5	40.59	103.3	41 05	103.1	41 50
	113	105.5	40.50	1053	40.96	1001	41 44		41 87
I	114	106.4	40.85	106.2	41.32	106.1	41,78	105.9	42.34
48	115	107-4	41.38	107 1	41 68	107 C	42 15	106.8	42 61
	116	108.3	41.57	108.1	42.04	167.9	42.51	107.7	42.98
	117	109.1	41.93	109.0	42.41	108.9	42.28	108.7	43.36
	119	110.1	42.65	110.0	42.77	109.8	43.25	109.6	43 73
	130	113.0	41.00	3116	43.13	116.7	43.48	111.5	44-10
1		Dep.	Lat.	Dep.	Lat	Dep.	-	Dep.	Lat.
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-	0.93	0.37	0.93	0.38	0.92	0.38	0.92	0.39
2	1.85	0.75	1.85	0.76	1.85	0.77	1.84	0.77
3	2.78	1.12	2.78	1.14	2.77	1.15	2.77	1.16
4	3.7 I 4.64	1.50	3.70 4 63	1.51	3.70 4 62	1.53 1.91	3.69 4.61	1.55
5 6	-	2.25	5.55	2.27	5.54	2 30	5-53	2.32
	5.56 6.49	2.62	6.48	2.65	6.47	2.68	6.46	2.71
7 8	7.42	3.00	7.40	3.03	7.39	3.06	7.38	3.09
9	8.34	3.37	8.33	3.41	8.31	3.44	8.30	3.48 3.87
10	9.27	3.75_	9,26	3.79	9.24	3.83	9.32	
11	10.20	4.12 4.50	10.18	4-17 4-54	10.16	4.21 4.59	10.14	4.25 4.64
13	12.05	4.87	12.03	4.92	12.01	4-97	11.99	5.03
14	12.98	5.24	12.96	5.30	12.93	5.36	1291	5.41
15	13.91	5.62	13.38	5.68	13.86	5.74	13.83	5.80
16	14.83	5.99	14.81	6.06	14.78	6.12	14.76	6.19
17	1576	6.37 6.74	15.73	6 44 6.82	15.71 16.63	6.51	15.68 16 60	6.57 6.96
19	16 69 17.62	7.12	17.59	7.19	17.55	7.27	17.52	7.35
20	18.54	7.49	18.51	7.57	18.48	7.65	18.44	7.73
21	19.47	7.87	19.44	7.95	19.40	8.04	19-37	8.12
22	20 40	8.24	20 .6	8.33	20.33	8.42	20.29	8.52
23	21 33	8.62	21.29 22.31	8.7 I 9.09	21.25	8.80 9.18	21.21 22.13	8.89 9.28
24 25	22.25	8.99 9.37	23.14	9.47	23 10	9.57	23.06	9.67
26	24.11	9.74	24 06	9.84	24.02	9.95	23.98	10.05
27	25.03	10.11	24.99	10.22	24.94	10.33	24.90	10.44
28	25.96	10.49	25.92	10.60	25.87	10.73	25.82	10.83
20	26.89	10.86	26.84	10.98 11.36	26.79 27.72	11.10	26 .74 27 .67	11.21
30	27.82	11 24	27.77	11.74	28.64	11.86	28.59	11.99
31	28.74 29.67	11.61	28.69 29.62	12.12	29.56	12.25	29.51	12-37
33	30.60	12 36	30.54	12.50	30.49	12.63	30-43	12.76
34	31.52	12.74	31-47	r2.87	31-41	13.01	31.35	13.15
35	32.45	13.11	32.39	13.25	32-34	13.39	32.28	1.3.53
36	33.38	13.49 13.86	33.32 34.25	13 03 14.01	33.26 34.18	13.78	33.20 34.12	13.92 14.31
37 38	34.31 35.23	14.24	35.17	14-39	35.11	14.54	35.04	14.69
39	36.16	14.61	36.10	14-77	36.03	14.92	35.97	80.21
40	37.09	14.98	37.02	15.15	36.96	15.31	36.89	15.47
41	38.01	15.36	37.95	15.52	37.88	15.69	37.81	15.86
42	38.94	5.73	38.87	15.90	38.80 39-73	16.46	38.73 39.65	16.24 16.63
43 44	39-87 40.80	16.11	39.80 40.72	16.66	40.65	16.84	40.58	17 02
45	41.72	16.86	41.45	17.04	43.57	17.22	41.50	17.40
46	42.65	17.23	42.57	17.42	42.50	17.60	42.42	17.79
47	43.58	17.61	43 50	17.80	43.42	17.99	43-34	18.18
48.	44.50	17.98	44-43	18.18	44-35	18.37	44-27	18.56 18.95
50	45.43 46.36	18.36 18.73	45-35	18.93	46.19	19.13	46.11	19.34
51	47.29	19.10	47.20	19.31	47.12	19.52	47.03	19 72
52	48.21	19.48	48-13	19.69	48.04	19.90	47-95	20 11
53	49.14	19.85	49.05	20.07	48.97	20.28	48.88	20.50 20.88
54	50.07	20.23 20.60	49 .9 8 50.90	20 45 20 83	49.89	20.66	49.80 50.72	21.27
56	51.00		51.83	21.20	51.74	21.43	51.64	21.66
57	51.92 52.85	20.98 21.35	51.03	21.58	52.66	21.81	52-57	22.04
58	53.78	21.73	53.68	21.96	53.59	22.20	53.49	22.43
59	54.70	22.10	54.61	22.34	54.51	22.58	54 41	22.82
60	55.63	22.48	55.53	12.72	55.43	22.96	55-33 Nep	23.20 Lat.
Dist.	Dep.	La	Dep.	Lut	Dep.	Lat	Dep.	
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Ä	Lat.	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1 61	56.56	22.85	56.46	23.10	56.36	23.34	56.25	23.59	
62	5749	23.23	57-38	23.48	57.28	23.73	57.18	23.98	
63	58.41 59 34	23.60 23.97	58.31	23.85 24.23	58.20	24.11	58.1C	24.36 24.75	
65	60.27	24.35	60.16	24.61	60.05	24.87	59.94	25.14	
66	61.19	24.72	61.09	24.99	60 98	25.26	60 87	25.52	
67	62.12 63.05	25.10 25.47	62.01 62.94	25 37 25.75	61.90	25.64 26.02	61.79	25.91 26.30	
69	63.98	25.85	63.86	26.13	63.75	26.41	63.63	26.68	
70	64.90	26.22	64.79	26.51	64.67	26.79	64.55	27 07	
71	65.83	26.60	65.71	26.88	65.60	27.17	65.48	27.46	
72	66.76 67.68	26.97 27.35	66.64 67.96	27.26 27.64	66.52	27.55 27.94	66.40 67.32	27.84 28.23	
74	68.61	27.72	68.49	28.02	68.37	28.32	68.24	28.62	
75	69.54	28.10	69.42	28 40	69.29	28.70	69.17	29.00	
76	70.47 71.39	28.47 28 84	70.34	28.78 29.16	70.21	29.08 29.47	70.09 71.01	29.39 29.78	
78	72 32	29.22	71.27	29.53	72.06	29.85	71.93	30.16	
79	73.25	29.59	73.12	29.91	72.99	30 23	72.85	30.55	
80	74.17	29.97	74.04	30.29	73.91	30.61	73.78	30.94	
81 82	75.10 76.03	30 34 30.72	74·97 75.89	30.67 31.05	74.83 75.76	31.00	74.70 75.62	31.32	
89	76 96	31.09	76.82	31.43	76.68	31.76	76.54	32.10	
84	77.88	31.47	77.75	3,1.81	77.61	32.15	77.46	32.48	
86	78.81	31.84	78.67	32-19	78.53	32.53	78.39	32.87	
87	79.74 80:66	32.22 32.59	79:63 80.52	3 t. 56 3 2 9 4	79 45 80,38	32.91	79.31	33.26 33.64	
88	81.59	32.97	81.745	33.32	\$1,30	33.68	81.15	34.03	
89	82.52	33.34	82.37	33 70	\$2.23	34.06	82.08	34.42	
90	83.45	33.71	83.30	34.08	83 15	34.44	83.00	34.80	
91 92	84.37 85.30	34.09 34.46	84.22	34.46 34 84	84.07	34 82 35.21	83.92 84.84	35.19	
93	86.23	34.84	86.08	35.21	85.92	135.59	85.76	35.96	
94	\$7.16 \$8.08	35.21	87.00	35.59	86,84	35.97	86.69	36.35	
95	89.01	35.59 35.96	87.93	35 97 36.35	87 77	36.74	\$87.61 \$8.53	36 74 37-12	
97	89.94	36.34	89.78	3 6 .73	8 9.6 a	37.12	89.45	37.51	
98	90.86	36 71	90.70	37.11	90.54	37.50	90:38	37.90	
99	91.79	37.09 37.46	91.63	39·49 37.86	91.46 92.39	37 89 38.27	91.30	38.24 38 64	
101	93.65	37.84	93.48	38.24	93.31	38.64	93.14	39.0	
103	94-57	38.21	94-41	38.62	94-24	39.03	94.06	39.4	
103	95.50	38.58	95.33	39.00	95.16	39.42	94-99	39.	
105	96.43 97·35	38.96 39.33	96.26 97.18	39.38 39.76	96.08	39.80	95.91 96.83	40.2 40 6	
106	98.28	39.71	98.11	40.14	97.93	40.56	97-75	40.	
107	99.21	40.08	99.03	40.52	98.86	40.95	48.68	41.	
801 109	100.1	40.46	99.96	40.89	99.78	41.33	199.60, 100.5	41.7	
110	102.0	41.21	101 g	41.65	101 6	42.10	101 4	42.	
111	102.9	41 58	102.7	42.03	102.6	42.48	102.4	42.9	
113	103.8	41.96		42.41	103.5	42.86	103.3	45 3	
114	104.8	42.33	104.6	42.79	104.4	43 24 43.63	104.2 105.1	43-7	
115	106.6	43.08	106.4	43.54	106.2	44.01	106.1	44.4	
116	107.6	43.45	107.4	43.92	107.2	44.39	107.0	44	
117	108.5	43.83	108:3	44.30 44.68	108.1	41.77	107.9	45-	
1119	110.3	44.58	_	45 06	109.0	45.16	109.7	45. 46	
120	111.3	44.95	111.5	45.44	110.9	45.92	110.7	46.	
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	0.92	0.39	0.92	0.39	0,92	0.40	0.92	0.40
	1.84	0.78	1.84	9.79	1.83	0.80	1.83	0.81
3	2.76	1.17	2.76	1.18	2-75	1.20	2.75	1.21
4	3.68	1.56	3.68	1.58	3.67	1 60 1.99	3.66 4.58	1.61 2.01
5	4.60	1.95	4.59		4.59	1.39		2.4€
6	5.5 2 6.44	2.34	5.51 6.43	2.37 2.76	5.50 6.42	2.79	5-49 6-41	2.83
7 8	7.36	3.13	7.35	3.16	7-34	3 19	7.32	3.22
9	8 28	3.52	8 27	3.55	8.25	3.59	8.24	3.62
110	9.21	3.91	9.19	3.95	9 17	3.99	9-15	103
11	10.13	4.30.	10.11	4 34	10.09	4.39	10.98	4-43 4-83
12	11.05	4.69 5.08	11.03	4.7 4 5.13	11.92	4.79 · 5118	11.90	5.24
13	12.89	5 47	12.86	5.53	12 84	5.58	12.81	5.64
15	1381	5.86	13.78	5.92	13.76	5.98	13.73	6 04
16	14.73	6.25	14.70	6.32	14.67	6.38	14.65	6 44
17	15.05	6.64	15.62	6.73	15.59	6.78 7.18	15.56.	6.85
18	16.57	7 03	16.54	7.11	16.51 17.42	7.58	16.48. 17.39.	7.25
19	17.49	7.81	18 38	7.89	18.34	7.98	18.31	8.05
1 21	19.33	\$.21	19.39	8.29	19.26	8.37	19.22	8.46
22	20.25	8.60	20.21	8.68	20.18	8-77.	30,14	8.86
23	21.17	8.99	21.13	9.08	21.09	9-17	21.05	9.26
24	12.09	9.38	22.05	9-47	22.01	9.57	21,97	9.67
25	23.01	9.77	22.97	9.87	22.93	10.37	23.80	10.47
26	23.93 24.8 5	10.16	23.89 24.81	10.36	23.84	10.77	24.71	10.87
27 28	25.77	10.94	25.73	11.05	25.68	11.16	25.63	11.28
29	26.69	11.33	26.64	11.45	26.59	11.56	26.54	11.68
30	27.62	11.72	27.56.	11.84	27.51	11.96	27.40	80.91
31	28.54	12.11	28.48	12.24	28,43	14.36	28.37	12 45
32	29.46	12.89	29.40 30.32	13.03	39.35 30.26	13.16	39.29. 30.21	13.89 13.39
33 34	30.38	13.28	31.24	13.42	31,18	13.56	31.12	13.69
35	32.22	13.68	32.16	13.82	32,10	13.96	32.04	14.10
36	33.14	14.07	33.08	14 21	13.01	14.36	32.95	14.50
37	34.06	14.46	34,00	14.61	33.93	14.75	33.87	14.90
38	34.98	14.85	34.91 55.83	15.00	34.85	15.45	34.78 35.70	15.74
39 40	35.90 36.82	15.24	36.75	15.40	35.77 36.68	15.55	36.61	16.11
		16.02	37.67	16.18	37.60	16.35	37 53	16.51
41 42	37.74 38.66	16.41	38.59	16.38	38.52	16.75	3844	16.92
43	39.58	16.80	39.51	16 97	39:43	17.15	39.36	17.32
44	40.50	17.19	40.43	17.37	40.35	17.54	40.27	17.72
45	41.42	17.58	41 35	17.76	41.27	17.94	41 19	
46	42.34	17.97 1 \$.36	42.26 43.18	18.46	42.18 43,10	18.34	42.10 43 -0 2	18.53
48	43.26	18.76	44.10	18.95	44.02	19.14	43-93	19.33
49	45.10	19.15	45.02	19.34	44.94	19.54	44.85	19.73
50	46.03	19.54	45.94	19.74	45.85	19 94	45.77	20.14
51	46.95	19.93	46.86	20.13	46.79	29.34	46,68	20.54
. 52	47.87	20.32	47.78	20.53	47:50	20.74	47.60	20.94
53 54	48.79 49.73	20.71 21.10	48.70	20.92	48.6p	21.13	48.51 49-43	21.35
55	50.63	21.49	50.53	21.71	50.44	21.93	50.34	23.15
56	51.55	21.88	51.45	22. E I	\$1:36.	22.33	51.26	22.55
57	\$2.47	22.27	52.37	22.50	52.27	22.73	52,17	23.96
58	53.39	22.66	53.29	22 90		23.13	53.09	23.36
59 60	54.31	23.05 23.44	54.28	23.29 23.68	54117	123.53 123.92	54.00	23.76 24.16
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	*}	Lit	Dep.	Lat.	Dep	Lat.	Dep.	Lat	D:
ľ	61	56-15	23.83	56.09	24.08	55.94	24:32	. 55.83	24.57
1	62	57 07	24.23	56.97	34.47	55 86	24:72	56.75	24-97
1	6;	57.99 58.91	24.62 25.01	57.88 54.80	24 87 25.26	57·77 58.69	25112 25.52	58.58	25.78
1	65 -	59.83	25.40	59.72	25.66	59 61	25.92	59.50	26 18
l	66	60.75	125.79	60 64	26.05	60.53	26.32	60.41	26.58
1	67	61.67	26.18	61.56	26 45	61.44	26.72	61 39	26. 98
	68 69	62.59 63.51	26 57 26.96	62.48	26 84 27.24	62.3 6 63.28	27-11 27-51	62.24 63.1 6	27.39 27.79
1	70	64.44	27 35	64 32	27.63	64.19/	27.9 I	64.07	28.19
	71	65.36	27 74	15.23	\$8.03	65 11 .	28.31	64.99	28.6C
ı	72	66.38	28.13	66.15	28.42	66.03	28.71	65.90	29.00
ł	73	67-20	28.52 28.91	67.9 3	28.82 29.21	66.95 67.86	29.11 29.51	66.82 67.73	29.40 29.80
	74 75	69.04	29.30	68.91	29.61	68.78	29.91	68,65	30.21
ľ	76	69.96	29.70	69 83	30.00	69 70	30.30	69.56	30.6€
1	77	70.88	30.09	70.75	30.40	70.61	30.70	70.48	31 01
I	78	72.72	30 4 8 30.87	71.67 72.58	30.79 31.18	71.53	31.10 31.50	74.31	31.41
1	79 80	73.64	31.26	73.50	31.58	72.45 73.36	31.90	73.22	32.22
ŀ	18	74.56	31.65	74-42	31 97	74.28	32.30	7414	32.62
ı	82	75.48	32.04	75.34	32.37	75.20	32.70	75.06	33.03
ł	83	76.40	32.43 \ 32.82	76.26	32.76	76.12	33.10	75.97	33.43 33.83
1	84 85	77.32 78.24	33.21	77.18	33.16 33.55	77.03	33.49 33.89	76.89	34·23
ł	86	79.16	33.60	7.9 02	33.95	78.87	34.29	78.75	34.64
1	87	80.08	33 99	79.93	34-34	79.78	34.69	7963	35.04
-	88	81.00	34.38	80.85	34-74	80.70	35.09	80.55 - 81.46	35.44 35.84
1	89 93	82.85	34-78 35 17	81.77 82.6g	35.13 35.53	81.62 82.54	35.49 35.89	82.38	36.25
1	91	83.77	35.56	83 61	35.92	83.45	36.29	83.29	36.65
1	93	84.60	35.95	84-53	35.32	84.37	36.68	84 24	37.05
1	93	85.61 86.53	35 34	85.45	36.71	85.29	37 08	85.12. 86.04	37.46 37.86
1	94	87.45	36.73 37 12	86.37 87. 29	37.50	86 20 87.12	37.48 37.88	86.95	38 26
ł	95 96	88.37	37.51	88.20	37.90	88.04	38.28	87.87	38 66
4	97	89-29	37.90	89.12	3 8.29	88 95	38.68	88.79	39.07
I	98	90.21	38.89	90.04	38.68	89.87	39. 08	89.70	39·47 39·87
1	99	91.13	38 .58 39. 07	90.96 91.88	39. 06 39.47	90.79	39. 48 39.87	90.62 91.53	40.27
	101	92.97	39.46	92 80 .	39.87	92.62	40.27	93.45	40.68
	102	93.89	39.85	93-72	40.26	93.54	40 67	93.36	41.08
	103	94.81	40.25	94.64	40.66		41.07	94.28	41.48
	104	95.73 96.65	40. 64	95.55	41.45	95.37 96,29	41.47	95.19	12.29
-	106	97.57	41.42	97-39	41.84	جسوش ه	42.27	97.02	42.69
ł	107	98.49	41.88	98.31	42.24	98.13.	42.67	97-94	43.09
- 6	108	99-41	12.20		42.63	99.04	43.07	98-85	43.50
	109	100.3	42.59	1.001	43.03 43.43	99.96.	43.40	99-77	43.90 44.30
1	111		43.37	-	43.82		44 26	101.6	44.70
. 3	112	103.1	43.76	102 9	44.31	104.7	44 66	102.5	45.11
-	113	1040	44.15	_	44.61	103.6	45.06		45.51
ł	114	104.9	44·54 44·93	• •	45.40 45.40	104.5	45.86	104.3	45.91 46.32
	16	106.8	45.32	106.6	`	106.4			46.72
	117	109.7	45.72	107.5	46.19	107-3	46.65	. 107"1.	47-13
•	118	108.6	46.11	•	46.58	108.2	47.05	' 🖚	47.93
-	119	109.5	46.89		·4 5 .97 147.37	110.0	4 7 4 5 (-	47.93
1	· — ·	Dep.	Lat.	D. p	Lat.	'Dep	Lat.	Dep:	
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3 2.74 1.22 2.74 1.33 2.73 1.24 2.72 1.26 4 3.65 1.63 3.65 1.64 3.64 1.66 3.63 1.67 5 4.57 2.03 4.56 2.05 4.55 2.07 4.54 2.09 6 5.48 2.44 5.47 2.46 5.46 2.49 5.45 2.51 7 6.39 2.85 6.38 2.88 6.37 2.90 6.36 2.93 8 7.31 3.25 7.39 3.29 7.28 3.32 7.27 3.73 9 8.23 3.66 8.21 3.70 8.19 3.73 8.17 3.77 10 9.14 4.07 9.12 4.11 9.10 11 10.05 4.47 10.03 4.52 10.01 4.56 9.99 4.51 12 10.96 4.88 10.94 4.93 10.92 4.98 10.90 5.02 13 11.85 5.29 11.85 5.31 11.83 5.99 11.81 5.41 13 11.88 5.29 11.85 5.31 11.83 5.99 11.81 5.54 13 11.85 5.99 11.85 5.75 12.74 5.81 12.71 5.86 16 14.62 6.51 14.59 6.57 12.74 5.81 12.71 5.86 16 14.62 6.51 15.50 6.98 15.47 7.05 15.44 7.12 18 16.44 7.32 16.41 7.39 16.38 7.46 16.35 7.54 17 15.53 6.91 15.50 6.98 15.47 7.05 15.44 7.12 20 18.27 8.13 18.24 8.21 18.20 8.29 18.16 8.37 21 19.18 8.54 19.15 8.63 17.21 7.89 18.16 8.37 22 20.10 8.95 20.06 9.04 20.02 9.12 19.38 9.62 23 21.01 9.35 20.06 9.04 20.02 9.12 19.38 9.62 24 21.03 9.76 21.88 9.86 21.84 9.95 21.80 10.89 25 22.84 10.17 22.79 10.27 22.75 10.37 22.70 (0.47 26 23.775 10.58 23.71 10.68 23.66 10.78 23.76 10.89 27 24.67 10.98 24.62 11.09 24.57 11.20 26.34 11.43 28 25.58 11.39 25.53 11.50 25.48 11.41 2.39 26.94 11.72 29 26.49 11.80 26.44 11.91 26.39 12.03 26.34 12.14 29 26.49 11.80 26.44 11.91 26.39 12.03 26.34 12.14 21 2.00 27.55 12.32 27.30 13.68 29.97 13.83 3.00 13.85 31.97 14.24 31.91 14.83 31.85 14.55 11.29 26.34 11.73 27.91 27.91 12.20 27.55 12.32 27.30 13.68 29.97 13.84 29.23 13.60 13.83 31.00 13.96 30.94 14.10 30.88 14.23 31.91 15.40 39.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.85 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.84 29.95 13.85 29.95 23.95 29.		0.91	0.41	0.91	0.41			0.91	
3.65 1.63 3.65 1.64 3.64 1.66 3.63 1.67 5 4.57 2.03 4.56 2.05 4.55 2.07 4.54 2.09 6 5.48 2.44 5.47 2.46 5.46 2.49 5.45 2.51 7 6.39 2.85 6.88 2.88 6.37 2.90 6.36 2.93 8 7.31 3.25 7.29 3.29 7.28 3.72 7.27 3.35 9 8.22 3.66 8.21 3.70 8.19 3.73 3.17 3.77 10 9.14 4.07 9.12 4.11 9.10 4.15 9.08 4.19 11 10.05 4.47 10.03 4.52 10.01 4.56 9.99 4.51 12 10.96 4.88 10.94 4.93 10.92 4.98 10.90 5.49 13 11.88 5.29 11.85 5.34 11.83 5.39 11.81 5.44 14 12.79 5.69 12.76 5.75 12.74 5.81 12.71 5.86 15 13.70 6.10 13.68 6.16 13.65 6.22 13.68 6.28 16 14.62 6.5! 14.59 6.57 14.56 6.44 14.53 6.70 17 15.53 6.91 15.50 6.98 15.47 7.05 15.44 18 16.44 7.32 10.41 7.39 16.38 7.46 16.35 7.54 19 17 36 7.73 17.33 7.80 17.29 7.88 17.25 7.95 21 20.10 8.95 20.06 9.04 20.02 9.12 22 20 19 9.35 20.06 9.04 20.02 9.12 23 21 10.58 23.71 10.68 23.66 10.78 23.69 6.37 24 21.93 9.76 21.88 9.86 21.84 9.95 21.80 10.05 25 22.84 10.17 22.79 10.27 22.75 10.37 22.70 6.47 28 25.95 11.39 25.53 11.50 25.48 11.61 25.43 11.73 26 23.75 10.58 23.71 10.68 23.66 10.78 23.61 10.78 25 23.84 10.17 22.79 10.27 22.75 10.37 22.70 6.47 26 23.75 10.58 23.71 10.68 23.66 10.78 23.61 10.78 27 24.67 10.89 24.62 11.90 24.57 11.30 24.52 11.30 27 24 12.20 27.35 12.32 27.30 13.44 27.24 12.50 27 28 29 29 29 29 29 29 29	•				•		, -		
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43 39.28 17.49 39.21 17.66 39.13 17.83 39.05 18.00 44 -40.20 17.90 40.12 18.07 40.04 18.25 39.96 18.42 45 41 11 18.30 41.03 18.48 40.95 18.66 40.87 18.84 46 42.02 18.71 41.94 18.89 41.86 19.08 41.77 19.26 47 42.94 19.12 42.85 19.30 42.77 19.49 42.68 19.68 48 43.85 19.52 43.76 19.71 43.68 19.91 43.59 20.10 49 44.76 19.93 44.68 20.13 44.59 20.32 44.50 20.51 50 45.68 20.34 45.59 20.54 45.50 20.73 45.41 20.93 51 46.59 20.74 46.50 20.95 46.41 21.15 46.32 21.35 52 47.50 21.15 47.41 21.36 47.32 21.56 47.22 21.77 53 48.42 21.56 48.32 21.77 48.23 21.98 48.13 22.19 54 49.33 21.96 49.24 22.18 49.14 22.39 49.04 22.61 55 50.25 22.37 50.15 23.59 50.05 22.81 49.95 23.03 56 51.16 22.78 51.06 23.00 50.96 23.22 50.86 23.44 57 52.07 23.18 51.97 23.41 51.87 23.64 51.76 23.86 58 52.99 23.59 52.88 23.82 52.78 24.05 52.67 24.28 59 53.90 24.00 53.79 24.23 53.69 24.47 53.58 24.70 60 54.81 24.40 54.71 24.64 54.60 24.88 54.49 25.12 Dep Lat. Dep. Lat. Dep. Lat. Dep Lat.	•		•		1		1 '		
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47	-	41 11		41.03	-			<u> </u>	18.84
48 43.85 19.52 43.76 19.71 43.68 19.91 43.59 20.10 49 44.76 19.93 44.68 20.13 44.59 20.32 44.50 20.51 50 45.68 20.34 45.59 20.54 45.50 20.73 45.41 20.93 51 46.59 20.74 46.50 20.95 46.41 21.15 46.32 21.35 52 47.50 21.15 47.41 21.36 47.32 21.56 47.22 21.77 53 48.42 21.56 48.32 21.77 48.23 21.98 48.13 22.19 54 49.33 21.96 49.24 22.18 49.14 22.39 49.04 22.61 55 50.25 22.37 50.15 22.59 50.05 22.81 49.95 23.03 56 51.16 22.78 51.06 23.00 50.96 23.22 50.86 23.44 57 52.07 23.18 51.97 23.41 51.87 23.64 51.76 23.86 58 52.99 23.59 52.88 23.82 52.78 24.05 52.67 24.28 59 53.90 24.00 53.79 24.23 53.69 24.47 53.58 24.70 60 54.81 24.40 54.71 24.64 54.60 24.88 54.49 25.12 Dep Lat. Dep. Lat. Dep Lat. Dep. Lat.		1	·	_ <u>_</u>	1 -		1		
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\$2 47.50 21.15 47.41 21.36 47.32 21.56 47.22 21.77 53 48.42 21.56 48.32 21.77 48.23 21.98 48.13 22.19 54 49.33 21.96 49.24 22.18 49.14 22.39 49.04 22.61 55 50.25 22.37 50.15 22.59 50.05 22.81 49.95 23.03 56 51.16 22.78 51.06 23.00 50.96 23.22 50.86 23.44 57 52.07 23.18 51.97 23.41 51.87 23.64 51.76 23.86 58 52.99 23.59 52.88 23.82 52.78 24.05 52.67 24.28 59 53.90 24.00 53.79 24.23 53.69 24.47 53.58 24.70 60 54.81 24.40 54.71 24.64 54.60 24.88 54.49 25.12 2		***********							-
53 48.42 21.56 48.32 21.77 48.23 21.98 48.13 22.19 54 49.33 21.96 49.24 22.18 49.14 22.39 49.04 22.61 55 50.25 22.37 50.15 22.59 50.05 22.81 49.95 23.03 56 51.16 22.78 51.06 23.00 50.96 .23.22 50.86 23.44 57 52.07 23.18 51.97 23.41 51.87 23.64 51.76 23.86 58 52.99 23.59 52.88 23.82 52.78 24.05 52.67 24.28 59 53.90 24.00 53.79 24.23 53.69 24.47 53.58 24.70 60 54.81 24.40 54.71 24.64 54.60 24.88 54.49 25.12 Dep Lat. Dep. Lat. Dep. Lat. Dep. Lat.				_			1 7		
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56 51.16 22.78 51.06 23.00 50.96 .23 22 50.86 23.44 57 52.07 23.18 51.97 23.41 51.87 23.64 51.76 23 86 58 52.99 23.59 52.88 23.82 52.78 24.05 52.67 24.28 59 53.90 24.00 53.79 24.23 53.69 24.47 53.58 24.70 60 54.81 24.40 54.71 24.64 54.60 24.88 54.49 25.12 Dep Lat. Dep Lat. Dep. Lat.	54	49-33	21.96	49.24	22.18	49-14	22.39	49.04	22.61
57 52.07 23.18 51.97 23.41 51.87 -23.64 51.76 23.86 58 52.99 23.59 52.88 23.82 52.78 24.05 52.67 24.28 59 53.90 24.00 53.79 24.23 53.69 24.47 53.58 24.70 60 54.81 24.40 54.71 24.64 54.60 24.88 54.49 25.12 Dep Lat. Dep Lat. Dep Lat.	-	-	_		_	_			,
58 52.99 23.59 52.88 23.82 52.78 24.05 52.67 24.28 59 53.90 24.00 53.79 24.23 53.69 24.47 53.58 24.70 60 54.81 24.40 54.71 24.64 54.60 24.88 54.49 25.12 Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat. 15'		_			. 1		1		
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Dep Lat. Dep. Lat. Dep. Lat. Dep. Lat. 30' 15'	59	53.90	24.00	53.79	24.23	53.69	24.47	\$3.58	24.70
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of Degrees.

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l	Dist.	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.
1	61	55.73	24.81	55.62	25.05	55.5L	25.30	55.40	25.54
I	62 63	56 64	25.22 25.62	56.53	25.46 25.88	56.42	25.71 26.13	56 30 57.21	25.96 26.38
1	64	57-55 58.47	26.03	57.44 58.35	26.29	57.33 58 24	36.54	58.12	26.79
ı	65	59.38	26.44	59.26	26.70	59.15	26.96	59.03	27.21
1	66	60.29	26.84	60.18	27.11	60.06	27.37	59.94	27.63
	67	61.21 62.12	27.25 27.66	61.09 62.00	27.52 27.93	60.97 61.88	27.78 28.20	60.85	28.05 28.47
	69	63.03	28.06	62.91	28.34	62.79	28.61	62.66	28.89
1	70	63.95	28.47	63.82	28.75	63.70	29.03	63.57	29.31
1	71	64.86	28.88	64.74	39.16	64.61	29.44	64.48	29.72
1	72 73	65.78 66.69	29.29 29.69	65.65 66.56	29.57 29.98	65.52 66.43	29.86 30.27	65.39 66.29	30.34 30.56
}	74	67.60	30.10	67.47	30.39	67.34	30.69	67.20	30.98
1	75	68.52	30.51	68.38	30.80	68.25	31.10	68.11	31.40
	76	69 43 70.34	30.91 31.32	69.29 70.21	31. 21 31.63	69.16 70.07	31.5 2 31.93	69.02 69.93	31.82 32.24
ı	77 78	71.26	31.73	78.12	32.04	70.98	32.35	70.84	32.66
ł	79	72.17	32.13	72.03	32.45	71.89	32.76	71.74	33.07
	80	73.08	32.54	72 94	32.86	72.80	33.18	72.65	33.49
ł	81	74.00 74.91	32.95 33-35	73.85 74.76	33. 2 7 33.68	73.71	33.59 34.00	73-56 74-47	33-91 34-33
	83	75.82	33 76	75 68	34.09	75.53	34.42	75.38	34.75
	84	.76.74	34-17	.76.59	34:50	76.44	34.83	76.28	35-17
	85	77.65	34-57		34-91	77.35	35.25 35.66	77.19	35.59 36.00
	. 86 87	78.56 79.48	34.98 35.39	78.41 79.32	35.32 35.73	78.26 79.17	36.08	79.01	36.42
1	88	80.39	35.79	80.24	36.14	80.08	36.49	79.92	36.84
1	89	81.31	36.20 36.61	81.15 82.06	36.5 5. 36.96	80 99 81.90	36.91 37.32	80.82 81.73	37 26 37.68
1	90	83.13	37.01	82.97	37.38	8281	37.74	82.64	38.10
1	91 92	84.05	37.42	83.88	37.79	83.72	38.15	83.55	38.52
1	93	84.96	37 83	84-79	38.20	84.63	38.57	84.46	38.94
1	94	85.87 86.79	38.23 38.64	85.71 86.62	38.61 39-02	85.54 86.45	38.98 39.40	85.37 86.27	39·35 39·77
1	95 96	87.70	39.05	87-53	39.43	87.36	39.81	87.18	40.19
ì	97	88.61	39.45	88.44	39.84	88.27	40.23	88.09	40.6 t
	98	89.53	39.86	89.35	40.25	89.18	40.64	89.00	41.03
	99	90.44	40.27	90.26	40.6 6 41.07	90.09	41.05	89 91 90.81	41.45
	101	92.27	41.08	92.09	41.48	91.91	41.88	91.72	42.28
٠,	102	93.18	41.49	93.00	41.89	92.82	42.30	92.63	42.70
	103	94.10	41 89	93.91 94.82	42 30 42.71	93 73 94.64	42.71 43.13	93.54 94.45	43.12 43.54
	104 105	95.01 95 .9 2	42.30 42.71	95.74	43.13	95.55	43.54	95-35	43.96
	106	96.84	43.11	96.65	43.54	96.46	43.96	96.26	44-38
	107	·	43.52	97.56	43.95	97-37	44-37	97.17	44.80
	109	98.66 99.58	43.93 44.33	98-47 99.38	44.36 44.77		44-79 45.20	98.08 98.99	45.22 45.63
	110	100.5	44.74	100.3	45.18	100.1	45.62	99.90	46.05
	111	101:4	45.15	101.2	45.59		46.03	100.8	46.47
	112		45.55	Ï	46.00 46 41		46.45 46.86	101.7	46.89
	113		45.96	103.9	46.82		47.28		47-31 47-73
	115	105.1	46.77	104.9	47.23	104 6	47.69	104.4	48.25
	116	106.0	47.18	105.8	47.64	•	48.10	105.3	48.56
	117	106.9	47.59	106.7	48.05 48.46	106.5	48.52 48.93	106.3	48.98 49.40
	119	108.7	48.40	108.5	48.88	108.3	49.35	108.1	49.82
	1 20	109.6	48.81	. 109-4	49.29	109.2	49.76	109.0	50.24
	Dist.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat
	ä	1 0	/	45	نبست نيبدي	30		15	,
				65	DEGR	EES.			

10	0'		15/		30′		45'		
Dist.	Lat	Dep.	Lat.	Dep.	Lat	Dep.	Lat	Dep.	
1	0.91	0.42	0.90	0.43	0.90	0.43	0:90	0.43	
2	1.81	0.85	1.81	0.85	18.8	0.86	1.80	0.87	
3	2.72 3.63	1.27	2.71 3.62	1.28	2.7 t 3.6 t	1.72	3.70 3.62	1.30 1.74	
5	4.53	2.11	4-52	2 13	4.51	2.15	4.50	2.17	
6	5-44	2.54	5.43	2.56	5.42	2.58	5.40	2.61	
7	6.34	2.96	6.33	2.99	6.32	3 01	6.30	3.04	
8	· 7 25	3.38 3.80	7.24 8.14	3.41	7.22 8 12	3.44 3.87	7.21 8.11	3.4 3 3.91	
10.	9.06	4.25	6.04	4.27	903	4.31	9.01	4-34	
11	9-97	4.65	995	4 69	993	4-74	9.91	4-78	
12	10.88	5.07	10.85	5.12	10.83	5.17	18.01	5.21	
13	11.78	5.49	14.76	5.55	11.73 12.64	5.60 6.03	11.71 12.61	5.65 6.08	
14	12.69 13.59 •	5.9 2 6.34	13.66	5.97 6.40	13.54	6.46	13.51	6.5k	
16	14.50	6.76	14-47	6.83	14-44	6.89	14.41	6.95	
17	15.41	7.18	15.38	7.25	15-34	7 32	19.31	7 39	
18	16.31	7.61	16.28	7.68	16 25	7.75	16.21	7.82	
19	17.22	8.03 8.45	17.18	8.10 8.53	17.15	8.18 8.61	17.11	8 25 8.69	
21	19.03	8.88	18.99	8.96	18.95	9 04	18.91	9.12	
22	19.94	9.30	19.93	9.38	19.86	9.47	19.82	9.56	
23	20.85	9.72	20.80	9.84	20.76	9.90	20.72 21.62	9-99	
24 25	21.75 22.66	10.14	\$1.71 \$2.61	10.84	21.66 22.56	10.33	22.52	10.43	
26	23.56	10.99	23-52	11.00	23-47	03 11	23-42	11.90.	
27	24 47	11.41	24.42	11.52	24.37	11.62	24 32	11.73	
28	25.38	11.83	25.32	11.94	25.27	12.05	25.33	12.16	
29 30	26. 28 27.19	12.26	26.23 27.13	12.37	26.18 27.08	J 2.48 J 2.93	20.12	12.60 13.03	
31	28,10	13.10	28.04	13.88	27.98	13.35	27.92	13.47	
32	29.00	13.52	28.94	13.65	28 ¥8	13.78	28.82	13.90	
33	29.91	13.95	29.85	14.08	29.79 20.60	14.21	29.72	24.34	
34 35	30.81	14.37	39.75 · 31.66	14 50	30.69	14.64 15.07	30.62 31.52	14-77 15.31	
36	32.63	15.21	32.56	15.36	3249	15.50	32-43	15.64	
37	33.53	15.64	33.46	15.78	33.40	15.93	33-33	16.07	
38	34.44	16 06	3437	16.21 16.64	34:30	16.36	34-33	16.51 16.94	
39 40	35.35 36.25	16.48	35.27 36.18	17.06	35.20 36.10	17.22	35.13 . 36.03	17.38	
41	37.16	17.33	308	17.49	37.01	17.65	36.93	17.81	
43	.38.06	17-75	37-99	17.92	37.91	18.08.	37-83	18.25	
43	38.97	18.17	38.89	18.34	18.81	18.54	38.73 39.63	18.68	
44 45	39.88 40.78	18.60	39,80 40,70	19.30	40.62	19.37	40.53	19.12 19.55	
46	41.69	19.44	41.60	19 62	41.52	19.80	41.43	19.98	
-47	42 60	19.86	42.51	20.05	42.42	20.23	42.33	20.42	
48	.43-50	20.29 20.71	43-41	20 48 20.90	43.32 44-23	20. 66 21.10	43.23	20. 8 5 21 29	
49 50	44.41	21.13	45.23	21.33	45.13	21.53	45.03	21.72	
51	46.22	21.55	-	11.76	46.03	21.96	45.94	22.16	
52	47.13	21.98	47.03	22 18	46.93	22.39	46.84.	21.59	
53	48.03 48.94	22.40	47.94	22.61 . 23.03	47.84 48.74	22.82	47-74 48:64	23.03 23.46	
54 55	49.85	23.24	49.74	23.46	49.64	23.68		23.89	
56	50.75	23 67	50.65	23.89	.50054	24. 1.8	50.44	24-33	
57	51.66	24.09	51.55	24.31	51.45	24.54		24.76	
58	52.57	24.51 24.93	52.46 53.36	24.74 25.17	52.35	24.57 25.40	53-14-		
59 60	53-47 54-38	25.36	54-27	25.59	54:16	25.83		26.07	
1	Dep.	Lat.	Dep	Lat.	Dept	Lat	Dep.	Lat.	
Dist.	0		45' 30			1	15'		
64 DEGREES.									

20181.	?	0,		1	1		,	45'	
87.		Lat .	Dep.	Lat.	Dep.	Lat	Dep	Lat	Dep.
6		55.28	25.78	55.17	26.02	55.06	26.26	54-94	26.50
6	1	56.19	26.20 26.63	56.08	26.45	59.96	26.69	55.84	26.94
6	,	57.10	27.05	56.98 57.89	26.87 27.30	56 86 57 77	27.12 27.55	56.74 57.64	27 37 27 80
6	-	58.91	27.47	58.79	27.73	58.67	27.98	58.55	28.31
6		59 82	27.89	59.69	28.15	59-57	28.41	59.45	28.67
6	-	60.72	28.32 28 74	62.60	28.58 29.01	60.47 61. 1 8	28.84	60.35	29.11
6		62.54	29.16	62.41	29 43	62.28	29.27 29.71	62.15,	29.54 . 29.98
7	2	63.44	29-58	63.31	29.86	63.18	30.14	63.05	30.41
7		64.35	30.01	64.22	30.29	64.08	30.57	63.95	30.85
7	•	65.25 66.16	30.43 30.85	65.12	30.71	64.99	31.00	64:85	31.28
7.	_	67.07	31.27	66.93	31.57	66.79	31.86	66.65	31.71
7		67.97	31.70	67.83	31.99	67.69	32.29	67.55	32.58
7		68.88	32.12	68.74	32.43	68.60	32.72	68.45	33.03
7 7		69.79 70.69	32.54	69.64 . 79.55	32 85 · 33.27	69.50 ·	33.15 · 33.58	69.35	33.45 38 89
7	1	71.60	3,3-39	71-45	33.70	71 30	34.01	71.16	34.32
8	_	72.50	33 81	72.36	34.13	72.21	34.44	72.06	34-76
8	-	73-41	34-23	73.26	34.55	73.11	34-87	72 96	35.19
8		7432	34 65 35.08	74.17	34.98 35.41	74-91	35. 3 0	73.86	35 68 36. 06
8.	4	76-13	35.50	75 97	35.83	75.82	36.16	75.66	36.49
8		77-04	35.92	76.88	36.26	76.72	36.59	76.56	36.95
8	6 7.	77-94	36.35	77.78	36.68	77.63	37.02	77.46 78.36	37.36
8		78.85	36.77 37 19	78.69 79-59	37-11	78.53	37-45 37-89	79.26	37.80 .
8		80.66	37 61	80.50	37.96	80.33	38.32	80.16	38.67
9		81.57	38.04	81.40	38.39	81.23	38.75	81.06	39 10
9		83.47 83.38	38 46 38 88	84.31 83.41	38.82	82.14	39.18 39.61	81.96 82.86	39-53
9		84.29	39.50	84.11	39 24	83:04 83.94	40.04	83.76	39-97 40-40
9	4	85.19	39.78	85.02	40.10	84.84	40.47	84.67	40 14
9	_	86.10	40.15	85.93	40.52	85.75	40.90	85.57	41.27
9		87.01 87.91	40.57	86.83 87-73	40.95	86.65	41.33	86.47 87 37	41.75
9		88.82.	41.42	88.64	41.80	88.45	42.19	88.27	42.14 42.58
9		89.72	41.84	89.54	42.23	89 36	42 62	B9.17	43.01
10	-	90.63	42.26	90.45	42 66	90.26	43.05	90.07	43-44
10		91.54	43.41	91.35	43.08	91.16	43.48 43.91	90.97	43.88 44. 3 1
10	- 1	93-35	43.53	93.16	43.94	92.97	44.34	92.77	44-75
10.	- 1	94.26 95.16	43 95	94.96	44.36	93.87	44-77	93.67	45.18
10	_	96.07	44.80	94-97	45.22	94-77	45.63	94-57	45.62
10		96.97	45.22	96.78	45.64	96.58	46.06	96.37	46 49
10		97.88	45.64	97 68	46.07	97.48	46.50	97.28	46.92
10	- 1	98.79	46.49	98. 59	46.50	98.38 99 28	46.93 47.36	98.18 20.00	47.35
110		100.6	46.01		47 35	100 2	47.79	99.98	47.79
11	2	101.5	47.33	101.3	47.78	101.1	48.22	100.9	48.66
112	_	102.4	47.76	102.2	48.30	102.0	48.65	8,101	49.09
	-	103.3	48.60	103.1	48.63	103.8	49.08 49.51	102.7	.49.53 49.96
11		105.1	49.02	104.9	-	1047	49.94	104.5	50.40
11		1060	49.45	105 8	49.91	195.6	50.37	105.4	50.83
11		106.9	49.87	106.7	50.34	106,9	50.80	106.3	51.26
12	0	108.8	50.71	108.5	51.19	107.4	51.66	107.2	51.70
		Dep.	Lat.	Dep.	Lut.	Dep.	Lat	Dep.	Lat
	2	0	/		5'	30	ō. 	:	51
1	_	•		94	DEGH	PMS		Marie Land	

94 DECKEES.

Dist.	0	,	15	1	30	/	45	,
77	Lat.	Dep	Lat.	Dep.	Lat	Dep.	Lat.	Dep.
1	0.90	0.44	0.90 1.79	0.44	0.89	0.45	0.89 1.79	0.45
3	1.80 2.70	0.88	2.69	1.33	2.68	1.34	2.68	1.35
.4	3.60	1.75	3.59	1.77 2.21	3.58 4.47	1.78 2.23	3. 57 4. 46	1.80 2.25
6	4.49	2.19	5.38	2.65	5-37	2.68	5.36	2.70
7	5 39 6.29	3.07	6.28	3.10	6.26	3.12	6.25	3.15
8	7.19	3.51	7.18	3.54 3.98	7.16 8.05	3·57 4·02	7.14 8.04	3.60 4.05
10	8.09 8.99	3.95 4.38	8.97	4.43	8.95	4.46	8-93	4.50
11	9.89	4.82	9.87	4.87	9.84	4.91	9.82	4-95
12	10.79 11.68	5.26 5.70	10.76	5.31 5.75	10.74	5.35 5.80	10.72	5.40 5.85
14	12.58	6.14	12.56	6.19	12.53	6.25	12.50	6.30
15	13.48	6.58	13-45	6.63	13.42	6.69	13.39	6.75
16	14.38	7.01 7.45	14.35	7.08 7.52	14.32	7-14 7-59	14.29	7.20 7.65
18	16.18	7.89	16.14	7.96	16.11	8.03	16.07	8.10
19	17.08	8.33	17.94	8.40 8.85	17.00	8.48 8.92	16.97 17.86	8.55 9.00
31	17.98	9.21	18.83	9.29	18.79	9-37	18.75	9.45
12	19.77	9.64	1973	9.73	19.69	9.82	19.65	9.90
23	20.67	10.08	20.63	10.17	20.58 21.48	10.86	20.54	10.80
25	21.57	10.96	22.42	11.06	22.37	11.15	22.32	11.25
26	23.37	11.40	23.32	11.50	23.27	11.60	23.22	11.70
. 27 28	24.27 25.17	11.84	24.22	11.94	24.16 25.06	12.05	24.11 25.00	12.15
29	26.07	12.71	26.04	r2.83	25 95	12.94	25.90	13.05
30	26.96	13.15	26.91	13.27	26.85	13.39	26.79	13.50
31	27.86 28.76	13.59	27.80 28.70	13.71	27.74 28.64	13.83 14- 28	27:68 28.58	13.95
33	29.66	14-47	29.60	14.60	29.53	14.72	29.47	14.85
34	30.56	14-90	31.39	15.04	30-43 3432	15.62	30.36	15.30
35	31.46	15.34	32.29	15.92	32.22	16.06	32.15	16.10
37	33.26	16.22	33.18	16.36	33.11	16.51	33.04	16 65
38	34-15	16.66	34.08 34.98	16.81	34.01 34.90	16.96 17.40	33.93 34.83	17.60
39 40	35.05 35.95	17.53	35.87	17.69	35 80	17.85	35.72	18.00
41	36.85	17.97	36.77	18.13	36.69	18.29	36.61	18.45
42	37-75	18.41	37.67 38.57	18.58	37·59 38.48	18.74 19.19	37.51 38.40	18.90
43 44	38.65 39.55	19.29	39.46	19.46	39-38	19.63	39.29	19.80
45	40.45	19.73	40.36	19.90	40.27	20 08	40.18	20.25
46 47	41.34 42.24	20.17 20.60	41.26	20.35	41.17	20.53 20.97	41.08	20.70 21.15
48	43.14	21.04	43.05	21.23	42.96	21.42	42.86	21.60
49	44.04	21.48	43-95 44-84	21.67	43.85	21.86 22.31	43.76 . 44 65	22.05 22.50
50 51	44.94	21.92	45.74	22.56	45.64	22 76	45-54	22.95
52	46.74	22.80	46.64	23.00	46.54	23.20	46.43	23 41
53 54	47.64 48.53	23.23 23.67	47·53 48.43	23.44 23.88	47·43 48.33	23.65 24.09	47-33 48.22	23.86 24.31
55	49.43	24.11	49.33	24.33	49.22	24-54	49.11	24.76
56	50.33	24-55	50.22	24.77	50.12	24.99	50.01	25.21 25.66
57 58	51.23 52.13	24.99 25-43	51.12	25.21 25.65	51.01 51.91	25.43 25.88	50.90 51.79	26.11
59	53.03	25.86	52.92	26.10	52.80	26.33	52.69	26.56
60	53.93	26.30	53.81	26.54	53.70	26.77 Lat.	53.58 Dep	27.01 Lat
Dist	Dep.	Lat	Dep.	Lut.	Dep. 30			
18	0′		63 DEGRI		30 /		151	

i	0	0/		1:		307		437	
Ì	Dist	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	Dep.
ł	61	54.83	26.74	54-7 L	26.98	54-59	27.22	54-47	27.46
	62 63	55.73 56.64	27.18 27.62	55.61	27.41 27.86	55.49	27.66 . 28.11.	5 5.36 5 6.26	17:91 18.36
	64	57.52	28 06	57.40	28.3 t	57.98	28.56	57-15	28.81
	65	58.44	28.49	58.30	28.75	58.17	29.45	58.04	29.26 29.71
•	66 67	59.33	28.93 29.37	59.19 60.09	29.19 29.63	59.07 59.9 6	19.90	59.83	30.16
	68	66.12	29.81	60.99	30.08	60.86	30.34	60.73	30.61
	70	. 62.02 62.92	30.25 30 69	61.88	30.52 30.96	64.75 64.65	30.79 31.23	61.62	31,06 \$1.51
	71.	63.81	31.12	63.68	31.40	53.54	31.68	63.40	31.96
	72	6471	31.56	54-57	31.84	64.44	32.13.	64.29	32.41
1	73	55.61 56.51	32.00 32.44	55.47 1 66.37 1	32. 39	Б5.33. Б6.2 3	32.57 : 33.02	66.08	32.86 33 34
-	75	67.41	32.88	67.27	33.87	57.14	33.46	66.97	33.76
	76	68.34	33.32	68.16	33.61	68.02	33.91	67.87	34.21
	77 78	59.27 ·	33.75 34.19	69.06 69. 9 6	34.06 34. 50	58.91 ·	34.36 34.80	68.76 59.65	34.66 35.11
4	79	71.00	34.63	70.85	34.94	70.70	35.25	70.55	35 56
	19	71.90	35.07	91.75	35.38	71.59	35.70	71.44	36.01
	81	72.80 73.70	35.51 35.95	73.65	35.83 36. 27	7249	36. t4 36. 59	7233	36.46 36 91
7	83.	74.60	36.38	74.44	35.7.1	74-28	37.03	74.12	37.36
	84	75.50	36.84	75-34 76.23	37.05	75.17	37.48 - 37.93 '	75.01 75.90	37.81 38. 26
	86	76.40	37.26	77.13	37.59	76.46	38.37	76.80	38.71
Ì	87	77.30 78.30	37.70 38.14	78.03	38.48	17.86	38.82	77 69	39 16
	88	79.09	38,58	78.92	38.44	48.75	39.27	78.58	39. 61 40. 06
	99 94	79 99 80.89	39. 0 1	79-82	39.36 39.81	79.65 \$0.54	39.71 40.16	80.37	40.51
	91	\$1.79	39 89	81.62	40.15	81.44	40.60	81.36	40.96
	92	\$2 69	40.13	82.51	40.69	\$2.33	41.50	82.15 83.05	41.41
.:	93 94	\$3.59 \$4.49	40.77	83.41 84.31	41.13	83,23 84,12,	11.94	83.94	42.31
	99	\$5.39	41 65	85.20	42.01	85,02	42.39	84.83	42.76
Ì	96	86.28	42.08	86:10	41.46	85.91	42.83	85.73 86:62	43. 11 43.66
1	97 9 8	87.18 80.88	41.52	87.00 87.89	43.34	86.81-1 87.70	43.73	87.51.	44 14
Į	90	8 8.98	43.40	\$8.79	43.79	88 60	44-17	88.40	44.56
	-	89.88	43.84	89.69	44.11	89.49	44.62	89 30	45.01
	101 102	90.78	44 28 44.71	90.58 91.48	44.67 45.11	90.39	45.07 45 51	90.19	45.46 45.91
1	103	92.58	45.15	92.38	45.56	92.18	45.96	91.98	46 36
	104 105		49.59 46.03	93-27	46 00 46.44	93.07 93.97	46.85	92.87	46.81 47.26
- 1	106	94:37_ 95.27	46.47	95.07	46.88		47.30	94 66	47.71
I	107	96.17	46.gt	95.97	47-32	95.76	47 74	95.55	48 16
- 2	108	97.07	47:34 47 78	96,86 97.7 6	47-7 ? 48.21	96.65 97.55	48.19 48.64	96.44 97.33	48.6 t
••	1 10	97.97 98.8 ₇	48.23	98.66	48.65	98.44	49.08	98.23	49.51
	111	99.77	48.66	99.55	49.09	99-34	49-53	99.12	49.96
4	1.12	100.7	49.10	100.4	49.54 49.98	100.2	49.97 50.4 2	100.0	50.41 50.86
4	114	101.6	49.54 49.97	103.2	50.42	102.0	50.87	8.101	51.31
	115	1034	50.4.1	103.1	50 86	102.9	51.31	102.7	1.76
	116	104.3	50.85	1040	51.32	103 8	51.76 52.21	103.6	52.21
	117	104.2	51.29 51.73	104.9	51.75 52:19	104.6	52.65	104.5	52.66 ·
1	119	107.0	52.17	106 7	52.63	106.9	53.10	106.3	53 56
	120	107.9	52.60	107.6	53.07	107.4 · Dep.	53.54	107.2	54.01
	Dist.	Dep.	Lat	Dep.	Lat	30	Luc	Dep.	Lat
-1	3	0	2	4.5	DEGR			15	

U	0/		1.5	5/	3	0{	45	573
Dist	Lat	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep
	0.89	0.45	0.89	10.46	0.89	0.46	0.88	0.47
3	1.78	0.91	1.78	0.92	2.77	0.98	4.77	0.93
3	2.67	1.56	2.67	1.37	2.66	1.39	2.65	1.40 1.86
4	3.56	1.82 2 27	3.56 4.45	1 β3 2.29	3.55 4.44	2.85	3-54 442	2.33
5	4.46		5-33	2.75	5.32	2-77	5.21	2.79
7	5-35 6.24	2.72 3.18	6.22	3.21	6.21	3.23	6.19	3.26
. 8	7.13	3.63	7.11	3.66	7.10	3.69	7.08	3.72
9	8.02	4.09	8.00	4.12	7.98	4.16	7.96	.4-19
10	8.91	4.54	8.89	4.58	8.87	4.68	8.85	4.66
111	9.80	4-99	9-78 19.67	5.04	9.76 20. 64	5.08	9.73	5.18 5.59
12	10.69	5.45 5.90	11.56	5-49	21.53	5.54	1450	6.95
14	12.47	6.36	12.45	6.41	72.42	6.46	1239	6.58
15	13-37	6.81	13.34	6 87	13.31	6.93	13.47	6.98
16	14.26	7-26	14-32	7.33	14:19	7-39	1416	7-45
17	15 15	7.72	15.81	7.78	15.08	7.85	15.04	7-92 8.38
18	16.04 16.93	8.47 8.63	16.8g	8.24 8.70	15.97	8.31 8.77	15.93	8.85
20	17.82	9.08	17.78	9.16	17.74	9.24	17.70	9-81
21	18.75	9 53	18.67	9.63	18.63	9.70	18.58	9.78
22	19.60	9.99	19.56	10.07	19.51	10.16	19.47	10.34
23	20.49	10.44	20.45	10.53	20.40	10.62	20.35	10.71
24	21 38	10.90	21.34	10.99	. \$1.2g	11.08	36.34	12.17
25	23.28	11.35	23.23	11 45	22.18	11.54	32-12	11.64
26	23.17	11.80	23.11	11.90	23.06	12.01 .	23.01	12.57
27 28	24.06 24.95	12.26	24.89	12.36	23.95 . 24.84	12.47	24.78	13.04
29	25.84	13.17	25.78	12.38	85.72	13.39	25.66	13.50
30	26.73	13.62	26.67	13.74	26,61	13.85	26.55	13.97
31	27.62	14.07	27.56	14.19	27.50	14.31	27.43	14.43
32	28.51	14-53	28.45	14.65	28.38	14.78	28.32	14.99
33	29:40	14.98	29.34	15.14	29.27	15.24	79.20	15.37
34 35	30.3b	15.44	30 23	15.57	30.16	15.70	30.09	15.83 16.30
36	-	16 34	32,00	16.48	31:93	16.62	31.86	16.76
37	32.08 32.97	16.80	32.89	16.94	32.82	17.08	32 74	17 83
38	33 86	17.25	33.78	17.40	33.71	17-55	33.63	17.69
39	34.75	17.71	34.67	17.86	34/59	18.QL	34-51	18.16
40	35.64	18.16	35.56	18,32	35.48	18.47	35-40	18.62
41	36.53 -	1861	36.45	18.77	36.37	18.93	36.28	19.09
42	37.42	19.07	37.34	19.23	37,225	19.39	37/17	19.56
43 44	38.31 39. 40	19.52	38.23 39.42	19.69	38.14 39. 03	19.86 20.32	38.05 38.94	20 02 20.49
45	40.10	20.43	40.01	20.60	39.03	20.78	39.82	20.95
46	40.99	20.88	40.89	21.06	40.8Q	21.24	40.71	21.42
47	41.88	21.34	41.78	21.52	41.69	21.70	41.59	21.88
48	42.77	21.79	42.67	21.98	42.58	32.16	42.48	22.35
49 · 50	43.66	22.25	43.56	22.44 22.89	43.46	22.63	43.36	22.82
	44-55	22.70	44.45		44-35	23.09	44.25	23.28
- 51- 52	45.44	23.15 23.61	45.34 46.23	23.35 23.81	45.24	23.55	45.13 46.02	23.75 24.21
53	47.23	24.06	47.12	24.27	47.01	24.01 24.47	46.90	24.68
54	48.11	24.52	48-01	24.73	47.90	24.93	47.79	25.14
55	49.01	24 97	48.90	25.18	48.79	25 40	48 67	25.68
- 56	49.90	25.42	49.78	25.64	49.67	25.86	49.56	26.07
57	50.79	25.88	50.67	26.10	50.56	26.32	50.44	26.54
58 59	51.68	26.33 26.79	51.56	26.56 27.01	51.45	26.78	51.23	27.01
60	53.46	27.24	53.34	27.47	52.33 53. 3 2	27.24 27.70	52.21 53.10	27-47 27-94
	Dep.	Lai	Dep.	Lui.	Dep	Lat	المنهدة بيشبه	Lat.
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I E					Lat.	D-p	Lat	Dep.
1	Lat	Dep.	Lat	D-p.		28.17		28.40
61	54-85 55-84	27.69 28.15	54.83	27 93 28.39	54.11 54.99	28 63	53.98 54.87	28.87
63	56.13	28.60	56.01	28 85	55.88	29.09	55.75	29.33
4	57.02	29.06	56.90	29.30	56.77	29.55	56.64	39.80 30.26
65	57-92.		57-79.	29.76	58-54	30.01	57.52	30.73
66	58.81	29.96 30.42	58.68 59.56	30.22 30.68	59-43	30.94	59.29	31.20
68	60.59	30.87	60.45	31.14	60.32	31.40	60.18	31.66
69	61.48	31.33	61.34	31.59	61.20	31.86 32.32	61.06	32.13 32.59
70	62.37	31.78	63.12	32.05	62.48	32.78	62.83	33.06
71 72	63:26	32.69	64.01	32.51 32.97	63.86	33.25	63.72	33.52
73	.65.04	33.14	6490	33.44	64.75	33.71	64.60	33 99
74	65.93 66,83,	33.60 34.05	65.79 .66.68	33.88	65.64	34.17 34.63	65.49 66.37	34.46 34.9 2
75	67:72	34.50	67.57	34.34 34.80	67.41	35.09	67.26	35.39
76 77	68.61	34 96	68.45	35 26	68.30	. 35.55	68.14	35.85
78	69.50	35.41	69.34	35.71	69.19	36.02	69.03	36.32
79 80	70 3 9 71.28	35.87 36.33	70.23 71.12	36.47 36.63	70.07	36.48 36.94	69.91 70 80	36.78 37.25
81	72.17	36.77	7201	37.09	71 85	37.49	71.68	37.71
82	73.06.		72.90	37.55	72.73	37.86	73.57	38 18
83	73-95	37.68	73.79	38.00	73.62	38.33	73-45	38.65
84 85	74-84. 75-74		.74.68 25.57	38.46 38.92	74.51	38.79 39 25	74-34	39.11
86	-	39.04	76.46	39-38	76.28	39.71	76.11	40.04
87	77-53.		77-34	39.84	77-17	40.17	76.99	40.51
88	78-41	39.95	78.23	40 29	78.06	40.63	77.88	40 97
89 90	79.30 80.19	40.86	79.12 80.01	40 75	78.94 79.83	41.10	78.76 7 9.65	41.44
91		41.31	80.90	41.67	80.72	42.02	80.53	42 37
92	81497	41.77	81.79	42.12	81.61	42.48	81.42	42.84
93	_	42.32	82.68	42.58	82.49	42.94	82.30	43.30
94 95	83.75 84.65	43.13	\$3.57 \$4.46	43.94	83.38 84.27	43.40 43 87	83.19	43.77
96	85.54	43.58	85 35	43 96	85.15	44.33	84-96	44-70
97	86.43	44.04	86.23	44 41	\$6.04	44.79	85.84	45.16
98	87.32	44-49	87 12	44-87	86.93 87.81	45.25	86.73 87.61	45.63
99	89.10	44-9 5 45 40	88.90	45-33 45-79	\$8.70	45.71	88.50	46.56
101	89.99	45.85	89-79	46.25	89.59	46.04	89.38	47.03
108	90 88	46.31	90.68	46.70	90.48	47.10	90.27	47.49
103	91.77 92.66	46.76	91.57 92.46	47.16 47.62	91.36	47.96 48.01	91.15	47.96 48.42
104	93.56	47.67	93-35	48.08	93:14	48.48	92.92	48.89
106	94.45	148.12	94-24	48.53	94-02	48.95	93.81	49 36
107	95-34	48.58	95.12	48.99	94.91	49 41	94.69	49.82
109	96.23 97.12	49 03 49-49	96.90	49.45	95.80	49.87	95,58 96.4 6	50.29
110	98.01	49.94	97.79	50 37	97-57	50.79	97.35	51.22
111	98.90	50.39	98.68	50.82	98.46	51.25	98.23	51.68
112	99.79	50.85	99 57	51.28	99.35	51.72	99.12	52.15
113	100.7	51.30	100.5	51.74	100.2	52.18	100.0	52.61
115	107.5	51.21	102.2	52 66	102.0	53.10	101.8	53 55
816	103.4	52.66	103.1	53.11	102.9	53.56	1327	54.01
317	104.2	53 12	101.0	53-57	103.8	54.02	103.5	54-48
119	106.0	53·57 54·02	104.9	54.03 54.49	104.7	54-49 54-95	105.3	54.94 55.41
120	106.9	54.48	106.7	54-94	106.4	55.41	106.2	55.87
	Dep.	Lat.	Dep.	Lat.	Dep.	Lai	Dep.	Lit
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		4	50	DEGR	DEC			

1	0.		15	242-038	30	3	45' 1	
	Lat	Dep.	Lat.	Dep	Lat.	Dep.	راهيا.	Dep.
1	O 88	i '—I	0.88		0,88	0.48	0.88	0.48
	1.77	0.47 0.94	1.76	0.47	2.76	0.95	1.75	0.96
3	265	1.41	2.64	1.42	2.64	1.43	1.63	1-44
4	3.53	1.88	3.52	1.89	3 52	2.91	3-55	1.93
5	441	2 75	4.40	2.37	4-39	2.39	4.38 5.36	1.40 1.89
6	5.30	3 19	5.29 6.17	3.31	5.17	3-34	6.14	1.37
7 8	7 06	3 76	7.05	3.79	7.03	3.83	7.01	3.85
9	7.95 8.83	4.13 4.69	7.93	4.26	7.91	4.19	7.89	4-33 4-81
10		5.16	8.81	4-73	4.67	4.77	9 64	5.29
111	9.71	5.63	9.69	5.31	10.55	5-25	10.52	5-77
13	11.48	6.10	11:45	6.15	11-43	6.20	11:40	6 25
14	E2.36	6.57	12.33	7 10	12.30	6.68 7.16	22.27	6-73
15	13 24	7.04	13.21		13-18	7 63	13 15	7.28
16	14-13	7.51	14.09	7.57 8 QS	14-94	8.11	14.03	*-70 8.18
18	15.89	8 45	15.86	8.52	15 83	8.99	15.78	1.06
0 19	16.78	8.42	16.74	8.99	16.70	9.07	16.66	9-34
37	17 66	9 39	17.62	9.47	17.58	9:54	17.53	9.62
3.1	18,44	9 86	18 50	9.44	18.4 6 19.33	10.01	18.41	10, 10
23	20.31	10 \$5	20.26	30.89	20.21	10.97	23.16	11.06
24	21.19	11.27	11.14	11.36	31.09	11645	17,04	16.54
25	22.07	11.74	22 02	11 83	21 97	11 93	21,92	12.03
20	32 96	12.21		112 31	22.85	12.88	22.79 23.67	12.51
27	23 84	13.45	25.78 24 66	13.25	23.73 24 f I	13.36	33.07	E2.99
28 29	25 61	1361	25 55	#3 73	15 49	13 54	25.43	13.95
33	26.49	14.08	26,43	14 20	26 35	14-31	26 30	T4 43
31	27.37	14.55	47 .t	14,67	27 34	14.79	7.18	La ys
12	28.25	15.02	28.19	15.15		15 27	28.06 ·	15 39
33	29.14 30.02	15.49 15.96	29 07 19 95	15.62	29.55 29.55	15 75	29.81	15 80
34	30.90	16.43	30 83	16 57	30.76	16 70	30.69	16 %
36	31.79	16 90	31 71	17.94	31 64	17 18	31.56	17.32
37	33.67	17 37	33 59	17.51	32.52	17.65		17 80
38	33-55 34-44	17.84 18.31	33-47 34-35	17-99 18-46	33 40 34-27	18.61	33.32 34.19	18.28 18,76
39 40	35.32	18.78	35 24	18 93	35 15	1903	35.07	19 24
41	36.30	19.25	36 12	19.41	36.03	tg. 96	35 95	19.73
42	37.¢8	19.72	37 00	19.88	36.91	20.04	36.82	20.20
43		20.19		20.35		10 52	37.70 38 58	20.68
44	38.85 39 73	21.13	38.76 39.64	21,30	38 67	20.99	39 45	21.26 21.64
45 46	40 61	21 60	40.52	21.77	40 43	21.95	40.33	32.13
47	41.50	12.07	41.42	22 25	41 30	22 43	41.42	12.61
48	42.38	22.59	42.28	22.72		12 90		23 09
49	100	'13 CO 23.47	44.04	23.19	43 06 43 94	13 38 13.86	43.96	23 57 24.05
50		23.94	44 93	24 14	44.82	24 34		24 53
51		24 41	45 81	24.61	45.70	24.81		25:01 :
53	46 80	24.88	46.69	25.09	46.58	25.39	46.47	25-49
54	47.68	25.35	47-57	25.56	47 46	25 77		15.97
55	48.46	25.82		26 03	48 33	26.24	<u> </u>	26.45
56	49-45	26.76	49-33	26.51 26.98	49.21	16,72 17,70	49.97	20 94 : 17:42 :
57 58	51 21	27.23	51.09	27.45		17.68		27 90
59	52.00	27.70	51.97	17 Q3	\$1.85	28.15	\$1.73	28.38
60	52,98	28.17	52.85	18.40	58.73	28 63	52.60	28 86
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ř		Lat	Dep.	Late	Dep.	Lat.	D-p	Lat	D-
6		53.86	28.64	53-73	28.87	53.6L	29.11	53.48	24 54
1	•	5474	29.11	54.62	29.35	54-49	29.58	54.36	29.8
64	_	55. 6 3 56.51	2 9.5\$ 30.05	59.50 56.38	29.82 30.29	55-37 56 24	30.06	55.23	30.7
6	- 1	57-39	30.52	57.26	30.77	57-12	31.02	56.99	31 20
66		58:27	30.99	58.14	31.24	58.00	31.49	57 86	31.7
68		59-16	31.45 31.40	5 9.90 °	31.71	5 8.88 59.7 6	31 97	58.74	32./, 32.
64	4	60:04 60:92	32.39	69.78	32.66	60.64	3292	60.49	33.41
70	•	18.10	32.86	61.66	33.13	61.52	33.40	61 37	33.6
71		62.69	33.33	62.54	33.61	62.40	33.88	62.25	34.1,
. 7		63.57	33.80 34.97	63.42 6435	34.08 34.55	63.27 64.15	34.3 6 34.83	63.13	34 6
73		65.34	34.74	69.19	35.03	65.03	35.31	64.88	35-39
7		66.22	35.81	66.07	3550	65.91	35.79	65.75	36.07
7		67.10	35.68	66.95	35 97	66.79	36.26	66.63	36.56
77		67.99 68.87	36.15 36.62	67.83 68.74	36.45 36.92	67.67 68.55	36.74 37.83	67.51 68.38	37.04 37.52
79		69.75	37.69	69.59	37-59	69 43	37.70	69.26	38.00
80	51	7 0.64	37.56	70.47.	37.87.	70.31	38.17	70.14	38 48
8		71.54	38.03	7 - 35	38.34 38.81	75.18	38.65	73 Ot	38.96
8:		72.40	38.50 38.97	7423	39.29	72.06	39.13 39.60	7 m 8 9 7 m 7 7	39·44 39.92
84	4	74.57	39.44	73-99	39 76	73.82	40.48	73 65	40.40
8	-	-	39.91	74.88	40 23	74.70	40 56		40.88
80		75.93 76.82	40.37 40.84	75.76	40.71	75.58 76.46	41.51	75.40 76.28	41.85
8	_	77.70	41.38	77.52	41.65	77-34	41.99	77.15	42.33
84	9	78.58	41.78		42.13	78-25	42.47	78.03	42.81
90		79.47	42.25	79 28	42.60	79.09	42.94	78.91	43.29
9:		80.35	42 72 43.19	80,16 81,34	43 Q7 43:55	79.97 80.85	43.42 ⁻	79 78 80.66	43·77 44·25
9:		8211	43.66	81.92	44.02	81.73	44 38	81.54	44 7.3
94	4	83,00	44-13	82,80	44.49	82.61	44-85	82.41	45.21
9	-	83.88	44 60	83.68	44.97	83.49	45.81	83,29	46.17
90	1	84. 76 85.65	45.07 45.54	84.57 85.45	45.44 45.91	84.37	46.38	85,04	46.66
9		:86.53	46 01	86.33	46.39	86.12	46.76	85.93	47-14
99		87·41 88.29	46.48 46.95	88.09	46.86 47.33	87.00 87.88	47- 24 47- 72	86,80 87.67	47.62 48.10
10	-	89.18	47 42	88.97	47 81	88.76	48.16	88.55	48.58
10			47.89	89.85	48.18	89.64	48.67	89143	49.06
10	- 1		48.36	90.73	48.75	90.52	49.15	92.30	49.54
10	•	91. 83 92.71	48.82 49.39	91161	49.23. 49.70	91.40	49. 62 50.10	91.18	50.02
100	-	93.59	49.76	- 93.37	50.1%	93.15	50.58	92.93	50.98
10	7	94.48	50.23	94.26	50.85	94.03	51.96	93.81	51.47
10		95.36	50.70 51 27	95.14	51.42	94.91	51.53 52.01	94.69 95.56	51.95 52.43
10	- 1	97.12	51 64	96.90	53.07	96.67	52.49	96.44	5291
11	;	98.01	52. ti	97.78	52.54	97-55	52.96	97-32	53-39
1 2		98.89	52.58	98.66	53:01	98.43	53 44	98.19	53.87
111	٠,	99.77 100.7	53.52	9 9 -54 100.4	53.49 53.96	99.31	53.92 54.40	99.07 99.95	54.35 54.83
11	•	101.5	53-99	101.3	54.43	1.601	54.87	100.8	22-3T
11		102.4	54.46	100.3	54.90	104.9	55-35	101.7	55.79
11	_	109.3	54.93	103.1	55.38	102.8	55.83	102.6	56.28 56.76
111		104.1	55.40	104.8	56.33	103.7	56.30 56.78	104.3	57.24
120	0	106.0	56.34	105.7	56.80	105.5	57.26	105,2	57.72
1		Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.	Lat
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				61	DEGR	W.P.			

1 0	0/		1.5	7	30	4	43	,
Di A	Lat	Dep.	Lat	Dep.	Lat.	Bep.	Last.	Dep.
	0.87	0.45	0.87	0.49	0.87	0.49	0.87	0 50
1	1.75	0.97	1.75	O.g8	1.74	0.93	1.74	3.99
3	3.61	1-45	3-49	1-67	2.61 3.48	1.48	3-47	1.49
\$	3.90 4-37	1.94 2.43	436	2.44	435	2.46	4-34	2 48
6	5.85	2-91	5:94	293	5.33	2.95	5.88	2.98
7	6.13	3 39	8.11	3-48	6.09	3-46	6.08	3-47
1	7.00	3-88 4-36	7.85	3.91 4.40	7 85	3-94 4-43	9.95 , 7.81	3-97
10	9.87 8.75	4.85	8.73	4 %	1 70	491	1.68	4 96
11	9.63	5 33	9.60	5-37	9 57	5-48	9-55	5-45
13	10.50	5.82	10.47	5.86	10.44	5-97	10.48	5-95
13	21.37	6.30	21.34 12.31	6.4	14.31 12,18	6.40 6.50	19-15	6.45 6.95
13	13.12.	7.27	13.09	7-33	13 06	7.39	13.01	7-44
76	13 99	7.76	13.96	7.83	13-91	7.88	13.89	7.44
17	14.87	8.84	14.83	8.32	14.80	8.37	14-74	44
18	15 74	8.73	14.70	8.80 9.38	15.67 16 54	9.36 9.36	16.50	1-93 9-43
19	17-49	9-31	26.58 17.45	9.77	17 41	9.85	17.19	9.95
31	18.37	10.18	1841	10 16	18.06	10.34	1843	10.43
22	19.54	10.69	19.19	10.75	19-15	10.83	19-10	10.93
25	10.11	11,64	1007	11:54	20.02	11.83	19-97	16,61
24 25	30.99 31.87	18,13	50.94 51.81	13.22	21.76	J2-31	31.70	13.41
25	32.74	62 6L	41.61	1170	33.63	13.50	32.67	11.90
27	23 61	13.09	23 56	13.19	13.50	13-30	23-44	13-40
25	24.49	13.57	84-43	13.68 14.17	24-37	13.79 14.28	24.36 25.18	14.59
10	26.19	14-00 14-5 <u>4</u>	25.30	14.66	26.11	14-77	26 05	14 89
1	37.11	15.03	87.05	15.15	26.98	15.27	26,91	15.38
15	47-99	15.54	17-91	15 64	27.85	15 76		15.88
33	38.86	16.00 ·	28.79 29,66	16.13	28 72 20-59	16.74 :		16.38
34	29.74 30.6c	16.97	10.54	17.10	30 46	17.83	30.79	17-37
36	31-49	17-45	11:41	17-59	31.33	17 73	31.36	17 84
1 27	31.26	17-94	lrag	18.08	32.30	18.13	_	18.36 18.56
1 !! 1		68.42 48.91	31.15 14.03	18.57 19.0 0	33.07 33.94	18.71 19 80	33.56	19-35
39 40	14.98	19-19	34 90	19-54		19.73	34-73	19.85
41		19.\$8	35-77	10.01	35.68	30.19		20.34
42	34.73	20.36	36.64	20.52	36.55	20 62	36 46	20.14
121	37.61 18.48	10.85 11.33	37-50 11-39	21.9L 21.50	37 43 18.30	21.67	37-33 38-90	31.63
44	39.36	21.12	39.26	11.99	39.17	22.16	39.07	12.33
46	40.13	11.30	40.13	22 45	40.04	22.65	39-94	33.83
47	41-11	11.79	41.01	23.97	40/91	23 14 23.64	40.81	23.32 23.82
1 48		29.87 23.76	41,48 -	25-45 25 94	41.78	24.13	42-54	24 31
49 50	43-73	1414	43.62	24-43	43.52	24 63	43.41	44.61
31		24 73	44.50	14-93	44-39	25.11	44.23	35.34
52	45.48	25.22	45-37	25-41 -	45.26	25.62	45.15	25.80 26.30
133	46.35	35.69 26.18	46.54 47.11	25.90 16.39	46.13	26.10 26.59		36.50
. 54 55	47.83 48.10	16:66	47 99	16.87	47.87	27,08	47-75	17.19
33		27 15	48.86	17.36	48.74	27.58	48.61	27 79
57	49.85	27 63	49-73	17 85	49.61	18 07	49-49	23.25 11.75
50	50.73	18.11 18.60	50,60	28.34 28.83	50-48 51-35	18 56 : 19-05 :		38.78 39.38
59	51.60 52.48	19.09	5148 52.35	29-32	52.22	29-55	52.09	19.77
	Dep	Late	Dep	Lat	Dep.	Lat	Dep.	Loss
13.			4	,	30	<i>,</i>	1.	77

	. 0'.		13	51	30'		451	
Dist.	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Lat	Dep.
.61	53-35	29-57	53.23	29.81	53.09	30.04	52.90	30.27
66	54-28	30.06	54.09	30.59	53.96	30.53	53.83	30.77
63 64	55.10	30.54	54-97	30.78	54.83	31.02	54.70	31.26
65	55.9 8 56 8 5	31.03	55.84	31.27 31.76	55.70 56.57	31.52 32:01	55.56 56.43	31.76 32.25
66	57-72	32.00	57.58	32.25	57.44	32.50	57-30	32.75
67	58.60	32.48	58:46	32.74	58 38	32.99	58.17	33.25
68	59.47 60 35	32-97 33-45	59-33	33.23 33.71	59.18	33.48 33.48	59.04	33.74 3 4.24
70	61.23	33.94	61.07	34.20	60.92	34-47	59.91 60.77	34-74
71	62.10	34-42	.61.95	34.69	61,80	34.96	61.64	35.23
72	62.97	34-91	62.82	35.18	68.67	35-45	62.51	35.73
73	63:85 64-72	35.39 35.88	63.69 -64-56	35.67 36.16	63.54°	35.95 36.44	63.38 64.25	36.22 36.72
74 75	65.60	36.36	65-44	36.65	65.28	36.93	65.11	37 22
76	66.47	36.85	66.31.	37-14	66.15	37-42	65.98	37-71
77	67.35	37.33	67.18	37.62	67.02	37.92	66 85	38.21
78.	68.22 69 09	37.82 38.30	68.05. 68.93	38.51 38.60	67.89 68.76	38.41 38.90	67.78 68 59	38.70 39. 2 0
79 ·	69.97	38.78	69.80	39.09	69.63	39.39	69.46	39.70
81	70.84	39.27	70.67	39.58	70.50	39.89	70.32	40.19
80	7272	39.75	71.54	40.07	71.37	40 38	71.19	40.69
83 84	72.59	40.24	73.43 73.29	40.56 41.04	73.34	40.87 41.36	72.06	41.19 41.68
85	73-47 74-34	40.72 41.21	74.16	41.53	73.98	41.86	73.80	42.18
86	75.22	41.69	75.03	42.02	74.85	42.35	74.67	42.67
87	76.09	42.18	75.91	42.51	75.72	42.84	75-53	43.17
88 89	76.97 77.84	42.66	76.78	43.49	76.59 7 7.4 6	43 5 3 ·	76.40 ·	43.67 44.16
90	78.72.	43.63	78.52	43.98	78.33	44.32	78.14	44.66
91	79-59	44-12	79.40	44-46	79.20	44.81	79.01	45.16
92	80 47	44.60	80.27	44-95	80.07	45.90	79.87	45.65
93 94	81.34	45.09	81.14 82.01	45- 44 45-93	80.94 81.81	45.80 46.29	8074 81.61	46.15 46.64
95	83.09	46.06	8289	46.42	8268	46.78	8248	47.84
96	83.96	46.54	83:76	46-91	83.55	47.27	83:35	47.64
97	84.84	47.03	84.63	47.40	84.42	47.77	84.22	48.13
98 99	85.71	47.51 48.00	85.50 86.38	47 88 48.37	85.29 86,17	48.26	85.08 : 85-95	48.67 49.13
100	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.68
101	88,34	48.97	88.12	49-35	87-91	49-73	87.69	50.12
103	89.21	49.45	88.99	49.84	88.78 89.65	50.23	88.56	50.61
103	90.00	49.94	89.87 90.74	50.83	90.53	50.72	89.42 90.89	51.11
105	91.84	10.02	97.61	58.31	91-39	51 70	97.16	52.10
106	92.71	51.39	92.48	51.79	92 26	52.20	9203	52.60
107	93.58	51.87	93.36	52.28	93.13 94.00	52.69	92.90	53. to
109	94.46 95.33	52.36	94.23	52.77 53.26	94.87	53.18 53.67	93.77 94.63	53.59
110	96.21	53.33	95.97	53 75	.95.74	54.17	95.50	54.58
111	97.08	53.81	96.85	54.24	96.61	54.66	96.37	55.08
712 713.	97.96	54.30	97.72	54-73	97.48	55.15	97-24	55.58
714	98.83 99.71	54.78 55.27	98.55 99.46	55.21 55.70	98.35 99 22	55.64 56. 24	98-11 98-97	5 6.07
415	100.6.	55.75	100.3	56.19	100.1	56.63	99.84	57.06
116	101.5	56.24	101.2	56.68	0.101	57-13	100.7	57.56
317 118	102.3	56.72	102.1	57.17	102.7	57.61	101.6	58.06
119	103.2	57 31 57. 69	103.8	57.66 58.15	103.6	58.11 58.60	103.4	58.5 5 59.0 5
1 20	105.0	58.18	1047	58.63	1044	59.09	104.2	59-55
zi.	Dep.	Lat.	Dep.	LAL	Dep.	Lut.	De 1.	Lat.
Dia	Ú		451		30/		15	
• ••••••••••••••••••••••••••••••••••••			60	DEGR	PPC			-

	0/		15	1	30)'	45	
Die	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
	0.87	0.50	0.86	0.50	0.86	0.51	0.86	0.51
2	1-73	1,00	1.73	1,01	1.78	1.02	1.74	1.02
3	2.60	1.50	2.59	151	2.58	1.58	2.58	1.53
4	3.46	2.0C	3.46	2.02	J:45	2.03	3.44	2.05
5_	4-33	2.50	4-31	2.52	4.31	2 54	4.30	3.07
. 6	.5.29 6.0 6	3.00 3.50	6.0.8	3.08 3.53	5.17 • 6.03	3.05 3.55	5.16 603	3.58
7 8	6.93	4.00	6.94	4.03	4.89	4.06	6.88	4.09
9	7.79	4.50	7.77	4-53	7.75	4.57	7.73	4.60
10	8.66	500	8.64	5.04	8.61	5 08	8.59	5,81
11	9.53	5.50 6.00	9.50	5.54 6.05	9.48 - 16.34	5.58	945	5.62 6.24
13	10.39 11.26	6 50	10.37	6.55	11.20	6 60	1 17	6.65
14	12-12	7.00	11.04	765	11:06	7-11	1403	7-16
15	12.99	7.5G	12.96	7.5	:15.93	7.51	11:69	7.67
16	13.86	8.00	13.84	8.06	43.79	8.12	13.75	8.18
17	1472	8.50	1469	9.07	1465 35.51	8 6 ₃	14.65	8.69 9.40.
18	16.45	9.00 9.50	15.55	9.57	16 37	9.64	16.33	9.71
20	1732	10.00	17.28	10.08	17.23	10.15	17.19	10 23
21	18.19	10.50	18 14	10.58	48.09	10.66	18.04-	10.74
32	19.05	11.00	19.90	11.08	18.96	11.67	18.91	18.25
23	19.92	1150	19.87	11.50	19.82	12.48	19.77	11.75
25	21 65	12.50	21.60	12.59	21.54	12.69	11.49	14.78
26	22.52	13.00	22.46	13.10	22.40	13.20	82 34	13.29
27	23.38	13.50	23.32	13.60	. 23.26	13.70	23.20	13 80
28	24.25	14.00	24.19	14.81	24 15	14.71	14.06	14.83
39 30	25.98	14.50	25 05 25.92	14.61	24 99	15.23	23 92 25.78	15.34
31	26.85	15.50	26.78	15.62	26.71	15.73	R6.64	15.85
33	27.71	16.00	27.64	16.13	27.57	16.4	\$7.50	16 36
33	28,58	16 50	28-51	16.64	28.43	16.75	18.36	16.87
34	29.44 30.31	17.00	29.57 30.23	17.15	29.30 30 16	17.26	30.08	17.38
35	31.18	18.00	31.10	18.14	31.02	18.27	20.04	18.41
37	32.04	18.50	31.96	18 64	31.88	18.78	31.80	18.92
38	3291	19.00	32.83	19. 14	32.74	19.39	32166	19.43
39	33-77	19.50	33.69.	19.65	33.60	19.79	33.52	19.94 20.45
40	34 64	20.00	34-55	20.15	34-47	20.81	34-38	20.96
41 42	35.51 36.37	20.50 21.00	35.42 36.28	20.65.	35.33	21 32	35.24	21.47
43	37.24	21.50	37.14	21.66	37.05	21.82	16.95	21.99
44	38.11	22.00	38.01	22.17	37 91	22.33	\$7.81	22.50
45	38.97	22.50	38.87	22.67	38.77	22.84	38,67	23.01
46	3 9.84 4 0.70	23.00 23.50	39-74 40.60	23.17 23.68	39.63 40.50	23.35	19.53 40.39	23.52
47	41 57	24.00	41-46	24.18	41.36	24.36	41.25	24-54
49	42.44	24.50	42 33	24.68	42.22	24.87	42.11	25.05
50	43.30	25.00	43.19	25.19	43.08	25.38	42.97	25.50
51	44.17	25 50	44.06	25.69	43.94	25.88 26.39	43.83 44 -69	26.99
53	45.03 45.90	26.00 26.50	44.92 45.78	26.20 26.70	44-80	26.90	45.55	27.50
54	46.77	27.00	46.65	27.20	46 53	27.41	46.41	27.61
55	47.63	27.50	47 51	27.71	47-39	27.91	47.27	28. 72
56	48.50	28.00	48.37	28 21	48.25	28.42	48.13	28.63
, 57 58	49.36	28.50	49.24	28.72 29.22	49.11 49.97	28.93 29.44	48.94	29.14 29.65
5 8 5 9	50.23	29.00 29.50	50.10	29.73	50.84	29.94	50 70	30.17
60	51.96	30.00	51.83	30 23	51.70	30 45	51.50	30.68
ن	Dep.	lat.	Dep.	Lat .	Dep.	Lat	Dep.	Lat.
Dist.	01		4:	,	30	'	1.	
-			59	DEGR	EES.			

1 7.	0)'	1.	51	3()'	4	;•
] #	Lat.	Dep	Lat.	Dep.	Lat	Dep.	Lat	Dep.
61	52.83	30.50	52.69	30.73	52.56	30.96	52.42	31.19
62	53.69	31.00	53.96	31.23	53.42	31.47	53.28	31.70
63	54.56	31.50	54.42	31.74	54.28	31.97	55.00	32.21 32.72
64 65	55.43 56.29	32.50	55.29 56.15	32-75	5601	32.99	55.86	33.23
66			57.01	33.25	56.87	33.50	56 72	33.75
67	57.16	33.00 33.50	57.88	33.75	57 73	34.01	57.58	34.26
68	-58.89	34.00	58.74	34.26	58.59	34-51	28-44	34-77
69	59 76	34.50	59.60	34.76	59 45	35 02	59. 30	35.28
70	60.62	35.00	60.47	35.16	60.31	35.58	61.02	35 79
71	61.49	35.50	61.33	35.77 36.27	61.18	36.04 36.54	61.88	36.30 36.81
72 73	62.35 63.22	36.00 36.50	63.06	36.78	62.90	37.05	62.74	37-32
74	64:09	37.00	63.93	37.28	63 76	37.56		37.84
75	64 95	37.50	64.79	37.78	64.62	38.07	64.46	38.35
76	65.82	38.00	65.65	38.29	65.48	38.57	65.31	38.86
77	66.68	38,50	66.52	38.79	66.35	39.08	66.17 67.03	39 37 39.88
78	67 55	39.00	67.38 68.24	39 2 9 39.80	68.07	39.59 40 LO	67.89	40.39
79 80	65.42 69.28	39.50 40 00	69.31	40.30	68.93	40.60	68.75	40 90
8	70.15	40.50	69.97	40.81	69.79	41.11	69.61	41.41
82	71.01	41.00	70.83	41.31	70.65	4862	70.47	41.93
83	71.88	41.50	71.70	41.81	71 54 .	42.13		42-44
4	72.75	42.00	72.56	42.82	72.38	42 63	72.19	42.95 43.46
85	73.61	42.50	73.43		74.10	43.65	-	43.97
86	74 48	43.00	74.29 75.15	43.32 43.83	74.96	44-16		44-48
87 88	75.34 76.21	43.50 44.00	76.02	44-33	75.82	44.66	75.63	44-99
89	77.08	44.50	76.88	44 84	76.69	45.17		45.51
90	77-94	45.00	77.75	45.34	77-55	45.68	77-35	46 92
91	78.81	45.50	78.61	45.84	78.41	46.19	78.21	46.53
Q 2	79.67	46.00	79.47	46.35 46 85	79-27 80-13	46.69 47.20	79.07 79 92	47.04
93	\$0.54 \$1.41	46.50	80.34 81.30	47.35	80.99	47.71	80.78	48.06
95	82.27	47.50	82.06	47.86	81.85	48.32	81.64	48.57
96	83.14	48 00	83.93	48.36	82.72	48.72	82.50	49.08
97	84.00	48.50	83.79	48.87	83.58	49.33	85.36	49.60
98	84.87	40.00	84.66	49-37	84-44 - 85-30	49.74	84.22 85.08	50.11
99	\$5.74 \$6.60	49.50 50.00	85.52 86.38	49 87 50 38	86 16	50.75	85.94	58.43
00]	87.25	50.88	87 02	51 26	\$6.85	51.64
101	87.47 88.33	\$0.50	88.11	51.38	87 89	5477	87 66	52.15
103	89.20	51.90	88.97	51 89	88.75	52.28	88.52	52 66
104	90.07	91.00	\$9.84	52.39	8981	54.78	89.38 90.24	53.69
105	90 93	53 50	90.70	52.90	90.47	53.80	<u> </u>	-
126	91.80	53.00	91.57	53.40 53. 9 0	91.33	54.31	91.10	54.20 54.71
107	92 66 93.53	53 50 54.00	94.43	54 41	93 06	54.81	9282	55.23
109	94 40	54.50	94.16	54.91	93.92	55.32	93.68	55.73
110	95.26	55.00	95.02	55.42	94.78	55.83	94 53	56.24
111	96 13	55.50	95.89	55.92	95.64	56.54	95.39	56.75
112	96.99	56.00	96.75	56.42	96.50*	57.35	90.25	57.74
113	97.86 98.73	56.50 57.00	97 61 98.48	5 0.93 5 7.43	98.23	57.86	97.97	58.20
115	99.59	52.50	99.34	57.93	99 09	58.37	98.83	58.89
116	100.5	58.00	100.2	58.44	99-95	58.87	99.69	59.31
117	101.3	58.50	101.1	58.94	100.8	59.38	100.6	59.88
118	103.2	59.00	1049	59-45	104.7	59. 89	105.4	60.84
1119	103.1	59.90	102.8	59.95 60 45	10a.5	60.90	102.3	61.30
120		63.00		上記	Dep.	Lat	Dep	Lat
Diet	Dep.	Rat	Dep.		30			51
1 4	. 0		4:	TOPO DA			·	

I NEWKERS.

	<u>C</u>	. 0/		15	1	30)/	4	5'
	Dist.	Lat.	Dep	Lat.	Dep.	Lat	De .	Läl.	Dep
-	-	0.86	0.51	0.85	0.52	0.85	0.52	0.85	0.53
ł	2 }	1.71	1.03	1.71	1.04	1.71	1.04	1.70	1.05
ł	3	2.57	1.55 2.06	2.56 3.42	1.56 2.08	2.56 3.41	1.57 2.09	2.55 3.40	1.5¢ 2.10
I	4 5	3·43 4·29	2.58	4.27	2.59	4.26	2.61	4.25	2.63
	6	5.14	3.09	5-13	3.11	5.12	3 13	510	3.16
}	7	6.00	3.61	5.48	3.63	5-97	3.66	5.95	3.68 4.21
	8	6.\$6 7.71	4.12 4.64	6.84 7.69	4.67	6.82° 7.67	4.18	6.80 7.65	4-74
1,	9	8.57	5.15	8 55	5.19	8.53	5.22	8.50	5 26
i	11	9.43	5.67	9.40	5-71	9 38	5-75	9-35	5.79
	12	10.29	6.18	10.26	6.23	10.23	6.27	10.20	6 31 6.84
	13	1 f. 14 12.00	6.70 7 24	11.11	6.74 7.26	11.08. 11.94	6.79 7.32	11.05	7-37
-	14	12.86	7.73	13.82	7.78	12 79	7-84	12.76	7.89
1	16	13.71	8 24	13.68	8.30	13.64	8.36	13.61	8.42
1	17	14-57	8.76	1453	8. 82.	14.49	8.88	14.46	8.95
	18	15.43 1 6.2 9	9.27 9.79	15.39 16.24	9-34 9-86	15.35. 1 6.2 0	9.40	15.31	9-47 10.00
_	19 20	17.14	10.30	17.10	10.38	17.05	10.45	17.01	10.52
	2!	18.00	10.82.	17.95	10.89	17.91	10-97	17.86	11.05
	22	18.86	11.33*	18.81	11.41	18.76 19 61	11.50	18.71	11.58
	25 24	19.71 20 57	11.85	20.52	13.45	20 46	12.54	20.41	12 63
1	24	21 43	12 88	21 37	12.97	21.32	13.06	21.26	13.16
	26	22.29	13.39	22.23	13.49	22 17	13.59	22,11	13.68
_	27	23.14	13.91	23.08	14.01	23.02 23.87	14.63	22.96 23.81	14-21
	18 29	· 24.00 24.86	14.43	23.94 24.79	14.53 15.04 .		15.15	24.66	15.26
	30	25.71	15.45	25.65	15.56	25.58	15.68	25.51	15.79
	31	26 57	15.97	26 50	16.08	26.43	16 20	26.36	16.31
	32	27.43	16.48	27.36 28.21	16.60	27.28 28.14.	16.72 17.24	27.21 28.06	16.84 17.37
	33 34	28.29 29.14	17 00	29.07	17.64	28.99	17.77	28.91	17.89
	35	30.00	18.03	29.92	18.16	29.84	18.29	19.76	18.42
	36	30.86	18.54	30.78	18 68	30.70	18.81	30.61	18.94
	37 38	31.72	19.06 19.57	31.63 32-49	19.19	31.55	19.33	31.46	19.47 20.00
	39	32.57 33.43	20.09	\$3-34	20.23	33-25	20.38	33.16	20.52
	10	. 34.29	20.60	34.20	20.75	. 34-11	20.90	34.01	21.05
	41	35.14	21.12	35-05	21.27	34.96	21.42	34-86	21.57
	42 43	36.86	21.63 °	35.91	21.79 22 3 t	36: 66	21.94	36.57	22.63
	44	37.72	22.66	37.52	22.83	37-52	22.99	.37 42	23.15
~	45	38.57	23.1%	38.47	23.34	38.37	23.51	38.27	23.68
	46	39-43	23.69	39-33 40.18	23.86 24 38	39,22 40.07.	24.03 24.56	39.12	24.21 24.73
	47• 48	40.29	24.21 24.72	41.04	24 90	40.07.	25.08	40.82	25.26
] 4	49	4200	25.24	41.89	25.42	41.78	25.60	41.67	25.78
	40	42.86	25.75	42.75	25.94	42.63	26.12	42.52	26.31
	51 52	43-72 44-57	26.27 26.78	43.60 44.46	26.46 26.98	43.48 44.34	26.65 27.17	43·37 44-22	27.36
	33	45.43	27.30	45.31	27.50	45.19	27.69	45.07	27.89
	\$4 \$5	46.29	27.81	46.17	28.01	46.04	28.21	45.92	28.42
_	_	47.14	28,33	47.02	28.53	46 90	28.74	46.77	28.94
	56	48.86	28.84 29. 56	47.88· 48.73.	29.05 29.57	47.75 48.60	29.26 29.78	47.62 48.47	29.47 29.99
	58	49.74	29.87	49.58	30.09	49-45	30.30	49.32	30.52
	59	50.57	30.39	50-44	30.61	.50.31	30 83	50.17	31.05
-	50	51:43	30.90	51.29	31.13	51.16 Den	31.35 Lat	51.02 Den	31.57 Lat.
	tist.	1)ep.	Lat.	Dep.	Lat.	Dep. 30		Dep.	
Ť	<u> </u>		}/	45	DEGR		, - - , - , - , - , - , - , - , - , - ,	-	

1 5	0/		1.5	1	3	0'	45'	
Diat	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat	Dep.
61	52.29	31.42	52.15	31.65	52.01	31.87	51.87	32.10
62	53.14	31.93	53.86	32 16 34.68	52.86	32.39. 32.92	52.72	32.63 33.55
63	54.00°	32 45 32.96	54.71	33.20	53.72 54 57	33.44	54.42	33.68
65	55.72	33.48	\$5-57	33 72	55.42	33.96	55 27	34.20
66	56.57	33.99	56.42	34.24	56.27	34.48	56.12	34.73
67	\$7.43 \$8.29	34.51	57.28	34.76 35.88	57.13 57.98	35.53	56.98 57.82	3 5.25
69	59 14	35.04 35.54	58.99	35.80	58.83	36.05	58.67	36.3m
70	60.00	36.05	59.84	36.31	59.68	36.57	59.52	36 S#
. 71	60 86	36 57	60.70	36.83	60 54	37.10	60 37	37.36
72	61.72 62 57	37.60	61.55	37.35 37.87	61.39	37.62 38.14	61.23	37.8g 38.41
73 74	63-43	38.11	63.26	38.39	63.50	38 66	62.93	38.94
75	64.29	38 63	64:12	38.91	63.95	39.19	63.78	39.47
76	65:14	39.14	64.97	39.43	64.80	39.71	64.63	39.99
77	66.00 66.86	39 66 4 9 .17	65.83 66.68	39.95 40.46	65.65 66°51	40.23 40.75	66 33	40 53. 41.04
78.	67.72	40.69	67.54	42.98	67.36	41.28	67.18	41.57
80	68.57	41.20	68.39	41.50	68.21	41.80	68.03	41.10
8:	69 43	41.72	69.25	42.02	69.06	44.32	68.88	42.62
82	70.29	42.33	10.10	42 54	69:92	42.84	69.73	43 15
83	71.14	42.75 43.26	70.96	43.58 43-58	70.77 71.62	43-37 43-89	70.58	43.68 44. 20
84	72 86	43 78	72.67	44.10		44.41		44.73
86	73-72	44.49	73.52	44.61		44.93		45.25
. 87	74.57	44.81	74 38	45.13	74.18	45.46	73-98	45.78
88.	75.43	45.32	75.23	45.65		45.98		46.83
89	76.29	45.84 46 35	76.09	46.17 46.69	75.89	46.50 47 02	75.68 76.53	47.36
90	78.00	46-87	77.80	47.25	77.59	47 55	77.38	47.89
91	78.86	47-38	78.65	47.73		48.07	178,23	18.45
93	79.72	47.90	179-51	48.25	7930	48.59	-	48.94
94	80.58 81.43\	48.41 48.93	81.22	48.76 49.28	80,15	49.11 49.64 -	79.93 :80.78	4 9.47 4 9. 99
95	82.29	49 44	82:07	49 80		50.16	81.63	50.52
96 97.	83.15	49.96	82.93	50 32	82.71	50.68	82.48	51.04
98	84.00	50.47	83.78	50.84	:83 56.	51.20	83.33	51.57.
99	84.86 85.72	50.99 51. 5 0	84.64 .85.49	51.36	84.41 85.26	51 73	85.04	52.62
100	86.57	52.02	86.35	52 40		52.77	.85.89	53.15
101	87.43	58.53	47.20	52.91		53.29	-86.74	53.67
103	88.29	53.05	\$8.56	53.43	87 82	53 82	§7-59.	54.30
404	89.15	5 3.50 54.08	80.77	53.95	8816 7 8 9-53	54- 3 4 54.86	-88-44' 89 29	54 73
105	90.00		90.62	54-47	90.38	55.38	90.14	55.78
105	90.86	54.59 5 5.1 1	91.48	54 99 ·	91.23	[5 5 .94	90.99	56.30
128	92.57	55.62	92.33	56.03	92:09	50.43	91.84	56.83
109	93.43	56.14	93.19	56.55	92,94	56.95	92.69	57.36.
110	94.29	56.65	94.04	57.06	93.79	57.47	93.54	57.88
111	95.15	57-17 57. 68	94-90	58.10	95.50	1	94·39 95·24,	58.94
113	96.86	58.20	96.61	,8.62	96 35	59.04	96.09	59.46
114	97.72	58.71	97.46	59.14	97.20	59.56	96.94	59.99
115	98.57	59.43	98.31	59.66	98.05	60.09	97.79	60.51
116	99.43 100.3	59.74 62.36	994J7 100.0	60. r 8 60. 70	98.91 9976	60.64	-98-64	61.57
118	_	60.77	100.0	61.22	109.6			62 09
119	102.0	68.19	101.7	61.73	•	62.18	101.2	64.62
120	102.9	61.80	102.6	62.25	1013	62.70	102.0	63.15
استساء					11		111	4.
Dist	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	<u>Dep</u>	Lat.

12:	0'		157		30		4.7	
4	Lat.	Dèp	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.85	0.53	0.85	0.53	0.84	6.54	0.84	0.54
] =	1.70	1.06	1,69	1.07	1.69	1.07	1,68	1.08
3	2.54	1.59	2.54	1.60	2,53	1.61	2.52	1.62 2.16
1 :	3-39	2.12 2.65	3. 3 8 4. 25	2.13	3 37 4.22	2.15	3.36 4.21	2.70
-5	4.24	3.18		3.20		3.22	5.05	3.25
7	5.09 5.94	3.71	5.07 \ 5.92	3.74	5.06	3.76	5.89	3-79
2	6 78	4-34	6.77	427	6.75	4.30	6.73	4-33
•	7.63	4-77	7.61	4.80	7.59	4.84	7.57	4.87
10	8.48	5.30	8.46	5.34	8-43	5.37	8.41	5.48
111	9.33	5.83	9.30	5.87	9.28	5.91	9.35	5.95
12	10.18	6.36	10.85	6.40	10,12 10.96	6.45 6. 98	10.09	7.03
14	11.87	7.42	14.64	7.47	11.81	7.52	11.77	7.57
15	12.72	7.95	12.69	8.00	12.65	8.04	12.62	8.11
16	13.57	8.48	13.53	8.54	13-49	8.60	13-46	8.66
177	14.42	9.02	14.38	9.07	14.34	9.13	14.30	9.20
18	15.26	9-54	15.22	9.61	15.18	9.67	15.84	9.74
19 20	16.31 16.36	10.07	16.91	10.14	16.02	10.31	15.98	10.82
	-			11.21		11.28	17.66	11.36
31	17.81	11.13	17.76	11.74	17 74	11.82	18.50	11.90
23	19.51	14.19	19 45	12.23	19.40	12.36	19.34	12.44
. 24	20.35	12.72	20.30	12.81.	20.34	12.90	10.18	12.98
25	21.20	13.25	21 14	13.34	21.08	13.43	21.03	13.53
26	22 05	13.78	21.99	13.87	21.93	13.97	21.87	14.07
27	22 90 23.75	14.31	22.8 3 23.68	14-48	22.77 23.61	14.51	22-71. 23-55	14.61
29	24.59	15.37	24-53	15-47	24.46	15.58	14 39	15.69
30	25.44	15.90	25.37	16.01	25.30	16.12	45-23	16.23
31	26.29	16.43	26.22	16.54	26 15	16.66	26.07	16.77
32	27.14	16.96	27.06	17.05	26.99	17.19	26.91	17.31
33	27.99	17.49	27.9L	17.61	27.83	18.27	47.75 48,60	17.85
34 35	28.83 29.68	18.02	28.75	18.14	28.68 29.52	18.81	29-44	18.93
36	30.53	19.08	30.45	19.21	30.36	19.34	30.28	19.48
37	31.38	19.61	31.29	19.74	31.24	19.88	31.12	20.02
38	32.23	20.14	32 14	20.28	32.05	20 43	31.96	20.56
390	33.07	20.67	\$2.98	20.81	32.89	20.95	32.80	21.10
40	33.92	21.20	33.83	21.34	33-74	21.49	33.64	21.64
41	3477	21.73	34.67	21.88	34.58	22.03	34 48	22.18
42	35 62 36.47	22.26 22.79	35.52	23.41	35 42 36.27	23 57	35.32 36.16	23.26
44	37.31	23 32	37.24	23.48	37-11	23.64	37.01	23.80
45	38.16	23.85	38.06	24.01	37.95	24.18	37.85	24.34
46	39-0I	24.38	38 90	24.55	38.80	24.72	-38.69	24.88
47	39.86	24.91	39-75	25.08	39.64	25.25	39-53	25.43
48	40.71	25.44 25.97	40.59	25.61 26.15	40.48	25.79	40.37 41.21	25.97 26.51
50	42.40	20 50	41.44	26.68	42.17	26.87	42 05	27.05
51	43.25	27.03	43.13	27.21	43.01	27.40	42.89	27.59
52	44.10	27 56	43.98	27.75	43.86	27.94	43-73	28.13
53	4495	28.09	44.82	28.28	44.70	28.48	44 58	28.67
54	45.79	28.62	45.67	28.82		29.01	45-4 2 46.26	29.21
95	46.64	29.15	46.52	29.35		29.55		29.75
57	47.49 48 34	29.08 30.21	47.36 48.21	29.88 30.42	47.23 48.07	30.09 30.63	47.10 47.94	30.29 30.84
58	49.19	30.74	, •	30.95	48.92		48.78	3138
59	\$0.03	31.27	49.90	31.48	49.76	31.70	49.62	31.92
60	50.88	31.80	-	32.02	50.60	31.24	50.46	32.46
1 2	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.	ist
Dist	0'		45	/	30/		15	
, —			. Km	DEGRE	100			

Ē	<u> </u>		15'		30'		451	
=	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.
61	51.73	32.33	51.59	32.55	51.45	32.78	51.30	33.00
62	53.43	'32.86 33.38	52.44 53.28	33.08 33.62	52.29 53.13	33.31	52.14	33.54
64	54.28	33.91	54-13	34.15	53.98	34-39	53.83	34 08 34.62
65	55.12	34-44	54-97	34.68	54.82	34.93	54-67	35.16
66	55-97	34.97	55.82	35.22	55.66	35.46	55.51.	35.70
67 68	56 82	35. 50 36.03	56.66 57-51	35.75 3 5 .29	\$6.51 \$7.35	36.00 36.54	56 35 57.19	36.25 36 79
69	58.52	36.56	58.36	36.82	58 19	37.07	\$8,03	37 33
70	59.36	37.09	59.20	37-35	59.04	37.61	59.87	34.87
71	60.31	37.62	60.05	37.89	19.88	38.15	\$9:71	38.44
72 73	61.06 61.91	38.15 38.68	60.89	38.42	60.72	38.69 39.17	60,55 61,40	3 8 .95 3 9 .49
74	62.76	39.21	62-58	39.49	62.41	39.76	62.24	40.03
75	63.60	39.74		40.02	63.25	40 30	63.08	49.57
76	6445	40.80	64.28 65:12	49.55	64.10	40.83	\$3.92	41.11
73	66.15	41.33	65.97	41.63	64.94 65.78	41.37	6 4.76	41.66
79	67.00	41.86	66.81	42.16	66.63	42.45	66-44	42.74
80	67.84	42.39	67.66	41.69	67:47	42.98	67.28	43.28
81 82	68.69 69 54	42.92	68.50	43.22	68.31	43.52 44.06	68,12	43.82
83	70.39	43.94		44.29	70.00	44.60	69.81	44.36 44.90
84	71.24	44.51	71.04		70.84	45.13	70.65	45.44
85		45.04		45.36		49.07		45.98
86 87		45.57	72 73 73.58	45.43	72.53	46.21 46.75	72.33	46.52 47.06
88		46.63	74-42	46.96	74.22	47.28		47 61
89		47.16	75,27	47.49		47.82	74.85	48.15
90	-	47.69	76.F2 76 96	48.03	75.91	48.36		48.69
91	_	48.22	77.81	r	76.75	140.09 149.43	76.53 77-38	49.23 49.77
93	78.87	49.28	78.65	49.63	78.44	49-97	78.22	50.31
94	79 72 80 56	49.81	179.50 80.34	50.69	79.28	50.51	79.06	50.85
95	81.41	50.24		5 8.23		51.04	79.90	51.39
97	\$2.26	50.87	_	51.76		52.12	80.74 81.58	51.93 52.47
98	83:11	51.93	82,88	52.29	82.65	52.66	82.42	53.02
99	83.96 84.80	52 46	\$3.73 \$4.57	5 2.83 5 3 .36	.	53.19	83.26	53.56.
101	85.65	53.52	\$5.42	53.90	-	53.73	84.19	54.10
102	\$6.50	54.05	86.26	54.43	86.03		85-79	54.18
103	\$7.35	54.58	87.51	54.96	86 87	55.34	86.63	54.72
104	\$8.20 \$9.04	55.88	87.96 88.80	56.03	87.74 88.56	55.88 56.42	87-47 88 31	50.26 50.80
106	19.89	50.17	84.65	56.56		50.95	89.15	57.34
107	90.74	50.70	90.49	57.10	90.24	57-49	89 99	57.88
108	91-59	57 23	91.34	57.63		5803	90.83	58.42
110	92.44 93.29	57 76	92.18	58.16	#1.93 92 77	58.57	91.67 92.51	54.97 54.51
8 2 3	94-13	54.82		59.23		59.64		60.05
112	94.98	59.35	94.72	59.76	94.46	60.18	94 20	60.59
314		59.88 60.41	95.57 96.41	60.30 60.83		60.71	95.04	61.13
335	97-53	60.94		61.37	96.99	61.79	95.88 96 72	61.67
116	98.37	61.47		61.90	97.83	62.33	97.56	62.75
117	99.22	64.00	98.95	63.43	98.68	6286	98:40	6329
118	100.1-	63.06	95.80 100.6	62.50	-	63.40	99.24	63.83
120	_	63.59	101.5	63.50 64.03	101.2	63.94 64.48	100.1	64.38 64.92
نيا	Dep.	Lat	Dep.	Lat	Dep.	Luc	Dep.	Lati
ig.	T	, —	45		30		15	
				DEGR	FES.			

	0/		15/		30′		45'	
Dist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep
	0.84	0.54	0.84	0.55	0.83	0.55	0.83	0.56
2	1.68	1.09	1.67	1.10	1.67	1.10	1.66	2.11
3	2.52	1.63	251	1.64	2.50	1.66	2.49	1.67
4	3-35	2.18	3.35	2.19	3-34	2 1 t 2.76	3.33° 4.16	2.22 2.78
5	4.19	2.72	4 18	2.74	4.17			3.33
6	5. 03 5. 8 7	3.27 3.81	5.02 5.85	3.29 3.84	5.84	3.3° 3.86	4.99 5.82	3.89
7 8	6.71	4.36	6.69	4-39	6.67	4.42	6.65	4-44
ġ	7-55	4.90	7.53	4.93	7.51	4.97	7.48	5.00
10	8.39	5.45_	8.36	5.48	8.34	5:52	8.31	5.56
11	9.23	5.99	9.20	6.03	9.17	6.67 6.62	9.15 9 49 8	6.67
12	10.00	6.54 7.88	10.04	6.58	10.84	7.18	1081	7.22
13	10.90	7.63	11.71	7.68	11.67	7.73	11/64	7.78
15	12.58	8.17	12.54	8.22	12.51	8.48	12.47	18.33
<u>r6</u>	13.42	8.71	13.38	8.77	13.34	8.83	43.30	8.89
17	14.26	9.26	14:22	9.32	14.18	9.38	14.14	9.44
18	15.10	9 80	15:05	9.87	15.01	9.93	14.97	10.00
19	15.93 16.77	10.35	15.89	10.42	15.84 16.68	10.49	16.63	_
20			-			11.59	17.46	11.67
21	17.61 18.45	11.44	47.56 48.40	11.51 12.06	17.51	12.14	18.29	12.22
23	19.29	12.53	19.23	12.61	19.88	12.69	19.42	1 2.78
24	20.13	13.07	20 07	13.16		13.25	19:96	13.33
25	20.97	13.62	20.91	13.78		13.80	20.79	13.89
26	31.81	14.16	21.74	14.36	21.68	1435	41.62 · :42.45	14.44
27	22.64	14.71	22.58 23.42	14.80	22.51 23.35	14.90	23:28	15.56
28 29	23.48 24.32	15.25	**************************************	15.90	24.18	1601	24.11	16.11
30	25.16	16 34	25.09	16.45	25.02	16.56	24:94	16.67
3 i	26.00	16.88	25.92	17.00	25.85	17.11	25.78	17 22
32	26.84	17.43	26:76	17 55	-26/68	17.66	26.61	17.78. 18.33
33	27.68	17.97	27.60 28.43	18.09 18.64	27.52 28.35	18.21 18.77	27.44 28:27	18.89
34	28.51 29.35	18.52 19.06	29.27	19.19	19.19	19.32	19110	19.44
35	30.19	19.61	30.14	19.74	10.02	19.87	29.53	20.00
· 36	31.03	20.15	30.94	20 29	30.85	20.42	30176	20.56
38	31.87	20.70	31.78	20 84	31.69	20.97	31.00	21.14
39	32.71	21.24	32.62	21.30	32:52	21.53	32 43	21.67 22.22
40	33.55	21.79	33.45	21.93	33 36	22.08	33.26	
41	34-39	22.33	34.29	22.48	34.49	22.63 23.18	34.09 34.92	22.78 23.33
42	35 -22 36-06	22 87 23.42	35.12	23.03 23.58	35.86	23.73	35.75	23.89
43	36.90	23.96	36.80	24.12	36.69	24.29	36.58	24.45
45	37.74	24 51	37.53	24.67	37-52	24.84	37:42	25.00
46	38.58	25.05	38.47	25.22	38.36	25.39	38.25	25.56
47	39.42	25.60	39-81	25.77	39419	26.37	39.08	26.51 26.67
48	40.26	26.14 26.69	40.14	26.32 26.87	40.86	26.49 27.04	40.74	27.22
1 49	41.09 4493	27.23	41.81	27.41	41.59	27.60	41.57	27.78
50	42.77	27.78	42.65	27.96	42.53	28.15	42.40	28.33
52	43.61	28.32	43.49	28.51	43.36	28.70	43.24	28.89
53	44-45	28.87	44.32	29.06	44.20	29.25	44.07	20 00
54	45.29		45.16 46.00	29.61 30.16	45. 5 3	29.80 30.36	44.90	30.00 30.56
55	46.13	29.96			-		-	31.11
56	46.97	30.50	46.83 47.67	30.70 31.25	46.70 47.53	30.91 31.4 6	46.56 47.39	31.67
57	47.80 .48.64	31.04 31.59	48.50	3480	48.37	32.01	48.29	32.22
59	49.48	32.13	49.34	32+35	49.20	32.56	49.06	34.7
60		32.68	50.18	3290	50.03	33.12		33-33
نید	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
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7	Lat-	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
61	51.16	33.22	51.01	33.45	50.87	33.67	50.72	33.89
62	52.00	33-77	51.85	33.99	51.70	34.22	51.55	34-45
63	52.84 53.67	34.31 · 34.86	52.69	34-54	152 53	34.77	52.38	15.00
65	54-51	35.40	53-52 54-36	35.64	53·37 54·20	35.32	53.21	35.56 36.11
66	55.35	35.95	55.19	36 19	55.04	36.43	54.88	36.67
67	56.19	36.49	56.03	36.74	55.87	36.98	55.7.1	37.22
68	57.03	37.04	56.87	37.28	56.70	37-53	56.54	37.78
69	57.87 58.71	37.58	57.70 58.5 4	37-83 38.38	57-5 4 58-3 7	38.08	57 37	38.33
70				-		38.64	58.20	38.89
71 72	59 55 60.38	38.67 39.24	59.38 6021	38.93 39.48	59.21 60.04	39.19 39.74	59.03 59-87	39·45 40.00
73	61.22	39.76	64.05	40.03	60.87	40-29	60.70	40.56
74	62.06	40.30	61.89	40.57 -	61.71	40.84	61.53	41.11
7.5	63.90	40,85	62.73	41 12	62.54	41 40	62 36	41.67
76	63.74	41-39	63.56	41.67	63.38	41.95	63-19	42.22
77	64.58	41.94 42.48	64.39 65.23	42.22 42.77	64 21	42.50	64.02 64.85	42.78 43.33
79	66.25	43.03	66.07	43.32	65.88	43.60	65.69	43.89
8o	67.09	43.57	66.90	43,86	66.71	44.16	66.52	44-45
18	67.93	44 12	67.74	44.41	67.54	44-71	67.35	45.00
82	68.77	44.66	68.58	44.96	68.38	45.26	68.18	45.56
83 84	89.61	45 21	69.41 70.25	45.51	69.21 70.05	45.84 46.36	69.01	46.11 46.67
85	70.45 71.29	45.75	71 08	46.60	70.88	46.91	69 84 70.67	47.22
86	72-13	46.84	71.92	47-15	71.71	47 47	71.51	47.78
87	72.96	47.38	72.76	47.70	72 55	48.02	72-34	48 33
88	73.80	47-93	73-59	48.25	73.38	48.57	73-17	48.89
89	74.64	48.47	74-43	48.80	74.22	49.12	74.00	49.45
90	75.48	49.02	75.27	49.35	75.05	49.67	74.83	50.00
91	76.33 77.16	49.56	76.94	49.89	75.88 76.72	50.23 50.78	75.66 76.50	50.56
93	78.00	50 65	77.77	50.99	77-55	51.33	77.33	51.67
94	78.84	\$1.20	78.61	91.54	78.39	51.88	78.16	52.22
95	79 67	51.74	79-45	52.09	79.22	52.43	78.99	52.78
96	80.51	52.29	80.28	52.64	80.05	52.99	79.82	53-33
97 98	81.35 84 19	52.83 53.37	81.12 81.96	\$3-1 8 \$3-73	80.89	53·54 54.09	80.65 81.48	53.89
99	83.03	53.92	82.79	54.28	82 55	54.64	82.32	54-45 55.00
100	83.87	54.46	83.63	94.83	83.39	55.19	83.15	55.56
101	84.7.1	55 01	84 46	55-38	84.22	55.75	83.98	56 11
102	85.54	55-55	85.30	55.93	85.06	56.30	84.81	56.67
103	86.38 87.22	56.10	86.14 86.97	56.47	85 89 86.72	46.85	85.64	57.22
104	88 v6	56.64 57.19 -	87.81	57- 02 57-57	87.56	57 40 57 95°	86.47 87.30	57.78 58 33
106	88.90	57.73	88.65	58.12	88.39	58.51	88.14	58.80
107	89.74	58.28	_ 1	58.67	89.23	59 06	88 97	59 45
108	90.58	58.82	90.32	59.23	90.06	59.61	89.80	60.00
109	91.42	59.37	91.16	59-76	90.89	60.16	90.63	60.66
110	92.35	59.91	91 99	60.31	91.73	60.71	91.46	61.11
111	93.09	60.45 61.00	93.83 93.66	60.86	93.40	61.26	92.29	61.67
113	94-77	61.54	94.50	61.96	94 23	62 37	93.96	62.78
114	95.61	62.09	95.34	62.51	95.06	62.92	94 79	63.34
115	96.45	62.63	.96.17	63.75	95.90	68.47	95.62	63.89
116	97.19	63.18	97.01	63.60	96.73	64.02	96.45	64.45
117	98.12	63 72 64.27	97.85 9 8.6 8 -	64.70	97.56 98.40	64.58 65.13	97.28 98.11	65.00
119	99.80	64.81	99.52	65.75	99.43	65.68	98.94	65 56
120	100.6	65.36	100.4	65 80	100.1	66.23	99.78	66.67
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	0.83	0.56	0.83	0.56	0.82	0.57	0.81	0.57
2	1.66	1.12	1.65	1.13	1.65	1.13	1.64	1.71
3	2.49 3.32	2.24	2.48 3.31	1 69 3.25	3.30	1.70 2.27	2.46 3.29	2.28
5	4.15	2.80	4.13	2.81	4.12	2 83	4.11	2.85
6	4.97	3.36	4.96	3.38	4-94	3-40	493	3.42
2	5.80	391	5.79	3-94	5.77	3 96	. 5.75	.3.99
8	6.63 7.46	4.47· 5.03	6.61 7.44	4.50 5.07	6.59 7.42	4-53 5 10	6.57 7-39	4.56 5.23
10	8.29	5.59	8.27	5.63	8.24	.5.66	8.22	5.70
11	9.12	6.15	9.09	6.19	9.07	6.23	9.04	6.27
12	9.95	671	992	6.75	9.89	6 80	9.86	6.84
13	10.78	7.27 7.83	1075	7 32 7.88	10.71	7.36 7.93	10.68	7-41 7-98
14	13 44	8.39	11.57	8.44	12 36	8.50	12.32	8.55
16	13.26	8.95	13.23	-9.20	13.19	9.06	13-15	9.12
17	14 09	9.51	14.05	9-57	14.01	9.63.	13.97	9.69
18	1491	10.07	14.88	10.13	14.83	10.20	14-79	10.36
19	15.75	10.62	15.71	10,69 11.26	+6 48	11.33	16.43	11.40
21	17 41	11.74	17.36	11.82	17.31	17.89	17.25	11.97
22	18.24	12 30	18 18	12.38	18.13	12.46	80.81	12.54
23	19.07	12.86	19.01	12.94	18.95	13.03	18.90	13 11
24	19.90	13.42	19.84	13.51	19.78 20 60	13.59 14.16	19.78 20.54	13.68 14.25
25	20.73	13.98	20.66	14.63	21 43	14.73	21,36	14.82
26 87	21 55	14 54	21.49	15.20	22.25	15.20	22 18	15.39
28	23.21	15.66	23.14	15 76	23.08	15.86	23.01	15.96
29	24.04	16.22	23.97	16.32	23 90	16.43	25.83	16 53 17.10
30	24.87	16 78	24.80	16.88	24-72	16.99	24.65	17.67
31	25.70	17.89	25.62 26.45	17.45	25.55 26.37	17.56 18.13	25 47 26.29	18.24
32	26.53 27.36	18.45	27.28	18 57	27.20	18.69	27.11	18.81
34	28.19	19.01	28.10	19.14	28.03	19.26	21.94	19.38
35	29.02	19.57	28 93	19 70	28.84	19.82	28.76	19.95
36	29.85	20.13	29.76	20.26 20.22	29.67 30 49	20.39 20.96	29.5 8 30.40	20.52
37	30.67 31.50	20.69	30.58 31.41	21 39	31.32	11.52	31.23	21.66
39	32.33	21.81	32.24	21.95	39.14	22.00	32.04	22.23
40	33.16	22.37	33.06	22.51	32.97	22.66	32.87	22.80
41	33 99	22.93	33.89	23.07	33-79	23.22 23.79	33.69	23.37 23. 94
42 43	34.82 35.65	23 49 24.05	34 72 35-54	23.64 24.20	34.61 35.44	24.36	34.51	24-5i
44	36.48	24.60	36.37	24.76	36.26	24.92	36.15	25.08
45	37.31	25.16	37.20	25.33	37 09	25.49	36.97	25.65
46	38.14	25 72	38 02	25.89	37.92	26.05	37.80	26.28 26.79
47	38.96	26.18 26.84	38.85 39.68	26.45	38.73 39.56	20.62	38.62 39.44	27.36
48 49	39.79 40. 62	27.40	40.50	27.58	40.38	27.75	40 16	27.93
50	41.45	27 96	41.33	28.14	41.81	28.32	41.08	28.50
51	42.28	28.52	42.16	28.70	42.03	28.89	41.90	29.07
52	43.11	29 D8	42 98	29.27	42.68	29-45 30-02	4273	29,64 30.81
53 54	43·94 44·77	29.64 30.20	.43.81 44.64	29.83 30 39	43.68	30.59	43-55 44- 3 7	30.78
55	45.60	30.76	45.46	30.95	45.33	31 15	45.19	34.35
56	46.43	31 31	46.29	31.52		31.72	46.01	31 92
57	47.26	31.87	47.12	32.08	46.98	32.29	46.83	32.49
58	48.68	32.43	47·94 48. 9 7	32.64. 38.21	47.40	32.85 33.41	47.66 48.48	33.06 33.63
59	48,91 49.74	32.99 33.55	49.60	33-77	49-45	33.98	49.30	34.80
1	Dep.	Lat.	Dep.	Lat	Dep.	Lat	Dep.	Lat
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Dist.	Lat	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
61	52.57	34-11	50.42	34-33	59.27	34-55	50.12	34-77
\$2	51.40	34.67	51.25	34.89	51.10	35.12	50.94	35.34 35.91
63	53.23	35.23	52.90	35.46 36.02	51.92 52.74	36.25	52.59	36.48
64	53.06	35.79 36.35	53-73	36.58	53-57	36.82	53.41	37.05
66	5472	36.91	54-55	37.15	54-39	37.38	54.23	37.62
67	55.55	37-47	55.38	37.71	55.24	37.95	55.05	38.19
7 .48	56.37	38.03	56.21	38.97	56.04 56.86	38.52	55.87 5 6.69	38.76 39-33
69	57.20 58.03	38.58	57.86	38.83 39.40	57-69	39.08 39.65	57.52	39.90
70	58.86	39-14	58.69	39.96	58.51	40.21	58.34	40.47
71 72	59.60	39.70 40. 36	59.51	40.52	59.34	40.78	59.16	41.04
73	60.52	40.83	60.34	41.08	60.16	41.35	59.98	41.61
74	61.35	41.38	61.17	43.65	60.99	41.91	60.80	42 18 42.75
75	62.18	41.94	61,99	42.31	62.63		62.45	43.32
76	63.01 63.84	42.50	62,82 63.65	42.77 43.34	. 63.46	43.05 43.61	63.27	43.89
77 78	64.66	43.66 43.63	64.47	43.90	64.28	44.18	64.09	44-46
79	65.47	44.18	65.30	44.46	65.11	44-75	64.91	45.03
80	66.32	44.74	66.13	45.02	65.93	45.31	65.73	45.60
81	67.15	45.39	66.95	45.59	66.75	45.88	66.55 67.37	46.17 46.74
82	67.98 68.81	45.85	67.78 68.61	46.35 46.71	68.40	46.45 47.01	68.20	47.31
84	69.64	46.97	69.43	47.28	69.23	47.58	69.02	47.88
85		47-53		47.84	70.05	48.14	69.84	48.45
86	71.30	48.09	71.09	48.40	70.87	48.71	70 0 6	49.02
87	72.13	48.65	71.91	48.96	71.70	49 28	71.48	49.59
88	72.96	49.21	72.74	4 9 .53 50.09	72.52	49.84 50.41	72.30	50.73
- 8 9	73.78 74-61	4 9 ·77 50.33	73.57 74-39	50.65	74-17	50.98	73-95	51.30
94	75-44	50.80	75.22	51.22	75.00	51.54	74.77	51.87
.93	76.27	51.45	76.05	51.78	75.82	58.81	75.59	57.44
98	77.30	52.00	76.87	52.34	76.64	52.68	76.41	53.01
94	77.93	52.50	77.70	52 90 53.47	77·47 78.29	53 24 53.8a	77.13 · 78.06	53 58
95	78.76	53.12	79.35	54-03	79-12	54-37	78 88	54.72
96	79.59 80.42	53.68 54-44	\$0.18	54.59	79.94	54-94	79.70	55.29
98	81.25	54.80	10.18	55.15	80.76	55.61	80.52	55 86
99	82.07	55.36	81.83	55.72 56.28	81.59	50.07	81.34 82.16	56.43
100	82.90	55.92	82.66	·	82.41	56.64	82.99	
101	83.73	56.48	83.49 84.31	56.84 57.41	83.24 84.06	57.31	83.81	57.57
103	84.56 85.39	57.04 57.60	.85.14	57.97	84.88	58.34	84.63	58.7 i
104	86.22	58.16	85.97	58.53	85.71	58.91	85.45	59.28
105	87.05	58.72	86.79	59.09	86.53	59.47	86.27	59.85
106	87.98	59-27	87.62	59 6 6 6 0. 22	87.36 88.18	60.64	87.09 87.92	60.42 60.99
107	88.71 89.54	59.83 60.39	88 45 89.17	60.78	10.28	61.17	88.74	61.56
109	90.37	60.95	90.10	61.35	89 83	61.74	89.56	62.13
110	91.19	61.51	90.92	61.91	90.65	62.30	90.38	62.70
111	92.02	62.07	91 75	62.47	91.48	62.87	91.25	63.27
212	92.85	62.63	92.68	63 03	92.30	61.00	92.85	63.8 4 64.41
213	93-68	63.19 63.7 5	93.40 94.23	63.60 64.16	93.13	64.00 64.57	93.67	64.98
1-15	94.51	64.31	95.06	64.72	94-77	65.14	94-49	65.55
116	96.17	64.87	95.88	65.20	95.60	65.70	95.31	66.12
117	97.00	65.43	96.71	65.85	96.42	66.27	96.13	66.69
118	97.83	65.98	97.54	66.41 66.97	97.25	66.84 67.49	96.95 97.78	67.26 67 83
119	.98.66 99.48	66.54	98.36 99.19	67.54	99.90	67.97	98.60	68.40
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55 DECREES.

25 20.48 14.34 20.42 14.43 20.35 14.52 20 29 14 61 26 21.30 14.91 21.23 15.01 21.17 15 10 21.10 15-19 27 22.12 15.49 22.05 15.58 21.98 15.68 21.91 15.77 28 22.94 16.06 22.87 16.16 22.80 16.26 22.72 16.36 29 23.76 16.63 23.68 16.74 23.61 16.84 23.54 16.94 30 24.57 17.21 24.50 17.31 24.42 17.42 24.35 17.53					DEGRE	EES.		9	
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Table Tabl	-	Lat	Dep.	Lat.	Dep.		Dep.	Lat.	_
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7		4.10	2.87	4.08	2.89				
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9 7.37 5.16 7.35 5.19 7.33 5.23 7.37 5.37 10 8.16 5.74 8.17 5.77 8.14 5.87 8.18 [A4] 11 9.02 0 31 8.03 6.35 8.96 6.39 9.77 6.97 9.74 7.24 1.2 9.83 6.85 9.80 6.93 9.77 6.97 9.74 7.24 1.4 11.47 8.03 11.33 808 11.40 8.13 11.35 12.29 8.60 12.25 8.66 12.21 8.71 22.17 2.16 10 13.11 9.18 13.07 9.33 13.03 9.75 13.88 9.81 13.84 9.87 12.29 9.93 12.13 13.03 9.75 13.88 9.81 13.84 9.87 12.30 9.75 13.88 9.81 13.84 9.87 12.30 9.93 12.60 12.21 10.70 12.50			E i	-				I ~	4 '1
11		7-37		7.35		7-33	5.23	7-3	5.26
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10			8.03		8 08	11.40	8.13		8.18
17		12.29						12 17	
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16.38 11.47 16.33 11.54 16.28 11.61 16.23 11.61 17.00 12.05 17.15 12 12 17.10 12.19 17.04 12.12 18.02 12.62 17.97 18.70 17.91 12.78 17.85 12.35 18.84 13.19 18.78 13.27 18.72 12.36 18.67 13.46 22.41 19.66 13.77 19.60 13.85 19.54 13.94 19.48 14.08 25 20.48 14.34 20.42 14.43 20.35 14.52 20.29 14.61 27 27 22.12 15.49 22.03 15.58 21.98 15.68 21.91 15.69 23.68 16.74 23.61 16.84 23.54 16.94 23.51 16.33 24.42 17.42 24.57 17.31 24.50 17.31 24.42 17.42 24.57 17.31 24.50 17.31 24.42 17.42 24.35 17.87 25.32 17.89 25.24 18.00 25.64 18.37 18.37 25.61 18.47 26.05 18.58 25.97 18.70 27.77 19.62 27.68 19.74 27.59 18.86 23.67 27.68 23.67 27.77 19.62 27.68 19.74 27.59 18.86 23.67 27.77 19.62 27.68 27.74 27.59 18.86 23.67 27.68 27.77 25.32 27.72 27.68 27.75 27.	9		-						E L 10
22	20	16.38	11.47		11.54	16.28	11.61	16.23	1 1.63
18 13 19 18 13 19 18 13 19 18 13 19 13 13 13 13 13 14 13 14 14			_		1	1		17.04	
19.66			1					17.85 18.6~	
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27		20.48	-	-	14.43		14.52		14 61
28		_			A -	<u>'</u>	1 -	i	15-19
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977 Egr # 1	73	59.80	42.87	59.61	42.13	59 43	42.39	\$9.24	42.65
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17 44 445	91	74-54	52 29	74-31	53.52	74.08	52.84	73 85	53 17
1\$.00 13 ³¹	92	75.36	52.77	75.13	53.10	74-90	53 42	74-66	53.75
(Rg\$ 150) 4.16 201)	93	76 18	53-34	75-95	53 67 54.25	7,5.71	54.01 54-59	75.48 76.29	5434 5492
9.16 18.11 9.76 31.83	94	77.82	53.92 54-49	77.58	54.83	77-14	55.17	77 10	55 50
791 Alex	96	78.64	55.06	78,40	55.44	78.16	55-75	77.91	56 09
- PE 39-E	97	79.46	15564	79 21	55.98	78.97	56 33	78 72	56.67
40 [325]	98	80.18	56.81	80.03	56.56	79-78	56.92	79 53 80 35	57.26
27 30 kin g 30 kin	99 100	81.40	5 4. 78	80-85 81.66	57.14 57.71	80.60 81 41	57-49 58 07	81.16	57.84 58 42
\$ JH#5	101	82,73	57-93	82 48	58.29	82.13	58.65	\$r.97	59.01
1312	103	83.55	58.50	83 30	58.87	83.04	39 23	81.78	59 59
1 3 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	103	84-37	59.08	84-11	\$9-45	83.85	59.81	83.59	81.00
13466	104	85.19 86.01	59.65	84-93 85.75	60.01	84.67 85.48	60.39 60.97	84 40 85.12	61.35
15 11 E	106	86.83	60.23	86.56	61,18	86 30	61,55	86 03	64.93
11-11 m	107	87 65	61.37	87 38	61.75	87.11	62 14	86 84	62 51
- 接接型 - ・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・	108	88.47	61.95	88. 20	52.33	87.92	61.72	87.65	●3. ro
8 ga 25	109	89.10	62.52	89.01	62.g1	88 74	63.30	88.46 89 27	64.08
2.7" (\$1.1	110	90.11	63.09	89.83	63.4.	89.55	63 88		64.27 64.8g
112	113	90.93	63.67 ·	90.65 97.46	64.64 64.64	90.37	65.04	\$0.08 90.90	45'44
to lies.	1.13	92.56	64.41	92.28	6 22	97.00	65.62	91.71	j ē f) 02
1 Par	1/4	93.38	65.39	93.10	65.79	9181	66.20	92 52	66.60
te	115	94.20	65.96	. 93.91	1 0, 37	93 62	66.78	93-33	67.19
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	116	95,02	66 53	94-73	66,95	94-44	67 36	94-14 94-95	67.77 68.36
927	117	96.66	67.11 67.68	95.55	68.10	95.25	67.94 58.52	95.77	68.94
10 mg	119	97-48	68. 26	97.18	68.63	96 88	69,10	96.58	69 53 70 11
4,	120	98.30	68 83	98,40	69.26	97.59	49 68	97-39	
2	*	Dep.	Tale	Dep	Lat.		Late		Lat
£ .		, 0	,	45		30	, ,	13	·
-	-			51	DECR	BES		-	*

-	0	. 0/		15	1	30)/	451	
ı	Dist.	Lat.	Dep	Lat.	Dep.	Lat	De .	Läl.	Dep
ŀ		0.86		0.85	0.52	0.85	0.52	0.85	0.53
ı	2	1.71	0.51	1.71	1.04	1.71	1.04	1.70	1.05
I	3	2.57	1.55	2.56	1.56	2-56	1.57	2-55	1.58
I	4	3-43	2.06	3.42	2.08	3 41	2.09	3.40	2.10 2.63
Ì.	5	4.29	2.58	4.27	2.59	4.26	;	4.25	
I	6	5.14	3.09	5.13 5.48	3.11 3.63	5.12 5.97	3.06	5.95	3.16 3.68
ı	7 8	6.00 6.%6	3.61 4.12	6.84	415	6.82	4.18	6.80	4.21
ı	9	7.71	4.64	7.69	4.67	7.67	4.70	7.65	4-74
ł	10	8.57	5.15	8 5 5	5.19	8.53	5.22	8.50	5 26
ľ	11	9.43	5.67	9-40	5.71	9 38	5.75	9-35	5.79
ł	12	10.29	6.18	10.36	6.23 6.74	10.23	6.27 6.79	10.20 11.0¢	6.84
ł	13	18.14	6.70 7 21	1.57	7.26	11.08	7.32	11.90	7.37
I	15	12.86	7.73	12.82	7.78	12 79	7-84	12.76	7.89
ł	16	13.71	8 24	13.68	8.30	13.64	8.36	13.61	8.42
I	17	14-57	8.76	14-53	8. 8 2 .	14.49	8.88	14.46	8.95
I	18	15.43	9.27	15.39	9.34	15.35.	9.40	15-31	9-47
ł	19	16.29	9.79	16.24	9. 86 10.38	16.20 17.05	9.93 10.45	16.16	10.00
Į.	20	17.14	10.30		10.89		10-97	17.86	11:05
ł	2 ! 22	18.00 18.86	10 82	17.95	11.41	17.91 18.76	11.50	18.71	11.58
I	23	19.75	11.85	19.66	11.93	1961	12.02	19.56	12.10
ţ	24	20 57	12 36	20.52	12.45	20.46	12.54	20.41	12 63
-	25	21,43	12 88	21 37	12.97	21:32	13.06	21.26	13.16
ł	26	22.29	13.39	32.23	13.49	23 17	13.59	22,11	13.68 14-21
ł	27 18	23.14	13.91	23.08	14.53	23.02	14.11	22.96	14-73
I	39	· 24.00 · 24.86	14.48	24.79	15.04 .		15.15	24.66	15.26
I	30	25.71	15.45	25.65	15.56	25.58	15.68	25.51	15.79
I	31	26 57	15.97	26 50	16.08	26.43	16 20	26.36	16.31
ł	32	27:43	16.48	27.36	16.60	27.18	16.72	27.21	16.84
1	33	28.29	17.00	28.21	17.12	28.14 28.99	17.24	28.06 28.91	17.37 17.89
1	34 35	29.14 30.00	18.03	29.07 29.92	18.16	29.84	18.29	29.76	18.42
ł	36	30.86	18.54	30.78	18 68	30,70	18.81	30.61	18.94
ł	3 7	31.72	19.06	31.63	19.19	31.55	19.33	31-46	19.47
ł	38	32.57	19.57	32-49	19.71	32 40	19.85	32.31	20.00
I	39	33-43	20.09	33-34	20.23	33-25	20.38 20.90	33.16 34.01	20.52 21.05
ŀ	40	34.29	20.60	34.20	20.75	34.11		34-86	21.37
ł	41	35.14 36.00	21.12 21.63	35-05 35-91	21.27	34.96 35.81	21.42 21.94	35.71	22.10
I	43	36.86	22.15	\$6.76	22 31	36.66	22.47	36.57	22.63
	41	37.72	22.66	37.62	22.83	37-52	22.99	-37 42	23.15
	45	38.57	23.18	38.47	23.34	38.37	23.51	38.27	23.68
.]	46	39-43	23.69	39-33	23.86	39,22	24.03	39.12	24.21
ł	47• 48	40.29	24.21	40.18	24 3 ⁸ 24 90	40.07	24.56 25.08	39.97 40.82	24.73 25.26
	49	41.14	24.72 25.24	41.89	25.42	41.78	25.60	41.67	25.78
	10	42.86	25.75	42.75	25.94	42.63	26.12	42.52	26.31
ľ	51	43.72	26.27	43.60	26.46	43.48	26.65	43-37	26.84
1	52	44-57	26.78	44.46	26.98	44-34	27.17	44.22	27.36
	53	45.43	27.30	45.31	27.50 28.01	45.19 46.04	27.69 28.21	45.07	27.89 28.42
ļ	54 55	45.29	27.81 28,33	47.02	28.53	46 90	28.74	46.77	28.94
ŀ	56	48.00	28.84	47.88	29.05	47.75	29.26	47.62	29.47
	57	: 48.86	29.36	48.73.	29.57	48.60	29.78	48.47	29.99
}	58	49.72	29.87	49.58	30.09	49.45	30.30	49.32	30.52
1	59	50.57	30.39	50.44	30.61	50.31	30 83	50.17	31.05
-	60	51.43	30.90	51:20	31.13	51.16 Don	31.35 Lah	51.02 Dep.	31.57 Lat.
I	Tist.	Dep.	Lat.	Dep.	Lat.	Dep.		15	
7	-	. ()/	45		30	, , , , , , , , , , , , , , , , , , , 	1.	
	•	58 DEGREES.							

1 5	0'		1.5	51	. S	0'	45!		1
Dist.	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	
61	52.29	31.42	52.15	31.65	52.01	31.87	51.87	32.10	
62	53.14	31.93	53.00	32 16	52.86	32.39	52.72	32.63	ĺ
63 64	54.00 54.86	32 45 32.96	53.86 54.71	3 2.68 3 3.20	53.72° 54.57	33.92 33.44	53·57 54·42	33. F5 33.68	1
65	55.72	33.48	\$5.57	33 72	55.42	33.96	55 27	34.20	Į.
66.	56.57	33.99	56.42	34.24	56.27	34.48	56.12	34.73	ŀ
67	57 43	34.51	57.28	34.76	57.13	35.01	56.98	3 4.25	ŀ
68	58.29	35.02	58.13	35.28	57.98	35 53	57.82	35.78	ľ.
69 70	59 14 60.00	3 5.54 36.05	58.99 59.84	35.80 36.31	58.83 59.68	36.05 36.57	58.67 59.52	36.3n 36 S#	İ
75	60.86	36 57	60.70	36.83	60 54	37.10	60 37	37.36	ŀ
72	61:72	37.08	61.55	37.35	61.39	37.62	61.23	37.89	ľ
73	62 57	37.60	62.41	37.87	62.24	38.14	62.08	38.41	ŀ
74	63.43	38.11	63.26	38.39	63.ro	38 66	63.78	38.94	ļ,
75	64.29	سبب سات	64.12	38.91	63.95	39.19		39.47	ŀ
76	66.00	39.14 39.66	64.97	39:43 39:95	64.80	39.71 40.23	64.63	39.99 40 52	ŀ
77 78	66.86	49.17	66.68	40.46	66'51'	40.75	66 33	41.04	I
. 79	67.72	40.69	67.54	42.98	67.36	41.28	67.28	41.57	Į.
85	68.574	41.10	68.39	41.50	68.21	41.80	68.03	41.10	I
81	69 43	41.72	69.25	42.02	69.06	41.32	6 8.88 6 9.73	42.62	
82	70.29	42.75	70.96	42 54 43.06	69.92 •70.77	43.37	70.58	43 15 43.68	ŀ.
84	72 00	43.26	71.81	43-58		43.89	71.43	44.20	Ì.
85	.72 86	43 78	72.67	44.10	72.47	44.4.1	72.28	44.73	
86	73.72	44.49		44.61		14.93		45.25	I
87	74.57	44.81	74 38	45.65	•••	45.46 45.48	73.98	45.78 46.38	Į,
88.	75.43 76.29	45.84	75.23 76.09	46.17	175.89.	_	75.68	46.83	ľ
. 90	77.25	46 35	76.94		76.74	47 02	76.53	47.36	I
91	78.00	44.87	77.80	47.25		47 55	77.38	47.89	ķ
92	78.86	47-38	78.65	47.73	, , ,	48.07 48.59	178,23	18.46	ľ
93	79.72 8 0.58	47.90 48.41	179.51 80.36	48.76	79.30	40.59	79 .08 79 :9 3	48.94 49.47	L
94 95	81.43	48.93	81.22	49.28		49.64		49.99	ľ
96	82.29	49 44	82:07	49 80	81.85	50.16	81.63	50.52	Ì
97.	83.15	49.96	82.93	50 32	82.71	53.68	82.48	51.04	ļ
98	84.00 84.86	50.47 50.49	83.78 84.64	50.84 51.36	*83 56. 84.41	51.20	83.33	5 1.57	I
100	85.72	51.50	85.49	51.88	85.26	52 25	85.04.	51.62	İ
101	86.57	52.02	86.35	52 40	86.12	52.77	.85.89	53.15	Į,
102	87.43	58.53	47.20	52.91	86.97	53.29	-86.74	53.67	ŀ
103	88.29	53.05	88.06	53.43	8782	53 82	87-59 88-44	54.10	į.
104	89:15	54.08	88.91 89.77	53.95 54.47	88167 89-53	54.34 54.86	89 29	54 73	ł
105	90.86	54-59	90.62	54 99	90.38	55.38	90.14	55.78	ſ
107	91.72	55.41	91.48	55,51	91.23	55.44	90.99	56.30	ŀ
128	92.57	55.62	92.33	56.03	92,09	50.43	91.84	56.83	į
109	93.43	56.14	93.19	56.55	92,94	59.95	92.64	57.34. 57.88	ļ.
110	94-29	50.05	94.04	57.06	93 79	57.47	93.54	58.41	ł.
111	95/15	57.17 57.68	94.90	58.10	95.50	58.52	94.39 95.24	58.94	ļ
113	96.86	58.20	96.61	,8.62	96 35	59.04	96.09	59.46	
114	97.72	58.71	97.46	59.14	97.20	59.56	-96.94	59.99	Ì.
115	98.57	59.23	98.31	59.66	98.05	60.09	97.79	60.51	ŀ
116	99·43 100.3	59.74 60.26	99217	60. r8 60.70	98.91 99!76	61.14	98.64	61.57	
117		60.77	100.0	61.12	103.6	61.65	10C.3	61 09	1
119	401.0	61.29	101.7	61.73	104.5	62.18	101.2	63.63	j
120	102.9	61.80	102.6	62.25	1023	62.70	102.0	63.15	1
Dist.	Dep.	hat	Dep.	Lat.	Dep.	Lat.	Dep	Lat.	
i ä	0	1	4		3()/	15	<i>:</i>	ļ
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E	0	'	15		30/		457	
Diat.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.85	0.53	0.85	0.53	0.84	0.54	0.84	0.54
2	1.70	1.06	1.69	1.07	1.69	1.07	1,68	1.08
3	2.54	1.59	2,54	1.60	2.53	1.61	2,52	1.62 2.16
5	3-39 4-24	2.12 2.65	3.38 4.23	2.13	3 37 4.22	2.69	3.36 4.21	2.70
6	5.09	3.18	5.07	3.20	5.06	3.22	5.05	3-25
	5 94	3.71	5.92	3.74	5-90	3.76	5.89	3-79
8	678	4-74	6.77	427	6.75	4.30	6.73	4-33
	7.63	477	7.61	4.80	7.59	4.84	7·57 8.41	4.87 5.48
10	8.48	5.30	8.46	5.34	8.43	5.37		
13	9-33 10. 18	5.83 6.36	9.30	5.87 6.40	9.28	5.91 6.45	9.25	5-95 6-49
13	11.02	6.89	10.99	6.94	10.96	6.98	10-93	7.03
. 14	11.87	7.42	11.84	7.47	11.81	7.52	11.77	7.57
15	12.72	7:95	12.69	8.00	12.65	8.06	12.62	8.18
16	13.57	8.48 9.02	13.53	9.07	13-49	8.60 9.13	13.46 14.30	8.66 9.20
17	14.42	9-54	14.38	9.64	14 34	9.67	15.14	9.74
19	16 DI	10.07	16,07	10.14	16.02	10.21	15.98	10 28
20	16.96	10 60	16.91	10.67	16.87	10 75	16.82	10.82
21	17.81	11.13	17.76	11.21	17 74	11.28	17.66	11.36
23	19.51	11.66	18 61	11.74	18.55 19.40	11.82	18.50	11.90
24	20.35	12.72	20.30	12.81.	20.34	12.90	20.18	12.98
25	21.30	13.25	21 14	13.34	21.08	13.43	21.03	13.52
26	21 05	13.78	21.99	13.87	21.93	13.97	21.87	14.07
27	22 90	14.35	22.83	14.48	12.77	14-51	22-71	14.61
28	23.75 24.59	14.84	23,68 24-53	14-94	23.61 24.46	15.04 15.38	23.55 14.39	15.55
30	35.44	15.90	25.37	16.01	25.30	16.12	25.23	16.23
31	16.29	16.43	26.22	16.54	26 15	16.66	26.07	16.77
. 32	27.14	16.96	27.06	17.05	26.99	17.19	26,91	17.31
33	27.99	17.49	27.91	17.62	27.83 28.68	17.73	27.75 28.60	18.39
34	28.83 29.68	18.02	28.75 29.60	18.14	29.52	18.81	29.44	18.93
36	30.53	19.08	30.45	19.21	30.36	19.34	30.28	19.48
37	31.38	19.61	31.29	19.74	31.21	19.88	31.12	20.02
38	32.23	20.14	32 14	20.28	32.05	20 42	31.96	20:56
397	33.07	20.67 21.20	32 98 33.83	20.81 21.34	32.89	20.95 21.49	32.80 33.64	21.10
		21.73		21.88	33.74	22.03	34 48	22.18
41	34-77 35 62	22.26	34.67	23.41	34.58 35.42	23 57		22.72
43	36.47	22.79	36.37	22.95	36.27	23.10	36.16	23.26
. 44	37.31	23 32	37.24	23.48	37-31	23.64		23.80
45	38.16	23.85	38.06	24.01	37.95	24.18	37.85	24.34
46	39.01 39.86	24.38 24.91	38 90	24.55	38.80 39.64	24.72	·38.69	24.88 25.43
1 48	40.71	25.44	40.59	25.61	40.48	25.79	40.37	25.97
49	41.55	25.97	41.44	26.15	41.33	26 33	41.21	26.51
50	42.40	20 50	42.29	26.68	42.17	26.87	42 05	27.05
51	43.25	27.03	43.13	27.21	43.01	27.40	42.89	27.59 28.13
53	44-10 44-95	27 56	43.98 44.84	27.75	43.86 44.70	27.94 24.48	43.73 44 58	28.67
¥ 54	45.79	28.62	45.67	28.82	45.54	24.01	45-42	29.21
95	46.64	29.15	46 52	29.35		29.55	46.26	29.75
36	47.49	29.68	47.36	29.88		30.09	47.10	30.29
57	48 34 49.19	30.21 30.74	48.21	30.42	48.07 48.93.	30.63	47-94 48.78	30.84 33.38
_	50.03	31.27	49.90	31.48		31.70	49.61	31.92
. 60	50.8	31.80		32.02		32.24	50.46	31.46
12	Dep.	Lat	Dep	Lat.	Dep.	Let	Dep.	Lat
Dist	04		45	7	30/		15	
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Dist	. 0	4	1.) *	3	0'	45	7
1 4	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.
61	51.73	32.33	51.59	32-55	51.45	32.78	51.30	33.00
62 63	52.58 53.43	32.86 33.38	52.44 53.28	33.08 33.62	52.29	33.31	52.14	33-54
64	54.28	33.91	54-13	34.15	53.98	34-39	52.99 53.83	34.62
65.	55.12	34-44	54-97	34.68	44.82	34.93	54-67	35.16
66	55-97	34.97	55.82	35.22	55.66	35.46	55.51.	35.70
67	56 82 57. 6 7	35. 50 36.03	56-66 57-51	35.75 3 5 .29	\$6.51 \$7.35	36.00 36.54	56 35 57-19	36.25 36 79
69	58.52	36.56	58.36	36.82	58 19	37.07	\$8.03	37 33
70	59.36	37.09	59.20	37.35	59.04	37.61	59.87.	34.87
71	61.06	37. 62 38.15	60.84	37.89	19.88	38.15	\$9.71	38.44
72 73	61.91	38.68	61.74	38.95	61.57	38.69 3 9.1 2	60,55 61-40	3 8 .95 3 9 .49
74	62.76	39.21	62.58	39-49	62.41	39.76	\$2.24	40.03
75	63.60	39.74	63.43	40.02	63.25	40 30	\$3,Q8	40.57
76 77	65.30	40.80	64.28 65:12	49.55	64.1Q 64.94	40.83	\$3.92 \$4.76	41.11
78	66.15	41.33	65.97	41.62	65.78	41.91	65.60.	42.20
79	67.00	41.86		42-16	66.63	41.45	66.44	42.74
80	67.84	42.38	67.66	41.69	67.47	42.98	67.28	43.28
81	68.69 69 54	43.45	68.50 69'35	43.22 43.76	68.31	43.52	6 8.12 6 9.97	43.82 44.36
93	70.39	43.98	70.20	44.29	70.00	44.60	69.81	44.90
84		44.51	71.04		70.84	45.13		45.44
85		45.04	72.73	41.36	71.69	45.67		45.98
27		45.57	73.58	40.42	73.38	46.75		47.06
88	74-63	46.63	74.42	,44.96	74.33	47.28	74-01	47 61
89 90		47.16	75,27 76, F2	147-49 148-03	75.06 75.91	47.82 48.36	74.85	48.15 48.69
98	77-17	48.22	76 96		76.75	48.89	76.53	49.23
92	78.02	48.75	77.81	49.09	77.59	49.43	'. " =	49.77
93	78.87	49.28		49.63 50.16		49-97		50.31
94 95	79 72 80 56	49.83 50.24	<u> </u>	50.69	79.28	50.51 51.04	79.06 79.90	50.85 51.39
96	81.41	50.87		5 8. 23	80 97	51.58	80.74	51.93
97	82.26	51.40		51.76	81.81	52.12	81.58	52.47
98	83.11 83.96	51.93 52 46		52.29 52.83	82.65 83.50	5 2.66 53.19		53.02 53.56
100	84.80	52.99	84.57	53.36	84 34	53.73	84.10	54.10
201	85.65	53.52	85.42	53 90	85.18	54.27	84.94	54.64
103	\$6.50	54.05	_	54.43	86.03 86 87	54 80 5 5 34	85-79 86-63	54.18
104	\$8.20	54.58		54.96 54.50	87.74	55.88		54.72 50.26
105	89.04	55.64	88.80	56.03.	88.56	56.42	88 31	50 80
106	19.89	56.17		56.56	89.40	56.95	89.15	57.34
108	90.74	57.70	90.49	57.10 57.63	90.24 g1.09	57 .49 58.03		57.88 5 8.42
109	92.44	57 76	92,18	58.16	#1.93	58.57		58.97
1 10	93.29	58.29		58.70	92 77	59.10	92.51	59-51
111	94.13 94.98	58.82	93.88	59.23	93.62	59.64	93.36	60.05
113		59.35 59.88	94.72 95.57	59.76 60. 30	• • •	60.71	94 20 95.04	60.5g 61.13
314	96.68	60.41	96.41	60.83	96.15	61.25	95.88	61.67
315		60.94	97.26	61.37	96.99	61.79	96 72	62.31
116	98.37	61.47	98.10	61.90 62.43		6233 6286	97.56 98.40	62.75
318	100.1-	61.53	99.80	62.97	99-52			63.2g
119	100.9	63.06	100.6	6350	100-4	63.94	100.1	64.38
120		497 7. (6)	101.5	64.03	101.2	64.48	100.9	64.93
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Dist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep
	0.84	0.54	0.84	0.55	0.83	0.55	0.83	0.56
2	1.68	1.09	1.67	1.10	F:67	1.10	1.66	1.11
3	3.52	1.63	251	1.64	2.50	1.66	2.49	2.67
4	3.35	2.18	3.35	2.19	3.34	2 11 2.76	3.33° 4.16	2.78
5	4.19	2.72	4 18	2.74	417	3.34	4.99	3.33
	5. 03 5. 8 7	3.27 3.81	5.02 5.85	3.29 3.84	5.80 5.84	3.86	5.82	3.89
7 8	6.71	4.36	6.69	4.39	6.67	4.42	6.65	4-44
9	7-55	4.90	7-53	4-93	7.51	4.97	7.48	5.00
10	8.39	5-45_	8.36	5.48	8.34	5.52	8.31	5.56
11	9.23	5.99	9.20	6.03	9.17	6.67 6.62	9.15	6.67
12	10.06	6.54	10.04	7.13	10.01	7.18	9698	7.22
13	10-90 11i74	7.58 7.63	11.71	2.68	1 ry67	7.73	11/64	7.78
[4 [5	12.58	8.17	12.54	8.22	12.51	8.28	12.47	18.33
<u>r6</u>	13.42	8.71	13.38	8.77	13.34	8.83	43.30	8.89
17	14.26	9.26	14:22	9.32	14.18	9.38	14.14	9.44
18	15.10	9 80	15.05	9.87	15.01	9.93	14.97	10.00
19	15.93 16.77	10.35 10.8g	15.89 16.73	10.42 10.97	15.84 16.68	10.49	16.63	11.11
20			17.56		17.51	11.59	17.46	11.67
21	17.61	11.44	18.40	11.51 12.06	18.35	12.14	18.29	12.22
23	19.29	12.53	19.13	12.61	19.18	12.69	19.12	12.78
24	20.13	13.07	20 07	13.16	20:01	13.25	19:96	13.33
25	20.97	13.62	20.91	13.71	20.85	13.80	20.79	13.89
26	2181	14.16	31.74	14.26	21.68	1+35	21.62	14.44
27	22.64	14.71	22.58	14.80	22:51	14.90	:42.45 23.28	15.00
28	23.48 24.32	15.25	23.42 24 25	15.35	24.18	1001	24.11	16.11
2 9	25.16	16 34	25.09	16.45	25.02	16.56	24:94	16.67
31	26.00	16.88	-25.92	17.00	25-85	17-15	25.78	17 22
32	26.84	17.43	26.76	17 55	26/08	17.66	26.61	17.78
33	27.68	17-97	27.60	18.09	27.52	18.21	27.44	18.33 18.89
34	28.5t	18.52	28.43	18.64	28.35	18.77	18.27. 19110	19.44
35	29.35	19.06	29.27	19.19	19.19	19.87		20.00
36	30.19	19.61	30.14 30.94	19.74	30.85	20.43	39,93	20.56
37	31.03	20.15 20.70	31.78	20 84	31.69	20.97	31,60	21.11
39	32.71	21.24	32:62	21.38	32152	21.53	32 43	21.67
40	33.55	21.79	33.45	21.93	33 36	22.08	33.26	22.22
41	34-39	22.33	34.29	22.48	34.49	22.63	34.09	22.78
42	35.22	22 87	35.12	23.03	35.02	23.18	34.92	23.33 23.89
43	36.06	23.42	35.96 36.80	23.58	35.86 36.69	23.73 24.29	35.75 36:58	24.45
44 45	36.90 37.74	23.96 24 51	37.53	24.67	37.52	24.84	37:42	25.00
-	38.58	25.05	38.47	25.32	38.36*	25.39	38.25	25.56
46	39.42	25.60	39.81	25.77	39419	25.94	39.08	26.11
43	40.26	26.14	40.14	26.32	40 03	26.4g	39491	26.67
. 49	41.09	26 .69	40.98	6.87	40.86	27.04	40:74	27.28 27.78
50	4493	27.23	41.81	27.4T	41.69	27.60	41.57	28.33
. 51	42.77	27.78	42.65	27.96 28.51	42.53	28.15 28.70	42.40 43.24	29.33 28.89
52	43.61	28.32 28.87	43.4 9 44.32	29.06	43.36 44.20	29.25	44.07	29 45
53 54		29 41	45.16	29.61	45.03	29.80	44.90	30.00
55		29.96	46.00	30.16	45.86	30.36	45.73	30.56
56	46.97	30.50	46.83	30.70	46.70	30.91	46.56	34.11
57		31.04	47.67	31.25	47.53	31.46	47-39	31.67
' 58	.48.64	31.59	48.50	3480		32.01		32.22
59	49.48	32.13	49.34 50.18	32.35 32.90	49.20 50.03	32.5 6 33.12	49.86	32.78° 33.33
60		32.68				Lat		Lat.
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1	7	Lat-	Dep.	Lat.	Dep.	Lat.	Dep	Lat.	Dep.
,	61	51-16	33.22	51.01	33.45	50.87	33.67	50.72	33.89
4	62	52.00	33-77	51.85	33.99	51.70	34.22	51.55	34-45
36.	63 64	52.84 53.67	34.31. 34.85	52.69	34-54 35.09	52 53 53.37	34.77 35.32	52.38	35.56
	65	54.51	35.40	-54.36	35.64	54.20	35.88	53.21	36.11
1	66	55-35	35.95	55.19	36,19	55.04	36.43	54.88	36.67
-	67 68	56.19	36.49	56.03	36.74	55.87	36.98	55.7.1	37.22
4	69	57.0 3 57.87	37.58 37.58	56.87	37.28 37.83	56.7Q 57-54	37-53 38.08	56.54 57.37	37.78 38.33
	70	58.71	38.12	58.54	38.38	58-37	38.64	58.20	38.89
1	71	59 55	38.67	59.38	38.93	59.21	39.19	59 03	39.45
İ	72 73	60.38 61.23	39.24 39.76	61.05	39.48 ₃	60.04 60.87	39.74	59.87	40.00
1	74	62.06	40.30	61.89	40.57	61.71	40.84	60.70 61.53	40.56
1_	75	62.90	40,85	62.73.	41 12	62.54	41 40	62 36	41.67
1	76	63.74	41-39	63.56.	41.67	63.38	41.95	63-19	42.22
1	77 78	64.58	41, 94 42.48	64.39 , 65.23	42.22	64 21	42.50 43 05	64.02 64.85	42.78
	79	66.25	43.03	66.07	43-32	65.88	43.60	65.69	43.89
4 ~	<u>80</u>	67.09	43.57	66.90	43,86	66.71	44.16	66.52	44.45
•	18	67.93	44 12	67.74	44.41	67.54	44.71	67.35	45.00
•	82 83	68.77	44.66 45 21	68.58 69.41	44.96	68.38 69,21	45.26 45.81	69.01	45.56
}	84	70.45	45-75	70.25	46 06	70.05	46.36	69.84	46.67
	85	71.29	46.29	71 08	46.60	70 88	46.91	70.67	47.22
•	86 8 ₇	72.13	46.84	71.92	47-15	71.71	47 47	71.51	47.78
	\$ 8	73.80	47.38	72.76	47.70	73.38 73.38	48.02 48.57	72-34	48 33 48.89
	89	74.64	48.47	74-43	48.80 .	74.22	49.12	74.00	49.45
-	90	75.48	49.02	75.27	49.35	75.05	49.67	7483	50.00
-	91 92	76.33	49.56	76.94	49.89	75.88 76.72	50.23 50.78	75.66.	50.56
	93	78.00	50 65	77.77	50.99	77-55	51.33	76.50 77.33.	51.11
1	94	78.84	\$1.20	78.61	\$1.54	78.39	51.88	78.16	52.22
-	95	79 67	51.74	79.45	52.09	79-22	52.43	78.99	52.78
	96 97	84.35 80.51	52.29 52.83	80.28	52.64 53.18	80.05 80.89	52.99 53.54	79.82 80.65	53·33 53·89
	98	84 19	53.37	81.96	53.73	81.72	54.09	81.48	54.45
	99 00	83.03	53.92	82.79	54.28	82 55	54.64	82.32	55.00
1-	01	83-87	55 01	83.63	55-38	83.39	55.19	83.15	55.56
•	02	85.54	55.55	85.30	55.93	85.06	55.75 56.30	84.81	56.67
	03	86.38	56.10	86.14	56.47	85 89	46.85	85.64	57.22
3	04	87.22 88.06	56.64 57.19.7	86.97 87.81	57-02 57-57	86.72 87.56	57 40 57 9 5•	86.47 87.30	57.78 58 33
_	06	88.90	57.73	88.65	58.12	88.39	58.51	88.14	58.80
110	07	89.74	58.28	_ =	58.67	89.23	59 06	88 97	59 45
	08	90.58	58.82	90.32	59.22	90.06	59.61	89.80	60.00
•	10	91.42	59·37 59·91	91.16	59.76 60.31	90.89	60.16 60.71	90.63	60.56 61.11
ī	11	93.09	60.45	92.83	60.86	92.56	61.26	92.29	61.67
•	12	93.93	61.00	93.66	61.41	93.40	61.82	93-12	62.22
•	13	94-77	61.54 62.09	94.50 95.34	61.96 62.51	94 23 95.06	62 37 82.92	93.96	62.78
	15	96.45	62.63	.96.17	63.05	95.90	68.47	94 79 95.62	63. 34 63. 89
- 1	16	97.29	63.18.	97.01	63.60	96.73	64.02	96.45	64.45
	17	98.13	63.72	97.85	64.35	97.56	64.58	97.28	65.00
	18	98:96 9 9:8 0	64.27 64.81	98,68 : 99.52	64.70 65. 35	98.40 99-43	65.13 65.68	98.11 98.94	65 56
•	20	100.6	65.36	100.4	65 80	100.1	66.23	99.78	65.67
	*	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat
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1	J .	0/	•	15	7	30) /	45	
1 3		Let.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
}-		0.83	0.56	0.83	0.56	0.81	0.57	0.81	0.57
	2	1.66	1.13	1.65	1.13	1.65	1.13	1.64	1.14
	3	2.49	1.68	2.48	1 69	2.47 3.30	1.70 2.27	2.46 3.29	1.71 2.38
	4	3.32	2.24	3.31 4.13	2.25 2.81	4.12	283	4.11	2.85
	6	4.97	3.36	4.96	3.38	4.94	3-40	493	3.42
1	7	5.80	391	5.79	3 -9 4	5.77	3 96	. 5.75	3.99
J	8	6.63	4-47	6.61	4.50	6.59	4-53 5 10	6.57 7.39	4.56 5.13
	9	7.46 8.29	5 03 5-59	7.44 8.27	5.63	7.42 8.24	.5.66	8.22	5.70
[-	9.12	6.15	9.09	6.19	9.07	6.23	9.04	6.27
•	2	9.95	671	992	6.75	9.89	6 80	9.86	6.84
	3	10.78	7.27 7.83	10.75	7.32	10.71	7.36	10.68	7-41
	4 5	11.61	8.39	11.57	8.44	12 36	8.50	12.32	8.55
-	6	13.26	8.95	13.23	-9.20	13-19	9.06	13.15	9.12
1 :	7	14 09	9.51	14.05	9-57	14-01	9.63.	13-97	9.69
3	8	14.92	10.07	14.88	10.13	.14.83 15.66	10.20	14-79	10.26 20.83
	9	15.75	10.62	15.71	10,69 11.26	16 48	11.33	16-43	11.40
{	-	17.41	11.74	17.36	11.82	17.31	11.89	17.25	11.97
	2	18.24	12 30	18 18	12.38	18.13	12.46	18,08	12.54
	3	19.07	12.86	19.01	12.94	18.95	13.03	18.90	13.68
_	4	19.90 20.73	13.42 13.98	19.84 20.66	13.51	19.78 20.60	13.59 14.16	19.72 20.54	14.25
I	6	21 55	14 54	21.49	14.63	21 43	14-73	21.36	14.82
	7	23 38	15.10	22.32	15.20	22.25	15.29	22 18	15.39
	8	23.21	15.66	23.14	15 76	23.08	15.86	23.01	15.96
•	9	24.04 24.87	16.12 16.78	e 3.97 24.80	16.32 16.88	23 90 24.72	16.43	23.83 24.65	16 53 17.10
-	0	25.70	17.33	25.62	17.45	25.55	17.56	25 47	17.67
	2	26.53	17.89	26.45	18.01	26.37	18.13	26.29	18.24
	3	27.36	18.45	27.28	18 57	27.20	18.69	27.11	18.81
_	4	28.19	19.01	28.10 28 93	19.14	28.02 28.84	19.26 19.22	23.94 28.76	19.38 19.95
_	6	29.85	19.57	29.76	20.26	29.67	20.39	29.58	20.52
•	7	30.67	20.69	30.58	20.32	30 49	20.96	30.40	21.09
3	8	31.50	21.25	31 41	21 39	31:32	31 52	31.33	31.66 32.33
	9	32.33	21.81 22.37	32.24 33.06	21.95	32.44	22.00 22.66	32.04 32.87	22.80
	0 -	33.16	22.93	33.89	23.07	33-79	23.22	33.69	23.37
_	2	33 99 34 82	23 49	34.72	23.64	34.61	23.79	34.51	23.94
	3	35.65	24.05	35.54	24.20	35.44	24.36	35.33	24.51
	4	36.48	24.60	36-37	34.76	36. 26 37 09	24.92 25.49	3 6.1 5	25.65 25.65
1	5	37.31	25.16	37.20	25.89	37.91	26.05	37.80	20.22
-	7	38.96	26.28	38.85	26.45	38.73	26.62	38.62	26.79
4	.8	39.79	26.84	39.68	27.01	39.56	27.19	39.44	27.36
	9	40.62	37.40 27.06	40.50	27.58	40.38	27.75 28.32	45 26	27.93 28.50
	0	41.45	27 96 28.52	42.16	28.70	42.03	28.89	41.90	20.07
5	2	43.11	29 08	42 98	29.27	42.85	29.45	4273	29,64
5	3	43.94	29.64	.43.81	29.83	43.68	30.02	43.55	30.91
S		4+77 45.60	30.20 30.76	44.64 45.46	30.95		30.59	44-37	30.78
5		46.43	38 3T	46.29	31.53		31.72	46.01	31 92
5		47.26	31.87	47.12	32.08	46.98	32.89	46.83	32.49
5	8	48.08	32.43	47-94	32.64	47.40			33.06
5		48.91	32.55	48.77 49.60	3 3.21 3 3.77	48.62 49-45	3 3.41 3 3.98	48.48 49.30	33.63 34.80
1		49.74	33.55 Lat.	Dep.	Lat.	Dep.	Let	Dep.	LaL
		Dep.	<u></u>	45	<u>'</u> 1	30		15	i
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7.7	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
61	52.57	34-11	50.42	34-33	59.27	34-55	50.12	34-77
62	51.40.	34.67	51.25	34.89	51.10	35.12	50-94	35.34
63	52.23	35.23	52.90	35.46 36.02	56.92	35.68 36.25	51.76	35.91 36.48
64	53.06	35.79 36.35	53-73	36.58	53-57	36.82	53.41	37.05
66	5472	36.91	54-55	37.15	54-39	37.38	54.23	37.62
67	55.55	37-47	55.38	37.71	55.22	37-95	55.05	38.19
7 .68	56.37	38.03	56.21	38.27	56.04	38.52	55.87	38.76
69 .	57.80	38.58	\$7. 9 3 57. 8 6	38.83	56.86	39.08 39.65	56.69 5 7 -5 2	39-33 39.90
70	58.03	39-14		39.40	58.51	40.21	58.34	40.47
71	58.86 59. 60	39.70 40.86	58.69 59.51	39.96 40.52	59.34	40.78	59.16	41.0,1
72 73	60,52	40.82	60.34	41.08	60.16	41.35	59.98	41.61
74	61.35	41.38	61.17	41.65	60.99	41.91	60.80	42 18
75	62.18	41.94	61.99	42.31	61.81	42.48	61.62	42.75
7,6	63.01	42.50	62,82	42.77	62.63 • 63.46	43.61	62.45 63.27	43.32 43.89
77 78	6 3.84 6 4.66	43.66 43.62	63.65 64.47	43.34 43. 9 0	64.28	44.18	64.09	44.46
79	65-49	44.18	65.30	44.46	65.11	44-75	64.91	45.03
80	66.32	44.74	66.13	45.02	65.93	45.31	65.73	45.60
81	67.15	45.39	66.95	45.59	66.75	45.88	66.55	46.17
82	67.98	45.85	67.78	46.15	67.58	46.45	67.37 68.20	46.74
83	68.81	46.41	68.61	46.71	68.40 69.23	47.01 47.58	69.02	47.31 47.88
84	69.64 70.47	46.97 47-53	69.43 70,26	47.84	70.05	48.14	69.84	48.45
86	71.30	48.00	71.09	48.40	70.87	48.71	70 ö 6	49.02
87	72.13	48.65	71.91	48.96	71.70	49 28	71.48	49.59
88	72.96	49.21	72.74	49.53	72.52	49.84	72.30	50.16
-89	73.78	49.77	73.57	50.65	73-35 74-17	50.98	73.13 73.95	50.73
90	74-61	50.33	74-39	51.22	75.00	51.54	74.77	51.87
94	75.44 76.27	50.89	75.22	51.78	75-82	52-11	75.59	57.44
93	77.30	51.45	76.87	52.34	76.64	52.68	76.41	53.01
94	77.93	52.56	77.70	52 90	77-47	53 24	77.23	53 58
95	78.76	53.12	78.53	53-47	78.29	53.Ba	78.06	54.15
96	79.59	53.68	79-35	54.03	79-12	54.37	78 88	54.72
97	80.42 81.25	54- 34 54-80	81.01	54. 59 55.15	79.94 80.76	56-94	79.70 80.52	55.29 55 86
98	82.07	55.36	81.83	55.72	81.59	56.07	81.34	56.43
100	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00
101	83.73	56.48	83.49	56.84	83.24	57.31	82.99	57-57
102	84.56	57.04	84.31	57.41	84.06	57.77.	18,58	58.14
103	85.39	57.60	85.14 85.97	57.97 58.53	84.88 85.71	58.34	84.63 85.45	58.71 59. 2 8
104	86.22 87.05	58.16 58.72	86.79	59.09	86.53	59.47	86.27	59.85
106	87.98	59.27	87.62	59 66	87.36	60.04	87.09	60.42
107	88.71	59.83	83 45	60.22	88.18	60.61	87.92	60.99
108	89.54	60.39	89.27	60.78	80.81	61.17	88.74	61.56
.109	90.37	60.95	90.10	61.35	89 83 90.65	61.74	89.56 90.38	62.13 62.70
110	91.19	62.51		62.47	91.48	62.87	91.20	63.27
116	92.02	62.63	9175	63 03	92.30	63.44	92.02	63.84
E13	93.68	63.19	93.40	63.60	93.13	64.00	92.85	64.41
114	94-51	63.75	94.23	64.16	93.95	64-57	93.67	64.98
115	95.34	64.31	95.06	64.72	94-77	65.14	94-49	65.55
116	96.17 -	64.87	95.88	65.20	95.60 96.42	65.70	95.31	66.12 66.69
117	97.00	65.43	96.71 97·54	65.85 66.41	97.25	66.84	96.95	67.2 6
119	98.66	66.54	98.36	66.97	98.97	67.49	97.78	67 83
120	99.48	67.10	99.19	67.54	99.90	67.97	98.60	68.40
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-	61	49-97	34.99	49.81	35 BL	49.66	35.44	49-51	35.64
ì	61	50.79 51.61	35 56	50.63 \$1.45	36.74 36.36	50.48 £1.39	36.00 36.58	\$0.32 \$1-13]6.12]6.81
1	64	32.43	36 71	\$2.87	36.94	\$3.10	37.16	\$1.94	37.39
4	65	53-44	37 28	53 0\$	37-51	53.92	37-75	52.75	37-98
1	65	54.06	37,36	53.97	38.09	\$1.71	38.33	53-56	38.56
1	68	54.88	39.00	54.71 55-53	38.67 39.25	\$4-\$5	38.91 39.49	\$4.38 \$5.19	39-14 39-73
	69	56.52	39.58	\$6.35	19.82	\$9 47	40.07	\$6.00	40.31
1	70	• 57-34	42.15	57.16	40-40	56.99	40 65	56.81	40 90
1	71	\$8.16 \$8.98	49.78	57.98 58.80	40.9% 41.55	57.80 58.62	41.33 41.81	57 62 58.43	41.45
1	11	59.80	41.87	59-61	42-13	59 43	42.39	\$9.24	42 65
Ц	74	60.69	42-44	60 43 6L35	41.71 43.29	61.06	42.97	60.061	43 23 43 83
Н	75	62.26	43.02	62.06	43.86	61 \$7	73·33 44·13	61 68	44-49
Н	79	63.07	44-17		44-44	61.69	44 71	62.49	44 99
H	78	63.89	44-74	63.70	45.02	65 50	45.29	63 30	45 57
Н	87	64.71 65.53	45.31 45.89	64-51 75-33	45.59	64-31	45.85 46.46	64.11 64.93	46.16 46.74
I	81	66.35	46.46	66.15	+6 75	65 94	47-04	65.74	47 33
	22	67.17	47.03	66.96	47 33	66.75	47 62	66.55	47 91
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1	£7	71.27	49-90	71.05	50.21	70.B3	50.58	70.61	50.831
	23	72.09	50.47	71.86 71.68	50.79 54.37	71.64	51.68	71.41	51 41 53 00
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ŀ	91	74-54	53 2Q	7431	52.52	74.08	52.34	73 85	55-176
1	93	75.30	51.77 53-34	75-13	53.10 53.67	74-99	53:43 54:01	74.00	53-751 5434.
4	94	77.00	53.92	76.76	54.35	76.53	54-59	76 29	\$4 91.
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ı	96	78.64 79.46	55.06 55.64	78.40 79 21	55.41	7¥ 16 78.97	55:75 56 33	77 91 78,72	36 09 56.67 m
1	97	\$0.18	56.24	80.03	56.56	79.78	56.92	79 53	\$7.26
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·	103	84-37	59.08	84.11	59-45	83.85	59.81	\$3.59	\$0.18 \$0.76
J	104	\$6.19	59.65 60.33	\$4.93 \$5.75	60.01 60.60	84.67	60.39 60.97	84 40 85.22	61.35
1	106	\$6.83	60.10	86.50	61.18	86 30	61.55	\$6.03	61.93
1	107	\$7.65	61.37	87 38	61.75	\$7.11	61 14	86 8a	[62. Ş1. ¹]
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	125	94-20	65.96	91-91	16.37	93 62	66.78	93.33	67 79
1	116	95.01	66.53	94-73	66.95	94-44	67 36	94-14	67.77 48.36
	117 118	95.84 96.66	67.68 67.68	95.55 96.36	67.53 68.10	95.07	67.94 68.52	94-95 95-77	68.94
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1 3	2.43	1.76	240	1.77	9-4E -	1.70	240	1.79
1 1	3.34	2-35	3-53	2.37 2.96	3.11 4.01	9-38 1-97	3.90 4.01	39 3.99
1	405	2.94	4-05		414	3-57	4.81	3-59
	4-15 5.66	3:53	4.84	3-55 4-14	5.63	416	5.64	416
1 2	6.47	4.70	441	473	4.45	4.76	6.41	4-79
9	7.88	5.29	7.26	5.38	7.93	5-35	7.21	5.38
10	1.04	1.88	8.06	241	1.04	7.37	3.81	5.98
11	8.90	6.47	8.87	6.50 7.10	9.65	6.54 7.74	9.61	6.58 7.18
113	9.71	7.04	9 68 10.48	7.66	20.45	7.23	10.48	7 -8
13	11.33	8.23	11.14	8.08	81.25	3.35	31.58	1.38
1.45	12.14	8.83	13.10	8.87	12.00	8.98	11.01	3 97
14	12.94	9.40	11.90	9.46	12.86	9.54	10.52	9.57
1 12	13 75	9 99	13.71	10.05	33.67 E4.47	14.75	19.62	10. 17 10. 77
1 18	14.56 15.37	10.58	14.52	10.64	5-87	11 30	15.22	11 37
19	18.18	11.76	16 13	1187	16 08	11.90	16.03	IL 97
1	16.99	15.34	10.94	18-42	16.98	15.09	16.83	13.50
23	19.80	12 93	17.74	13.01	17.68	19 09	17.63	13-16
23	18.61	13-52	18 55	13 60	18.49 19.19	13.68		13-78 14-38
1 23	19.43 80.33	14.69	19.35	14.19 14.78	20,10	14.87	10.01	14 90
36	21.03	15 18	20.g-	15.37	90.90	15-47	20.83	15.50
27	81.84	15.87	\$4-7	15 97	21.70	16.06	41.63	16.19
98	\$2.65	10.46	21 58	16.56	22,52	10.65	25.44	16.79
29	25 46	17.05	13-39	17.14	13.31 24.15	17.25	39.94 54.04	17-39 17-99
10	24 27	17 63	24-19	17.74		18.44	54 84	18 55
1 21	25.0E	18.22 48.81	\$5.00 \$5.8r	18.33	14.93	19 03		ونوا
35 33	26.70	19.40	28.61	19.51	20.53	19.01	25.44	19.74
34	47 SP	19.98	97.43	30.10	27.33	20.63	27.24 28.04	20.34
35	25.32	30.57	28.13	20 70	28 19	20 61		10.94
36	39 18	E 5. 10	29 03	#1.29 #1.88	28.94	21,41 23.05	28.85 29.65	21.54 22.14
37	29-93 30-74	81.75 82.34	39.54 30.64	22.47	30.55	22.60	30.45	1174
. 39	37.55	82.92	31.45	B3 06	32.35	B1.20	31.25	3.33
40	32.36	23.51	32.25	e3 65	32.15	23 79	32.05	25.93
41	33-17	FF 10	35.06	24.54	32.96	84 39	33.65	24.53
42	33.98	84.69 85.87	33.87 34.68	14.83 15.43	33-76 34-57	24.98 25.58	34-45	25.43 25.73
44	34-79 35-60	25.26	35-48	26.01	35-37	16.17	35. 20	24.33
45	38.41	16.45	16.1g	16.61	36.17	86 77	36.06	26.92
46	37.22	17.04	37.10	20 יב		27 36	36.86	27 52
47	38,02	17.53	37.90	\$7.79 \$9.48	37.78	27.96	37.66 38.46	2×11 2×11
1 4	38.83 . 39.64 .	28.80 28.80	38.7 £ 39-52	18.38 18.97	28.59	29.55	39,18	29 32
49 50	40.45	19.39	40.31	19-57	40.19	89.74	40.06	29.93
51	47.16	±9 98	41.13	30.16	41.00	30 34	43,86	30 51
52	43.07	30.56	41.94	80.75	41 \$0	10.93	41.67	31 11
53	43.58	\$1.15		\$1.34		31.53	48-47 43-27	31 ~ 1
[54]	43.6g 44.50	32-74 32-23		\$1.93 \$2.52	43.45	32.72	44.07	3291
-55	45.30	32.92		33-11	45 08	13-11	44.87	3, 50
56 57	46.13	13.50	45.97	33.70	45.81	33 90	45.67	34 10
38	46.92	34.09	45-77	843°	45.63	34-50	46.47	34-70
69 60	47-73	34-68	47.5	34-89	47 43 48.13	35.69	47-17 48-08	31 30
	48.54	35.47	48.39	35-48 Lat		Lat	Dep.	Late
벌	TDep.	LAL.	Dep.		Dep.	<u></u>		
9.1	0,		45	Mercali)/		51

	Dist	0		1	5*	3	01	45	2
	34	Lat.	Dep.	Let.	Dep	Lat.	Dep.	Lat.	Dep.
	61	49-35	35.85	49.19	136.07	49.04	36.26	48.88	86 50
	62	50.16	35.44	20.00	36.66	49.84	36.88	49.63	B7 10
	63	50197	37-03	54.61	37.25	50.64	\$7.47° \$8.07°	51.28	37.69 38.29
-	65	51.78	138.21	53.42	38.44	51.45	8.66	54.08	38.89
	66	53.40	\$8.79	53.23	39.03	53.09	19.36	52.88	89 49
1	67	54.20	39.38	54.03	39.62	53.86	\$9.85	53.6B	40.09
1	68	55:01	\$9.97	54.84	40.21	54.66	40.45	54-49	40.69
\cdot	70	55.82	40.56	55 64 56.45	40.80	55.47	41.54	55.29 56 Oy	41.88
:	71	57.44	41.73	57.26	41.98	57.07	42.23		42.48
•	72	58.25	42.92	5800	42.57	57.88	42.83	57.60	\$3.08
1	73	59.06	42.9F	58.87	43-17	58.68	43.42	58.49	43.68
	74	59.87 60.68	43.50	60.48 59:68	43.76	59-49 60.29	44.61	59.2y 60.09	44.28
	75	I ———	44.08	61.29	44-35	61.09		60.90	44.87
	76 77.	64.45 64129	44.67	64.10	44-94	62.90	45.80	61.70	45.47
Ì	78	63:10	45.85	62.90	46.12	64.70	46.40	62.50	46.67
	79.	63.94	46.43	63.71	46.71	63.50	46.99	63.30	47.27
	. 80	64.73	47.02	64.52	47.30	64.31	47.59	64.10	47 87
	8 t	65.53	47.61	65.32°	47.90	65.11 65.91	48.18 48.78	64.90	48.46
4	83	67.15	48.79	66:93	49.08	65.72	49-37	66.50	\$9.06
*	84	67.98	49.37	67.74	49.67	67.58	49-97	67.34	50.26
	85	68.77	49,96	68.55	50.26	68.33	50.56	68.14	50.86
•	85	69.58	\$0.55	69.35	\$0.85	69.13	\$1.15	68.91	\$1.46
•	87	70.38	\$1.14	70.46	\$1.44	70.74	\$1.75 \$2.34	78.51	\$2.0¢
}	89	72,00	52.31	73.77	52.63	71.54	52.94	74.38	\$3.25
]	90	72.81	\$2.00	72.58	53.22	72.35	53-53	78.18	53.85
	91	73.68	53.49	73.39	\$3.81	73.15	54.13	72.92	\$4.45
	9 2 93	74-43 75-24	54.66	74.49	54.40	73.95 .74.76	\$4.72	73.74	\$5.64
1	94	76.03	55.25	75.81	\$5.58	75.56	55.32	75.32	\$6.24
ł	95	76.86	55.84	7661	\$6.17	76.37	\$6.57	76.12	\$6 84
1	96	77.67	\$6.43	77.42	56.77	77.17	57.10	76.92	57.44
1	97 98	78.47 79.28	57.60	78.25	57-36	77.97 78.78	57.70 58.29	78.52	58.64 58.64
1	99	\$6.09	58.19	79.84	\$8.54	79.58	58.89	79.32	59.23
	100	80.90	58.78	80.64	59.13	80.39	59.48	86 13	\$9.83
1	101	81.71	59-37	82-45	59.72	81.19	60.08	80.93	60.43
	102	82.52	59-95	81.26 83.06	60.31	82.99 82.80	60.67	84.75	61.03
ļ	103	84.14	60.54	83.87	60.90	83 60	61.27	84.53	61.63 62.23
I	POS	84.95	61,72	84.68	62.09	84.41	62.46	84.13	62.82
	206	85.76	62.31	85.48	62,68	85.21	63.05	84.93	\$3.42
I	107	86.56	62.80	86.29	63-27	86.01	63.65	85.73	64.02
	106 10g	87.37 88.48	63.4 8 64.07	87.10 87.90	63.86 64.45	86.82 87.61	64.24 64.84	86.54 87.34	64.62 . 45.22
ł	OTÍ	88.99	64.66	88.71	65.04	88.42	65.43	88.14	65.82
I	311	89.80	65.24	89.52	65.64	89.23	66.03	88.94	66'41
I	112	90.61	65.83	90.32	66.23	90.03	66.62	89 74	67.01
ſ	114	91.42	66.42 67.01	91.15	66.82	90.84	67. 28 67.81	90.54	67.61
-	115	93.04	67.60		68.00	92 44	68 40	91.34	68.81
1	116	93.85	68.48	93-55	68.59	93:25	69.00	91.95	69.41
ı	117	94.65	68.77	94.35	169.18	94.05	69.59	93.75	70.00
ł	811	95.46	69.36		69.77	94.86	70.19		70.60
	119 120	9 6.8 7 97.08	69.95 70.53	95·97 96 ¹ 77	70.37 70.96	95.66 96.46	70.78 71.38		71.80
ſ		Dep.	Lat.	Dep.	Let.	Dep.	Lat.	Dep.	Lat
I	Dist.	U		45	1	30/	-	15	
٠,					DEGR				

Dist	0		15	7	30)/	4.5	{
7.	Let	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
]	0.80	0.60	0.80	0.61	D-78	,0,61	0.79	0.61.
] .2	1.60	1.20	1.59	1.82	2.38	1.83	₹.5¥ 2.37	1.32
3 4	2.40. 3.19	2-41	2.39 3.18	2.42	3.17	1243	3.16	2.45
5	3.99	301	3.98	3.03	3.97	3.04	3.95	3.06
6	4-79	3.61	4 78	3.63	4-76	3.65	4-74	3.67
2	5.59	4.21	5.57	4.24	5:55	4.26 ,4.87	5.53 6.33	4.39
8	7.19	4.81 5.42	6.37 7.16	4.84 5.45	6.35 7-14	5.48	7.12	4.90 5.51
10	7.99	6.02	7.96	6.05	7-93	6.09.	7.91	6.12
11	8.78	6.62	8.76	6.66	8.73	6.70	8.70	6.73
12	9.58	7.22	9.55	7-26	9.52	7-21	9.49	7.35
13	10.38	7.82 8.43	10.35	7-87 8-47	10.31	7.91 8.52	10.28	7.96 8.57
14	1198	9.03	11.94	9.08	11.90	9.13	11.86	9.18
16	12.78	9 62	12.74	9.68.	1269	9-74	12.65	9.20
. 17	13.58	10.23	13.53	10.29	13.49	10.35	13-44	10.41 .
18	14.38	10.83	14-35	10.90	14.28	10.96	14.23	11.63
19	15.17	12.04	15.12	11.50	15.87	12.18	15.81	12.24
31	16.77	12.64	16.72	12.71	16.66	12.78	16.60	12.86
22	17.57	13.24	17.51	13.32	1745	13.39	17.40	13.47
23	18.37	13.84.	18.31	13.92	, 18.25	14.00	18,19	14.08 14.69
24	19.17	14-44	19.10	14-53 15-13	19.04	14.61 15.22	19.77	15.31
26	19.97 20.76	15.65	19.90	15:74	20.63	15.83	20.56	15.92
27	21.56	16.25	21.49	16.34	21.42	16.44	21.35	16.53
28	22.36	16.85	22.29	16.95	22.21	17.05.	22.14	17 14
29	23.16	17.45	23.08	17.55	23.01 23.80	17.65 18.26.	23.93 23.72	17.75 18.37
30	23.96	18.66	23.88 24 68	18.76	24.59	18.87	24.51	18.98
31	24.76	19.26	25-47	19.37	25.39	19.48	25.30	19.59
33	26.35	19.86	26.27	19.97	26.18	20.09	26.09	20.20
34	27.15	20 46	27.06	20 58	26.97	20.70 21.31	26.88 27.67	20.82 . 21.43
35	27.95	21.67	27.86	21.19	28.56	21 92	28 46	22.04
36 37	28.75 29-55	22.27	29.45	21. 79 22. 40	29.35	22.52	29.26	22.95
38	30.35	22 87	30.25	23.00	30.15	23.13	30.05	23.26
39	31.15	43.47	31.04	23.61	30.94	23.74	30.84 31.63	23.88 24.49
40	31.95	24.07	31.84	24.21	31.73	24.35		
41 42	32.74 33.54	24. 67 25.28	32.64 33.43	24.82 25.42	32.53 3 3. 33*	24.96 25.57	32 42 33.21	25.10 25.71
43	34.34	25.88	34-23	26.03	34.11	26.18	34.00	16.33
44	35.44	26.48	35.02	26.63.	34.91	26.79	34-79 -	26.94
45	35.94	27.08	35.82	27.24	39.70	27.39	35.58	27.55 28.46
46	36.74	27.68 28.29	36.62 37.41	27 84 28.45	36.49 37-29	28.00 28.61	36.37 37.16	28.77
47	37·54 38·33	28.89	38.21	29.05	38.08	49.22	37-95	29.39
49	39.13	29 49	39.00	29.66	38-87	29.83	38.74	30.00
50	39.93	30.09	39.80	30.26	39.67	30.44	39-53	30.61
54	40.73	30.69	40.60	30.87		31.05	40.33	31.22
52 53	41.53	31.29 31.90	41.39	31.48 32.68	41.25	32.26	41.91	32.45
54	43.13	32.50	42.98	32.69	42.84	32.87	42.70	33.06
55	43.93	33.10	43.78	33.29	43.63	33.48	43.49	33.67
56	44-72	33.70	44.58	33.90	44.43	34 09	44.28	34.28
57 58	45.52 46.32	34.30 34.91	45·37 46.17	34.50 35.11	45.22 46.01	34.70 35.31	45.07	34.90 35.51
59	47.12	35.51	46.96	35.71	46 81	35.92	46.65	36.12
60		36.11	47.76	36.32	47.60	36.53	47.44	36.73
	47.92		•				-	
Dist.	Dep. 0/	Lat.	Dep. 45	Lat.	<u>Dep</u>	Lut	Dep.	Lat.

2 2. 2003.			42
بيموسيان بساعا	فيحث بجد ما حال في		· · · · · · · · · · · · · · · · · · ·
1	30'	1 -	45'

	U'	151	30'	45'
Dist.	Lat Dep.	Lat. D.p.	Lat. Dep.	Lat. Dep.
61	48.72 36 71	48.56 36.92	48.39 37.13	48.23 37.35
61	49.52 37.31	49.35 37.53	49.19 37.74	49.02 37.96
63	50.31 37.91	50.15 38.13	49.98. 38.35	49.81 38.57
64	51.11 38.52 51.91 39.12	50.94 38.74 51.74 39.34	50.77 3 8 96 51.57 39.57	50.60 39.18
66	52.71 39.72	52.54 39.95	51.57 39.57	51.39 39.79 52.19 40.41
. 67	53.51 40.32	53.33 40.55	53.15 40.79	52.98 41.02
68	54.31 40.93	54.13 41.16	53.95 41.40	53-77 41 63
69	55.11 41.53 55.90 42.13	54.92 41.77 55.72 44.37	54 74 42.00 55.53 42.61	55.35 42.86
71	56.70 42.73	56.52 42.98	55.53 42.61	
72	57 50 43.33	57.31 43.58	57.12 43.83	56.14 43.47 56.93 44.08
73	58.30 43 93	58.11 44.19	57.91 44.44	57.72 44.69
74	59 10 44.53	58. 90 44.79 59.70, 45.40	58.71 45.05 59.50 45.66	58.51 45.30
75 76	60.70 45.74	60.50 46.00	59.50 45.66	59.30 45.92 60.09 46.53
. 77	61 49 46.34	61.29 46.61	61.09 46.87	60.88 47.14
78	62.29 46.94	62.09 47.21	61.88 47.48	61.67 47.75
79 : 80	63.09 47.54	62.88 47.82 63.68 48.42	62.67 48.09 63.47 48.70	62.46 48.37 63.26 48.98
81	64.69 48.75	64.48 49.03	64.26 49.31	64.05 49.59
82	65.49 49.35	65.27 49.63	65.05 49.93	64.84 50.20
83	66.29 49.95	65.07 50.24	65.85 50.53	65.63 50.81
84 · 85	67.09 50.55	66.86 50.84 67.66 51.45	66.64 54.14	66 42 51.43
86	68.68 SI.76	68.46 52.06	88.23 52.35	68.00 52.65
87	69.48 52.36	69.25 52.66	69.02 52.96	68.79 53.26
88	70.28 52.96	69.05 53.27	69.62 53.57	69.58 53.88
89	71.08 53.56 71.88 54.16	70.84 53.87 71.64 54.48	70.61 54.18 71.40 54.79	70.37 54.49 71.16 55.10
91	72.68 34.77	72 44 55.08	71.40 54.79	
92	7347 - 55.37	73-23 55.69	72.99 56.01	71.95 55.71 72.74 56.32
93	74-27 155-97	74.03 56.29	73.78 56.61	73-53 56.94
94	75.07 56.57 75.87 57.17	74.82 56.90 75.62 57.50	74.58 57.22 75.37 57.83	74-32 57-55
95	76.67 57.77	75.62 57.50 76.42 58.14	75.37 57.83	75.12 58.16
7 .97	77-47 58.38	77.21 58.71	76.96 59.05	75.91 58.77 76.70 5 9.39
98	78.27 58.98	78.01 59.32	77.75 159.66	77.49 60.00
99	79.06 59.58 79.86 60.18	78.80 59.92 79.60 60153	78.54 60.27 79.34 60.88	78.28 60.61 79.07 61.22
101	80.66 60.78	RO.40 61.13	80.13 61.48	79.86 61.83
101	81.46 61.39	81.19 61.74	#3.92 62.09	80.65 62.45
103	82.26 61.99	81.99 62.35	81.72 62.70	81.44 63.06
104	83.86 63.19	82.78 46 2.95 83.58 63.55	82.51 63.31 83 30 63 92	82.23 63.67
106	84.66 63.79	84.38 64.16	84.10 64.53	83.81 64.89
1407	85.45 64.39	85.16 64.77	84.89 '65.14	84.60 65.51
108	86.25 65.00 82.05 65.60	85.97 65.37	85.68 (65.75	85.39 66.12
109	87.05 65.60 87.85 66.20	86.76 65 98 87.56 66.58	86.48 '66.36 87 27 66.96	86.19 66.73 86 98 67.34
111	88.65 66.80	88.36 67.19	88.06 67.57	87:77 67.96
112	89.45 67.40	89.15 67.79	88.86 (68.18	88.56 68.57
113	90.25 68.11 91.04 68.61	89.95 68.40	89.65 68.79	89.35 39.18
114	91.04 68.61 91.84 69.21	90.74 69.00 91.54 6 9.61	90.44 69.40 91.24 70.01	90.14 69.79 90.93 70.40
116	92.64 69.81	91.34 70.21	92.03 70.62	91.72 71.02
- 127	93.44 70.41	93.13 70.82	92.82 71.23	92.51 71.63
119	94.24 71.01	93.93 71.42	93.62 71.83	93.30 72.24
120	95.84 72.22	94.72 72.03 95.52 72.64	94.41 72.44 95.20 73.05	94.09 72.85 94.88 73.47
-	Dep. Lat	Dep. Lat.	Dep. Lat.	Dep Lat.
Dist	0'	45'	30'	15.
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Dig.	Lat.								
 		Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
	0.79	0.63	0.79	0.63	0.78	0.62	0.78	0.63	
2	1.58	1.33	las7	1.34	1.57	1.24	1.56	R35	
3	2.36	1.85	2.36	1.86	2.35	1.87	2.34	1.88	
. 4	3.25	3.44	3.14	2.48 3.10	3 13	2.49 3.11	3.42	2.50 3.13	
5	3.94	3.08	3.93	-	3.91	3.74	4.68	3.76	
6	4-73	3.69	4-74 5.90	3.71 4.33	4.70 5.48	4.36	5.46	4.38	
7 8	5.52	4.32	6.48	4.95	6.26	4.98	6.34	5.01	
9	7.00	5.54	7.07	5.57	7-04	5.60	7.02 7.80	5.63	
10	7 88	6.16	. 7.85	6.19	7.83	6.23		6.36	
21	8.67	6.77	8.64	6.81	8.6r	6.85	8.58 9.36	6.89 7.51	
12	9,46	7-3 9 8.00	9.42	7.43 8.05	9.39 10.17	8.09	10.14	8.14	
13	11.03	8.62	10.99	8.67	10.96	8.72	10.92	8.76	
15	12.82	9.23	11.78	9.29	11.74	9.34	11.70	9.39	
16	12.61	9.8;	12.57	9.91	12.52	9.96	12.48	10.01	
17	13.40	10.47	13.35	10.52	13.30	10.58	13.26	10.64 11.27	
18	14.58	8011	14.14	11.14	14.87	11.83	14.04	11.89	
19	14 97	11.70	14.92 15.71	£2.38	15.65	11.45	15.60	12.52	
]	16.65		16 49	43.00	16.43	13.07	16.38	13.14	
21 22	17-34	12.93 13.54	17.28	43.62	17.22	13.70	17.16	13.77	
23	18.12	14.16	. 18 06	14.24	18.00	14.89	17.94	14.40	
24	18.91	14.78	18.85	14.86	18.78	15.56	18.72 49.50	15.08 15.65	
25	19.70	15.39	19.63	15.48	19.57	16.19	20.48	16.27	
26	20.49	16.61	20.43	16.10	20.35	16.84	21.06	16.90	
27	21.28	87.24	21.99	17.33	21.95	17.43	21.84	17.53	
29	22.85	17.85	22.77	17.95	22.70	18.05	22.62	18.15	
30	23.64	18.47	23.56	18.57	23.48	18.68	23.40	18.78	
'31	24.48	19.02	24-34	19.19	24.26	19.30	24.18	19.40 20.0g	
3.	25.22	19.70	25.13	19.81	25.04 25.83	20 54	24.96 25.74	20.66	
33	26.00	20.33	25.92 26.70	20.43	26.61	21.17	26.58	21.28	
34	27.58	21.55	27.49	21.67	27.59	21.79	27.30	21.91	
36	28.37	22.16	28.27	22.29	28.17	22.41	28.08	22.53	
37	19.16	22.78	29.06	22.91	28.96	23.03	18.86	23.16	
38	29.94	23 40	29.84	23.53	89.74	23.66	29.64 30.43	23.79 24.41	
39	30.73	24.63	30.63	24.14 24.76	30.52	24.28 24.90	31.80	15.04	
40	31.52	-	31.41	25.38	32.09	25.52	31.98	25.66	
41	32.31	25.24 25.86	32.20	.00	32.87	26 15	32.76	26.29	
43	33.88	26 47	33.77	26.62	33.65	26.77	33.53	26.91	
44	34.67	27.09	34-55	87.24	3443	27-39	34 31	27.54 28.17	
45	35 46	27 70	35.34	\$7.86	35 22	28.01	35.09	28.79	
46	36.25	28.32	36.12	28.48	36.00 36.78	28.64 29.26	35.87 36.65	29.43	
47	37.94	28.94 29.55	36.91 37.70	29.10	37.57	29.88	37.43	30.04	
48	38.61	30.17	38.48	30.34	38.35	30.50	38.21	30.67	
50	39.40	30.78	39.27	30.95	39.13	31.13	38.99	31-30	
51	40.19	31.40	40.05	31.57	39.91	31.75	39.77	31.92	
52	40.98	32.01	40.84	32.19	40.70	32.37	40.55	32.55	
53	41.76	3263	41.62	32.81	41.48 43.46	32.99 33.62	41.33 42.11	33.80	
54	42.55	33.25 33.86	42.41 43.19	33·43 34.05	43.04	34.24	42.89	34-43	
55		34.48	43.98	34.67	43.82	34.86	43.67	35.05	
56 57	44.92	35.09	44.76	35.29	44.61	35.48	44 45	35.68	
\$8	45.70	35.71	45.55	35.91	45.39	36.11	45.23	36.30	
59	46.49	36 32	46.33	36.53	46.17	36.73	46.01 46.79	36.93 37.56	
60	47.28	36.94	47.12	37.15	46.96	37-35	Dep	Lat.	
Dist	1	Dep. Lat.		Dep Lat.				15/	
IE	0	/	45' 30' 51 DEGREES.				1 VA.		

1 9.	1 4	1	1 1:	5/	34	9/	45	1
Di st	Lat.	Dep.	Lat.	Uep.	Lat.	Dep.	Lat.	Dep.
61	48.07	37.56	47.90	37.76	47.74	37.97	47.57	38.18
62	48.86	38.17	48.69	38.38	48.52	38.60	48.35	38.81
63	49.64	38.79	49.47	39.00	49.30	39.22	49.13	39.43
64	50.43	39.40	50.26	39.62	50.09	39.84	49.91	40.06 40.68
65	51.28	40.02	51.05	40.24	50.87	40 46	50.69	
66	52.01	40.63	51.83	40.86	51.65	41 09	51.47 52.25	41.31 41.94
68	52.80	41.25	52.62 53.40	41.48 42.10	52 43 53.22	41.71	53.03	42.56
69	54-37	42.48	54.19	42.72	54.00	42.95	53 81	43.19
70	55.16	43.10	54.97	43-34	54.78	43.58	54-59	43.81
71	55.95	43.71	55.76	43.96	55-57	44.20	55-37	44.44
72	56.74	44.33	56.54	44.57	56.35	44.82	56.15	45.07
73	57.52	44-94	57 33	45.19	57.13	45.44	56.93	45.69
74	58.31	45 50	58.11	45.81	57.91 58.70	46.69	57.71 58.49	46.32 46.94
7.5	59.10	46.17	58.90	46 43	-			47.57
76	59.89	46.79	59.68 60.47	47.05 47.67	59.48 60.26	47.31 47.93	59.27 60.05	48,20
77 78.		47.41 48 02	61.25	48.29	61.04	48.56	60.83	48.82
79	62.25	48.64	62.04	48.91	61.83	49.18	61.61	49.45
80	63.04	49.25	62.83	49.53	62.61	49.80	62 39	50.07
81	63.83	49.87	63.61	50.15	63.39	50.42	63.17	50.20
82	64.62	50.48	64.40	50 77	64.17	51.05	63.93	51:33
83	65.40	51.10	65.18	51.38	64 9 6 65.74	51.67	64 73 65.51	51.95 52.58
84	66.19	51.72	65.97 66.75	52.00 52.62	66.52	52.91	66.29	53.20
•86			67.54	53.24	67.30	53.54	67.07	53.83
87	68.56	52.95 53.56	68.32	53.86	68.09	54.16	67.85	54.46
88	69.34	54.18	69.11	54.48	68.87	54.78	68.63	55.08
89	70.13	54-79	69.89	55.10	69.65	55.40	69.41	55.71
90	70.92	55.41	70 68	55.72	70.43	56.03	70.19	56.33
91	71.71	56.03	7146	56.34	71.22	56 65	70.97	56.96
92	72.50	56.64	72.25	56.96 57.58	72.00	57 27 57.89	71.75	57.58
93	73.28	57.26 57.87	73.03 73.82	58.19	73.57	58.52	73.31	58.84
95	74.86	58.49	74.61	58.8t	74-35	59.14	74.09	59.46
96	75.65	59.10	75.39	59.43	75.13	59.76	74-87	60.09
97	76.44	59.72	76 18	60.05	75.91	60 38	75.65	60.71
98	77.22	60.33	76.96	60.67	76.70	61.01	76.43	61.34
99	78.01	62.95	77.75	61.29	77.48 78.26	61.63	77.21 77.99	61.97
100	78.80	61.57	78.53	61.91		62.87	78,77	63.22
101	79.59	62.18 62.80	79.3 2 80.10	62.53 63.15	79.04 79.83	63.50	79-55	63.84
103	80.38 81.17	63.41	80.89	63.77	80.61	64.12	80.33	64.47
104	81.95	64.02	81.67	64.39	81.39	64.74	81.11	65.10
105	82.74	64.64	82.46	65.00	82.17	65.36	81.89	65 72
106	83.53	65.26	83.24	65 62	82.96	65.94	82.67	66 35
107	84.32	65.88	84 03	66.24	83.74	66.61	83.4.5	66.97
1108	85.1.1	66.49	84.81 85.60	65.86 67.48	84.52	67.23	84.23 85.01	67.60 68.23
1109	85.89 86.68	67.11	86.3 8	68.10	86.09	68.48	85.79	68.85
1		68.34	87 17	68.72	86.87	69.10	86.57	69.48
1112	87.47 88.26	68.95	87.96	69.34	87.65	69.72	87.35	70.10
1113	89.05	69.57	88.74	69.96	88.43	70.34	88.13	70.73
1114	89.83	70.19	89.53	70.58	89.22	70.97	10 88	71.36
4115	90.62	70.80	90.31	71.20	90.00	71.59	89.69	71.98
116	91.48	71.42	91.10	71.84	-	72.21	90.47	72.61
117	92.20	72.03	91.88 92.67	73.43	91.57 92.35	72 83 73.46	91.25	73.23 73.86
1118	92.99	73.26	93.45	73.67	93.13	74.08	92.81	74.48
120	94 56	73.88	94-24	74-29	93.91	74 70	93.59.	75.11
·{	Dep.	Lat.	D-p.	Lat	Dep.	Lat	Dep.	Lat
U.st.		'	45/		30'		15'	
		·	51	المارينيون		-		·

Dist.	- 01	1	A -	/	30)/	45	1
Sr.	Lat.	Dep	Lat.	Dep.	Jan 1	Dep.	Lat.	Dep.
1	0.78	0.63	0.77	0.63	0.77	0.64	0.77	0.64
2	1.55	1.26	1.55	1.27	1,54	1.27	1.54	1.28
3	2.33	1.89	2.32	1.90	2.31	191	2.31	1.92
4 5	3.11 3.89	2.52 3.15	3.10 3.87	2.53 3.16	3.09 3.86	2.54 3.18	4.84 4.08	2.56 3.20
- 6	4.66	3.78	4.65	3.80	4.63	3.82	4.61	3.84
7	5.44	4.41	5.42	4-43	5.40	4.45	5138	4.48
8	6.22	5.03	6.20	5.06	6.17	5.09	6.15	5.12
9	6.99	5.66 6.29	6.97	5.69	6.94	5.72 6.36	6.92 7.69	5.75
10	7.77		7.74	6.33	. 7.72		-	6 39
11	8.55 9 33	6.92 7.55	8.52 9.29	6.96 7.59	8.49 9.26	7.00 7.63	8.46 9.23	7.03 7.67
13	10.10	8.18	10.07	8.23	10.03	8.27	9.99	8.31
14	10.88	8.81	10.84	8.86	19.85	8.91	10.76	8.95
15	11.66	9.44	11.62	9.49	11.57	9.54	11.53	9.59
16	12.43	10.07	12.39	10.12	12 35	10.18	12.30	10.23
17	13.21 13.99	10.70	13.16 13.94	10.76	13.12	11.45	13.07	10.87
119	14.77	11.96	14.71	12.02	14 66	12.09	14.61	12.15
20	15.54	12.59	15.49	1265	15.43	12.72	15.38	12.79
21	16.32	13.22	16.26	13.29	16.20	13.36	16.15	13.43
22	17.10	13.84	17.04	13.92	16.98	13.99	16.91	14.07
23	17.87	14.47	17.81	14.55	17.75	14.63	17.68 18.45	14.71
24 25	19.43	15.73	19.36	15.82	19.29	15.90	19.22	15.35 15.99
26	20.21	16.36	20.13.	16.45	20.06	16.54	19.99	10.63
27	20 98	16.99	20.91	17.08	20.83	17.17	20.76	17.26
28	21 76	17.62	2168	17.72	21.61	17.81	21.53	17.90
29	22.54	18.25	22.46	18.35	22 38	18.45	22.30	18.54
30	23.31		23.23	18.98	23.15	19.08	23.07	19.18
31	24 .99 24 .87	19.51	24.01 24.78	19.61	23.92 24. 69	19.72	23.83 24.60	19.82 20.46
32	25 65	20.77	25.55	20.88	25.46	20,99	25.37	21.10
34	26 42	21.40	26 33	21.51	26.24	21.63	26.14	21.74
35	27.20	22.03	27.10	22.14	27.01	22.20	26.91	22.38
36.	27.98	22.66	27.88	22.78	27.78	22.90	27.68	23.02
37	28.75	23.28	28.65 29.43	23.41 24 04	28.55	23.53	28.45	23.66
38 39	29.53 30.31	23.91 24.54	30.20	24.68	30.09	24.31	29.22	24.30 24.94
40	31.09	25.17	30.98	25.31	39.86	24.44	30.75	25.58
41	31.86	25.80	31.75	25.94	31.64	26.08	31.52	26.22
42	32.64	26.43	32.52	26.57	3241	26.72	32.29	26.86
43	33.42	27.06	33.30	27.21	33.18	27.35	33.06	27.50
44 45	34·19 34·97	27.69 28.32	34.07 34.85	28.47	33.95	27.99	33.83	28.14
46	35.75	28.95	35.62	29.10	35 49	29.26	35.37	29.41
47	35.75	29.58	36.40	29.74	36.27	29.90	36.14	30.05
48	37.30	30.21	37.17	30.37	37.04	30.53	36.90	30.69
49	38.08	30.84	37.95	31.00	37.81	31 17	37.67	31.33
50	38.86	31.47	38.72	31.64	38.58	31.80	38.44	31.97
51 52	39.63	32.10	39.49	32.27	39.35	32.44 33.08	39.21	32.61
53	40.41	32.72	4C.27 41.04	32.90 3 3.53	40.12	33.71	40.75	33.25 33 89
54	41.97	33 98	41.82	34.17	41.67	34-35	41.52	34.53
55	42.74	34.61	42.59	34.80	42.44	34.98	42.29	35.17
56	43.52	35 24	43.37	35.43	43.21	35.62	43.06	35.87
57 58	44.30	35.87	44.14	36.06	43.98	36.26	43.82	36.41
59	45.85	36.50	44.91	36.70 3 ⁵ ·33	44-75	36.89	44.59	37 09 37-73
60	46.63	77.76	46.46	137.96	46.30	38.16	46.13	38.37
نه	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
Dist.	·	<u>;</u>	4.5			()/	-	5,
			·	DEGR				

Jy DE	CILLIA,	41
	2.04	A / A
15'	+ 30'	45'

Lat. 47.41 48.18 48.96 49.74 50.51 51.29 52.07 52.85 53.52 54.40 55.18 55.95	Dep. 38.39 39.02 39.65 40.91 41.54 42.16 42.79 43.42 41.05	Lat. 47.24 48.01 48.79 49.56 50.34 51.11 51.88 52.66	Dep. 38.60 39.23 39.86 40.49 41.13 41.76 42.39	30 Lat. 47.07 47.84 48.61 49.38 50.16	Dep. 38.80 39.44 40.07 40.71 41.35	Lat. 46.90 47.67 48.44 49.21 49.97	1)cp. 39.01 39.65 40.28 40.92
48.18 48.96 49.74 50.51 51.29 52.07 52.85 53.52 54.40 55.18	39.02 39.65 40 28 40.91 41.54 42.16 42.79 43.42	48.01 48.79 49.56 50.34 51.11 51.88 52.66	39 23 39.86 40.49 41.13	47.84 48.61 49.38 50.16	39·44 40 07 40.71	47.67 48.44 49.21	39.65 40.28
48.18 48.96 49.74 50.51 51.29 52.07 52.85 53.52 54.40 55.18	39.65 40.28 40.91 41.54 42.16 42.79 43.42	48.79 49.56 50.34 51.11 51.88 52.66	39.86 49.49 41.13 41.76	48.61 49.38 50.16	40 07 40.71	48.44 49.21	40.28
49.74 50.51 51.29 52.07 52.85 53.52 54.40 55.18	40.91 41.54 42.16 42.79 43.42	49.56 50.34 51.11 51.88 52.66	40.49 41.13 41.76	49.38	40.71	49.21	
50.51 51.29 52.07 52.85 53.52 54.40 55.18	40.91 41.54 42.16 42.79 43.42	50.34 51.11 51.88 52.66	41.13	50.16			40 92
51.29 52.07 52.85 53.52 54.40	41.54 42.16 42.79 43.42	51.11 51.88 52.66	41.76			• •• · · · · · /	41.56
52.07 52.85 53.52 54.40	42.16 42.79 43.42	51 88 52.66	•		41.98	50.74	42.20
52.85 53.52 54.40 55.18	42.79 43.42	52.66		51.70	42.62	51.51	42.84
55.18	_	and the second second	43.02	52.47	43.25	52.28	43.48
55.18	11.05	53.43	43.66	53.24	43.89	53.05	44.12
		54.21	44.29	54.01	44-53	53.82	44.76
55.95	44.68	54.98	44-92	54 79	45.16	54.59	45.40
56.73	45.31	55.76 56.53	45.55 46.19	55.56 56.33	45.80	55.36 56.13	46.68
	45.94 46.57	57.31	46-82			56.89	47.32
58.29	47.20			57 87	47.71	57.66	496
59.06	47.83	58.85	48.09	58.64	48.34	58.43	48.60
50 B4	48.46	59.63		59 42		59.20	49.24
_							49.88
_		_					50.52 51.16
		-		-			51.79
						_ `	52.43
_	-		-	64.04	52.79	63.81	53.07
65.28	52 86	65.05	53.15	64.82	53.43	64.58	53.71
	53.49		53.78		54.07		54.35
	54.12		54.41		54.70		54.99
			55.05				55.63 56.27
			56.32				56.91
	56.64	69.70	56.94	69.45	57.25	69.20	57.55
·	57.27	70.47	57.58	70.22	57.88	64.96	58.19
71.50	57.90	71.24	58.21	70.99	58.52	70.73	58.83
72.27	_				T .	-	59.47 60.11
	E I						60.75
		-	,	-			61.39
				74.85			62.03
76.16	61.67		62.01	75.62	62.34	75.35	62.66
76.94	62.30	76.60					63.30
							63.94
							64.58 65.22
					_		65.86
			65.80	80.25	66.15		66.50
8.1.60	66.08	81.31	66 43	81.02	66.79	80.73	67.14
82.38	66 71	82.09	67.07	81.79	67.42	81.50	67.78
							68.42
				84.11	•		69.06 69.70
	_			84 88			70.34
	1						70.98
87.04		86.73	70.86	86.42	71.24	86. 1 1	71.63
87.82	71.11	87.51	71.50	87.19	71.88		72.26
							72 90
			ļ				73.54
_							74.17
		_		_			174.01 175.45
92 48	74.89	92.15	75 29	9182	75.69	91.49	76 09
93.16	75.52	92.93	74.92	92.59	76.33		76.73
Dep.	Lat.	Dep.	Lat.	Dep.	Lat	Dep.	Lat.
- 0	, –	4	5'	3)'	1	51
	57.51 59.62 59.62 61.39 62.17 62.95 63.73 64.50 65.06 65.06 67.72 73.83 74.61 78.49 79.72 73.83 74.61 78.49 79.72 78.49 79.72 78.49 79.72 79.72 79.72 79.72 79.72 79.73 79.74 79.75 79	\$7.51 \$6.57 \$8.29 \$7.20 \$9.06 \$47.83 \$9.84 \$48.46 \$60.62 \$49.09 \$61.39 \$50.97 \$62.95 \$50.97 \$63.73 \$51.60 \$64.50 \$52.23 \$65.28 \$53.49 \$66.83 \$54.12 \$67.61 \$55.38 \$69.94 \$7.27 \$6.64 \$7.27 \$71.50 \$58.53 \$73.83 \$59.79 \$74.61 \$61.67 \$6.94 \$60.41 \$75.38 \$60.41 \$6.16 \$6.230 \$77.1 \$63.56 \$79.27 \$64.82 \$6.49 \$60.81 \$83.93 \$67.34 \$6.26 \$7.48 \$71.71 \$73.63 \$74.74 \$74.74 \$75.52 \$73.63 \$6.26 \$74.89 \$75.52	\$7.51	\$7.51 46.57 57.31 46.82 58.29 47.20 \$8.08 47.45 59.06 47.83 58.85 48.09 59.84 48.46 59.63 48.72 60.62 49.09 60.40 49.35 61.39 49.72 61.18 49.98 62.17 50.35 61.95 50.62 62.62	\$7.51 46.57 57.31 46.82 57.10 \$58.29 47.20 58.88 47.45 57.87 \$9.06 47.83 58.85 48.09 58.64 \$9.84 48.46 59.63 48.72 59.42 60.62 49.09 60.40 49.35 60.19 61.39 49.72 61.18 49.98 60.96 62.17 50.35 61.95 50.62 61.63 62.95 50.97 62.73 51.25 62.50 63.73 51.60 63.50 51.88 63.27 64.50 52.23 64.27 52.51 64.04 65.28 52.86 65.05 53.15 66.482 65.05 66.06 53.49 65.82 53.78 65.59 66.39 55.38 68.15 55.68 67.90 69.17 56.01 66.60 54.41 66.36 67.13 56.01 68.92 56.94 69.45 70.72 57.27 70.47 57.58 70.22 71.50 57.90 71.24 58.21 70.99 72.27 58.53 72.04 58.84 71.76 73.83 59.79 73.57 60.11 73.30 74.61 60.41 74.34 60.74 74.08 75.38 61.04 75.12 61.37 74.85 76.16 61.67 75.89 62.01 73.30 74.61 60.41 74.34 60.74 74.08 75.38 61.04 75.12 61.37 74.85 76.16 61.67 75.89 62.01 75.62 76.19 64.82 65.45 80.54 88.80 80.25 86.82 65.45 80.54 88.80 80.25 80.05 64.82 80.54 88.80 80.25 81.60 66.08 81.31 66.33 83.34 82.38 66.71 82.09 67.07 81.79 83.15 67.34 88.80 67.70 82.56 83.93 67.97 83.63 68.33 83.34 84.71 68.60 84.41 68.96 84.41 82.38 66.71 82.09 67.07 82.56 83.93 67.97 83.63 68.33 83.34 84.71 68.60 84.41 68.96 80.25 82.38 66.71 82.09 67.07 82.56 83.93 67.97 83.63 68.33 83.34 84.71 68.60 84.41 68.96 80.25 82.38 66.71 82.09 67.07 82.56 83.93 67.97 83.63 68.33 83.34 84.71 68.60 84.41 68.96 80.25 82.38 66.71 82.09 67.07 82.56 83.93 67.97 83.63 68.33 83.34 84.71 68.60 84.41 68.96 80.25 82.38 66.71 82.09 67.07 82.56 83.93 67.97 83.63 68.33 83.34 84.71 68.60 84.41 68.96 84.41 82.38 66.71 82.09 67.07 82.56 83.93 67.97 83.63 68.33 83.34 84.71 68.60 84.41 68.96 84.41 82.38 66.71 82.09 67.07 82.56 83.93 67.97 83.63 68.96 83.74 70.48 86.73 70.86 86.42 87.94 70.48 86.73 70.86 86.42 87.95 71.74 88.28 72.13 87.97 90.15 73.00 90.80 74.03 90.28 90.93 73.63 90.60 74.03 90.28 90.93 73.63 90.60 74.03 90.28 90.93 73.63 90.60 74.03 90.28 90.93 73.63 90.60 74.03 90.28 90.93 73.63 90.60 74.03 90.28 90.93 73.63 90.60 74.03 90.28 90.93 73.63 90.60 74.03 90.28 90.94 75.52 92.93 74.92 92.59 Dep. Lat. Dep. Lat. Dep.	\$7.51 46.57 57.31 46.82 57.10 47.07 58.29 47.20 58.88 47.45 57.87 47.71 \$59.06 47.83 58.85 48.09 58.64 48.34 59.63 48.72 59.42 48.96 60.62 49.09 60.40 49.35 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.19 49.61 60.20 50.62 61.62 50.22 61.64 60.60 50.62 61.62 50.22 60.25 61.64 62.27 53.15 66.83 65.49 65.82 53.78 65.49 65.49 65.64 69.82 56.32 67.13 55	\$7.51 46.57 57.31 46.82 57.10 47.07 56.89 58.29 47.20 58.08 47.45 57.87 47.71 57.66 59.06 47.83 58.85 48.09 58.64 48.34 59.63 60.62 49.09 60.40 49.35 60.19 49.61 59.97 61.39 49.72 61.18 49.98 60.96 50.25 60.74 62.17 50.35 61.95 50.62 61.63 50.89 61.51 62.67 51.60 63.50 51.88 63.27 52.16 63.70 51.88 63.27 52.16 63.70 51.82 63.73 51.60 63.50 51.88 63.27 52.16 63.00 65.28 64.27 52.51 04.04 52.79 63.81 65.28 52.83 64.27 52.51 04.04 52.79 63.81 65.28 52.85 65.05 53.15 64.82 53.43 64.58 66.06 53.49 65.82 53.78 66.83 54.70 66.83 55.38 68.15 55.68 67.90 55.97 67.66 68.92 56.94 69.45 57.25 69.20 77.22 57.27 70.47 57.58 68.65 70.22 57.88 69.96 77.22 57.88 69.96 77.22 57.88 69.96 77.22 57.88 69.96 77.22 57.88 69.96 77.23 58.53 72.04 58.84 71.76 59.16 71.50 77.23 57.90 71.24 58.21 70.99 58.52 70.73 73.83 59.79 71.24 58.21 70.99 58.52 70.73 73.83 59.79 71.24 58.21 70.99 58.52 70.73 73.83 59.79 71.24 68.21 70.99 58.52 70.73 73.83 59.79 71.24 68.21 70.99 58.52 70.73 73.83 59.79 73.27 60.11 73.30 60.43 73.04 74.34 60.74 74.85 61.00 73.81 74.61 60.41 74.34 60.74 74.85 61.00 73.81 74.61 60.41 74.34 60.74 74.08 61.00 73.81 75.58 60.45 75.60 62.64 76.39 62.97 77.16 63.61 73.90 77.46 65.20 76.60 62.64 76.39 62.97 77.16 63.61 73.90 77.49 65.49 77.16 63.61 73.90 77.49 65.49 77.16 63.93 77.44 63.27 77.16 63.61 76.88 78.42 66.43 81.02 66.79 83.63 68.33 68.33 68.33 68.33 68.33 68.33 68.33 68.33 68.33 68.33 68.73 66.15 79.96 68.54 80.54 65.97 82.56 68.06 82.27 79.18 80.05 64.82 79.76 65.17 79.48 66.15 79.96 65.17 79.48 66.15 79.96 65.17 79.48 66.15 79.96 65.17 79.48 66.15 79.96 65.17 79.48 66.15 79.96 65.17 79.48 66.15 79.96 65.17 79.48 66.15 79.96 65.17 79.48 68.28 79.76 65.17 79.48 69.23 85.18 69.60 84.81 79.82 70.73 89.60 70.23 85.65 70.60 85.34 70.48 80.95 70.48 80.95 70.48 80.95 70.23 85.65 70.60 85.34 70.48 80.95 70.48 80.95 70.23 85.65 70.60 85.34 70.48 80.95 70.70 88.49 70.48 86.73 70.86 87.47 71.88 86.99 70.70 74.26 91.38 70.40 91.88 70.99 70.70 74.26 91.38 70.40 91.88 70.99 70.70 74.26 91.38 70.60 74.03 90.28 74.42 89.95 70.70

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1	Diec	01		15	/	30)1	45	-
1	77	Let.	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
	1	0.77	0.64	0.76	0.65	0.76	0.65	0.76	0.65
ł	3	1.53 2.30	1.93	1.53 2.29	1.29 1.94	1.52	1.30	1.52 2.27	1.31
I	4	3.06	2.57	3.05	2.58	3.04	2.60	3.03	2.61
ŀ	5	3.83	3.21	3.82	3.23	3.80	3.25	3.79	3.26
1	6 7	4.60 5.36	3.86 4.50	4.58 5.34	3.88 4.52	4.56 5.32	3.90 4.55	4.55 5.30	3-92 4-57
1	8	6.13	5.14	6.11	5-17	6.08	5.20	6.06	5.22
Į	9	6.89 7.66	5.79 6.43	6.87 7.63	5.82 6.46	6.84 7.60	5.84	6.82	5-87
ŀ	11	8.43	7.07	8.40	7-11	8.36	7.14	8.33	7.18
1	12	9.19	7-71	9.19	7-75	9.12	7.70	9.09	7.83
ł	13	9.96 10.72	8.36 9.00	9.92 10.69	8.40 9.05	9.89 10.65	8.44	9.85	8.49
ł	15	11.49	9.64	11.45	9.69	11.41	9.09 9.74	10.61	9.72
ľ	16	12.26	10.28	12.25	10.34	1217	10.39	12.13	10.44.
1	17 18	13.02	10.93	12-97	10.98 1 1.6 3	12.93	11.04	12.88	11.10
I	19	14.55	11.57 12.21	13.74	12.28	13.69 14.45	11.69	13.64	11.75
1	20	15.32	12.86	15.26	12.92	15.21	12.99	15.15	13.06
1	21	16.85	13.50	26.03	13-57	15.97	13.64	15 92	13.71
1	23	17.62	14-14	16.79 47.55	14.21	16.73 17.49	14.29 14.94	16.67	14.36 15.01
ł	24	18.39	15.43	18.32	15.51	18.25	15.59	18.18	15.67
ŀ	25	19.15	16.07	19.08	16.15	19.01	16.24	18.94	16.32
ł	27	19.92 20.68	16.71	19.84 20.61	16.80	19.77 20.53	16.89	19.70	16.97 17.62
I	28	21.45	18.00	21.37	18.09	21.29	18.18	23.25	18.28
1	29 30	22.98	18.64	22.90	18.74 19.38	22.81	18,83	21.97	18.93
ł	.31	23.75	19-93	23.66	20.03	23.97	20.13	23.48	20.24
ł	33	24.51	20.57	24.42	20.68	24-33	20.78	24.24	20.89
I	33 34	25.28 26.05	21.85	25.19 25.95	21.32	25.85	21.43	25 00	26.54
1	35	26.81	22.50	20.71	22.61	26.61	22.73	26.51	22.85
1	36	27.58	23.14	27.48	23.26	27.37	23.38	27.27	23.50
ł	37 38	28.34 29.11	23.78 24.43	28.24 29.00	23.91 24.55	28.12	24.03	28.03	24.15
ł	39	29.88	25.07	29-77	25.20	29,66	24.68 25.33	29.54	24.80
ı	40	30.64	25.71	30.53	25.84	30 42	25.98	30.30	26.11
ł	41	31.41	26.35	31 29 32.06	26-49 27-14	31.18	26.63	31.06	26.76
ł	43	32.94	27.64	32.82	27.78	31.94	27.28 27.93	31.82	27.42 28.07
1	44	33.71	28.18	33.58	28.43	32.46	28.58	33.33	28.7=
	45.	34-47	28.93	34-35	29.73	34.22	29.23	34.09	29-37
1	47	36.00	30.21	35-11 35-87	30.37	34.98 35.74	30.52	34.85	30.03°
	48	36 77	30.85	36.64	31.02	36.50	31.17	36.36	31-33
I	49 50	37-54	31.50	37.40 38.16	31.66	37 26 38.02	31.82	37.12 37.88	31-99 32.64
	ŞI	39.07	32.78	38.92	32.95	38.78	33.12	38.64	33.29
ł	52	39.83	33-42	39.6 9	33.60	39.54	33.77	39-39	33.94
	53 54	40.60	34-07 34-71	40.45 41.21	34.24 34.89	40.30	34-42 35-07	40.15	34.60 35.25
	55	42.13	35-35	41.98	35.54	41.82	35.72	41.67	35.90
	5 6	42.90	36.00	42.74	36.18	42.58	36-37	42.45	36.55
	57 58	43.66 44.43	36.64 37.28	43.50	36.83 37.48	43-34 44-10	37.02 37.67	43.18	37.21 37.86
	59	45.20	37.92	45.03	38.13	44.86	38.32	44-79	38.51
	60	45.96	38.57	45.79	38.77	45.62	38.97	45.45	39.17
	Dist.	Dep.	Lat.	Dep.	Lat.	Dep.	Lut.	Dep.	Lat.
4		0	·	4	DEG	3()'	1) '

49 DEGREES,

H	1 0	i	15	, ,	3()/	45	
Dist.	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.
6:	46.73	39.21	46.56	39.41	46.38	39.62	46.21	39.82
62	47.49	39.85		40.06	47-15	40.27	46.97	40.47
63 64	48.26	40.50		40.71 41.35	47.91 48.67	40.92 41.56	47·73 48.48	41.12 41.78
65	49.79	41.78		42.00	49.43	42.21	49.24	42.43
66	50.56	42.42		42.64	50. 19	42.86	50.00	43.08
67	51.32	43.07	51.14	43.29	50.95	43.51	50.76	43.73
68	52.09	43.71	51.90 52.66	43.94 1	51.71 52.47	44.16 44.81	51.51 52.27	44-39 4 5 -04
69 70	53.62	44.35	53-43	45.23	53.43	45.46	53.03	45.69
71	54-39	45.64	54.19	45.87	53-99	46.11	53.79	46.35
72	55.16	46.28	54.95	46.52	54-75	46.76	54-54	47.00
73	55.92	46.92	55.72 5 6.48	47.17 47.81	5.5.5 P 56.27	47.41	55.30	47.65
74 75	56 69	47·57 48.21	57.24	48.46	57.03	48.71	56.82	48.96
76	58.22	48.85	58.01	49.11	57-79	49.36	57-57	49.61
77	1 ~	49-49	58.77	49-75	58.55	50.01	58.33	50.26
78	59-75	50.14	59-53	50.40	59.31	50.66	59.09	50.92
79	60.52	50.78	60.30	51.69	60.07	51.31	59.85	51.57
81	62.05	52.07	61.82.	52.34	61.59	52.01	61.36	52.87
82		52.71	62.59	52.98	62.35	53.25	62.12	53.53
83	63.58	53.35	63.35	53.63	63.11	53.90	62.88	54-18
84	64.35	53-99 54-64	64.11	54-27 54-92	63.87	54-55	63.64	54.83 55.48
86		55.28	65.64	55.57	65.39	55.85	65,15	56.14
87			66.40	56.21	66.16	56.50	65.91	56.79
88	67.41	56.57	67.16	56.86	66.92	57-15	66.67	57.44
89		57 21	67.93	57.50	67.68	57.80	67.42	58.10
90	-	_		58.25			68.94	59.40
91			69.45	59-44	69.20	59-75	69.70	60.05
93	_	59.78	70.98	60.09	70.72	60.40	70.45	60.71
94	72.01			60.74	71.48		71.21	62.36
9		_	72.51	61.38	72.24	61.70	71.97	62.66
90			73.27	62.03 62.67	73.00	62.35	72.73	63.32
9			74.80	63.32	74.52	63.65	74.24	63.97
9	75.84		75.56	63.97	75.28			64.62
120		~ 	76 32	64.61	76.05			65.28
10	1 . 7		77.09	65.26	76.80 77.56		76.51	65.93 66 58
10	1 ^		78.61	66.55	78.32	66.89	78.03	67.23
10.	4 79.67	66.85	79.38	67.20	79.08			67.89
10				67 84	79.84		79-54	68.54
10				68.49 69. E4	80.60		80.30 81.06	69.19 69.85
10	_				82.12		81.82	70.5C
10	9 83.50	70.06	83.19	70.43	82.88	70.79		71.15
ER			83.96		83.64		83.33	71.8c
112	1 85.03	71.36	84.72	71.72	84.41	72.09	84.09	72.46
11	1 6 6 7				85.17	72.74	1	73-11 73-76
11	4 87.3	73.28	87.21	73.66	86.69	74 04	86.36	74.41
32						~		7.5 07
11		1			88.21			75.72
11				· 2				
112	1 -			-		1 -	90.15	77.68
12	- : -	1	91.59	_	91.25	77-93	90.91	78.3
	Dep.	Lat.	~	Lat.	Dep.		Dep.	Lat
1	Dep.	0*		151		Q'	1	5'
	-		40	DEGR	RES			

+ 0	1 0		- 13	5/	30		45	
Dist.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.75	0.66	0.75	0.66	0.75	0.66	0.75	3.67
2	1.51 2.26	1.31	1.50 2.26	1.32	1.50 2.25	1.33 1.99	1.49 2.24	1.33 2.00
3 4	3.02	2.62	3.01	2.64	3.00	2.65	2.98	2.66
5	3.77	3.28	3.76	3 30	3.74	3-31	3 73	3.33
6	4.53	3.94	4.51	3.96	4.49	3.98	4.48	4.00 4.66
7	5.28	4-59 5.25	5.26 6.01	4.62 5.27	5.24 5.99	4.64 5.30	5.22 5.97	5.33
8	6.04	5.90	6.77	5.93	6.74	5.96	6.71	5.99
9	.7-55	6.56	7.52	6.59	7.49	6.63	7.46	6.66
11	8.30	7.22	8.27	7.25	8 24	7 29	8.21	7·3 ² 7·99
12	9.06 9.81	7.87 8.53	9.02 9.77	7.91 8.57	8.99 9 74	7.95 8.61	8. 9 5 9.70	8 66
13	10.57	9.18	10.53	9.23	10.49	9.28	10.44	9.32
14	11.32	9.84	11.28	9.89	11.23	9.94	11.19	9.99
16	12.08	10.50	12.03	10.55	11.98	10.60	11.94	10.65
17	12.83	11.15	12.78	11.21	12.73 13.48	11.93	13.43	11.99
18	14.34	12.47	14.28	12.53	14.23	12.59	14.18	12.65
20	15.09	13.12	15.04	13.19	14 98	13.25	14.92	17.32
21	15.85	13.78	15.79	13.85	*5.73 f 6.48	13.91	15.67 16.41	13.98 14.65
22	16.60 17.36	14.43	16.54 17.29	14.51	17.23	14.58 15.24	17.16	15.32
23	18.11	15.75	18.04	15.82	17.97	15.90	17.91	15.98
24	1887	16.40	18 80	16.48	18.72	16.57		16.65
26	19.62	17.06	19.55	17.14	19.47	17.23 17.89	19.40 20.14	17-31 17.98
27	20.38	17.71 18.37	20.30 21.05	18.46	20.97	18.55	20.89	18.64
28 29	21.89	19.03	21.80	19.12	21.72	19.22	21.64	19.31
30	22.64	19.68	22.56	19.78	22.47	19.88	22.38	19.98 20.64
31	23 40	20.34	33.31	20.44	23.22 23.97	20.54 21 20	23.13 23.87	21.31
32	24 15 24.91	20.99 21.65	24:06 24:81	21.76	24.72	21.87	24.62	21.97
33 ³	25.66	22.31	25.56	22 42	25.46	22.53	.25.37	22.64 23.31
35	26.41	22 96	26.31	23.08	26.21	23.19	26.86	23.97
36	27.17	23.62 ° 24 27	27.07 ° 27.82	23.74 24 40	26.96 27.71	23.85 24.52	27.60	24.64
37 38	27.92 28.68	24.93	28.57	25.06	28 46	25.18	28.35	25.30
39	29.43	25.59	29.32	25.71	29.21	25.84	29.10 29.84	25.97 26.64
40	30.19	26.24	30.07	26.37	29.96	26.50	30.59	27 30
41	30.94	26.90 27.55	30.83	27.03 27.69	30.71	27 17 27.83	31.33	27.97
42 43	31.70 3 2. 45	28.21	32.33	28.35	32.21	28.49	32.08	28.63
44	33.21	28.87	33.08	29.01	32.95	19.16 19.82	32.83 33.57	29.30 29.97
45	33.96	29.52	33.83	29.67	33.70	30.48		30.63
46	34.72 35.47	30 18 30.83	34.58 35.34	30.33 30.99	34.45	31.14	35.06	31.30
47 48	36.23	31.49	36.09	31.65	35.95	31.81-	35.81	31.96 32.63
49	36.98	32.15	36.84	32.31 32.97	36.70	32.47 33 13	36.56 37.30	32.03
50	37.74	32.80	$\frac{37.59}{3834}$	33.63	37.45	33:79		33.96
51	38.49 39.24	33.46 34.12	30 34	34.29	38.95	34.46	38.79	34.63
52 53	40.00	34.77	39.85	34.95	.39.69	35.12	39.54	35.29 35.96
54	40.75	35.43	40.60	35.60 36.26	40.44	35.78 36.44	40.29 41.03	36.62
55	41.51	36 08	41.35	36.92	41.94	37.41	41.78	37.29
55	42.26 43.02	36.74 37.40	42.10 42.85	37.58	42 69	37· 77	42.53	37 96
57	43.77	38.05	43.61	38.24	43.44	38.43	43.27	38.62
59	44.53	38.71	44.36	38.90 39.56	44.19	39.09 39.76	44.02 44.76	39.29 39.95
60	45.28	39.36	45.11 Dep	139.50 Lat.	Dep.	Lat.	Dep.	Lat.
Dist.	De p.	Lat.	Dep 4:		30		خبيــــــــــــــــــــــــــــــــــــ	57
<u> </u>	(0'			DEGRI				<u>`</u>

48 DEGREES

91	0/		15/	ſ	3	0/	4	-
Dist	kat	Dea.	Late	Dop.	i.a.	Dep.	Lat	Der
61	46.04	40.02	45 86	40.22		<u> </u>		40.61
63	46 79	40.68	46.61	40 88	45.49 46.44	40.42 [41.08	45.51	41.18
63	47.55	41-33	47 37	41-54	47.18	41.75	47.00	41.95
64 65	48.30 49.06	41.99	48.11	42.20	47.93	42.41	47-75	42.62
66	49 81	42.64		42.86	48.68	43.07	48.49	43.18
67	50.57	43.30 43.96	49.62	43 52	49 43	43 73	49-24	43.95 44.61
68	51.32	44.61	51,13	44.84	50.93	45.06	49-99 50.73	45.28
69	52.07	45-27	51.88	45-49	51.68	45.72	51.48	45.95
70	52.83	45.93	52.63	46 15	52 43	46.38	52.22	46.61
71 73	53 58 54-34	46.58	53.38	46.81	53 18	47.05	52-97	47 28
73	55 Og	47.89	54.13	47 47	53-92 54-67	47 7 L 48.37	53.72	47.94 48.61
74	55.85	48.55	55.64	48.79	55.42	49.03	55.21	49.28
75	56.60	49.20	56.39	49.45	55 17	49.70	55.95	49.94
26	57.36	49.86	\$7.14	50.11	56.92	\$0.36	56.70	50.61
-9	58.11	50 52 . 51 67	57.8g 58.64	50.77	\$7.67	51.02	57.45	\$1.27
-70	50.62	51 83	59.40	51 43 52,04	58.42	51.68 52.35	58.19	54-94 52 60
80	60 38	. 2 48	60.15	\$1.75	\$9.92	\$3.01	59.68	53-27
81	61.13	53 54	60.90	53-41	60.67	53.67	60.43	53.94
82	61.89	53.80	61.65	54.07	61.41	\$4-33	61.18	54.60
8; 84	63.40	\$4-45	62.40	54 73 55 38	62 16	\$5.00	5010	\$5.27
8,	64.15	55.76	63.91	50.04	62.91 63.66	55 66 56.31	62.67 63.41	55.93 56.60
86	64.90	56.42	64.66	56.70	64.41	56 99	64.16	57-27
87.	65.56	\$7.08	65 41	57.36	65 16	57.65	64.91	57-93
88	14.66	57-73	66.16	58.02	65.91	5831	65.65	58.60
99	67.17 67.92	58 39 59.04	66.91 67.67	58.68 59.34	66.66	58 97	66.40	59.26
10	68.68	59.70	68.42	60.00	68 15	59 64 60 30	67.15	59- <u>93</u> 60.60
92	69.43	60.36	69 17	60.66	68 90	60 g6	68 64	61 29
93	70.19	61.01	69.92	61 32	69.65	6162	69.38	61.93
94	70.94	61,67	70.67	61.98	70-40	62 29	70.13	62.59
95	71.70	62.33	71.42	61.64	74.15	62 95	70.88	63.26
96 97	72.45	62.98 63 64	72,18 7493	63.30 63.96	71.90	6; 6:	71.62	63.92
98		64.29	73 68	64.62	73.40	64.94	73 14	65.26
99	74.72	64.95	74.43	65.28	74-15	65.60	73 86	65 92
100	75 47	65 61	25.18	65 93	74-90	66.26	74-61	66.59
101	76.98	66.26	75-94	66.59	75 64	66.92	75-35	67.25
103	77.74	66.92 67.57	76.69 . 77.44	67.91	76.39	67.59	76.10 76.84	68,59
104	78.49	68.23	78.19	68 57	77.89	68.91	77.59	69.25
105	79-24	68 89	78 94	69 23	78 64	69.58	78.34	69.91
106	80.00	69 54	79 70	69 8 9	79-39	70.24	79.08	70.58
103	80.75 81.51	70.20	80.45	70.55	85.14	70 90	79.83	71.25
103	82,26	71.51	81.95	71.87	83.89 81.64	71 56 72 23	80-57 81.32	71.92 72.58
110	83.01	72.17	82.70	72 53	82.38	72.89	82.07	73 25
111	83 77	72 82	8345	73 19	85.13	73.55	82.81	73 91
112	84.53	73 48	84.21	73 85	83.88	74 21	83.56	74 58
113	85.28 86 04	74.13	84-95	74-51	84-63	74.88	84.30	75 24
115	-86.79	74-79	85.71 86.46	75.82	85.38 86.13	75-54	85.80	75.91 76.59
116	87 55	76.10	87 21	76.48	86.88	76.86	\$6.54	77 24
117	88,30	76.76	87.97	77 14	87.63	77-53	87.29	77.9t
118	89.06	77-42	88.72	77 80	88.38	78. tg	88.03	78.57
11y 122	8 y 8 r 90.57	78.07 1 178.73	89.47	*8.46 *4.12	89.13	78.85	88.78 89.53	79 24
	Dep.	lat.	Dep	Tat.		79-51 Lat.		79.97
Dist	1×1×		45		Dep.		Dep.	Lat
		-		-	30		1	
			48	DEGR	APARENT.			

l A		y	1	15/	1	30'	, (6'
Disc	Let.	Dep.	Lat.	Dep	Lat.	Dep	_[Dep.
		0.67	0.74	0.67	0.74	0.68	0.73	0.68
1 2		1.34	1.48		1	V -	1.47	1.36
3 4	2.23 2.97	2.01 2.68	2.96	_		_	2.20	2.04
5	3.72	3.35	3.70		3.69	_	3.67	3.39
6	4.46	401	4.44		4-41		4-41	4.07
7 8	5.20	4.68 5.35	5.92		5.16		5.14	4-75 5-43
9	6.69	6.02	6.66	6.05	6.64	1 2 -	6.41	6.11
10	7 43	6.69	7-40		7.37	-	7-34	6.79
111	8.17	7.36	8.14 8.88	7-40	8.12		8.08	7-47
13	8.92 9.66	8.03	9.61		9.58	' I	9-55	8.15
14	10.40	9 37	10.36	9.41	10.32	_	10.28	9.50
15	11.15	10.04	11.10	_	11.06	_	11.01	10.18
16	11.89	10.71	11.84	_	11.80		11.75	10.86
17	12.63	11.38	12.58	11.43	12.53		12.48	11.54
119	14.12	12.71	14.06	12.77	14.01		13.95	12.90
20	14.86	13.38	14.80	13.45	14.75	13.51	14.69	13.58
31	15.61	14.05	15.54	14.12	15.48		15.42	14.25
22 23	16.35	14.72	16.28	14.79	16.22 16.96	14.86	16.89	14.93 15.61
24	17.84	16.06	17.77	16.14	17.69	16.21	17.62	16.29
25	18.58	16.73	18.51	16.81	18.43	16.89	18.36	16.97
26	19.32	17.40	19.25	17-48	19.17	17-57	19.09	17.65
27 28	20.06	18.07	19.99	18.15	19.91	18.24	19.83	18.33 19.01
39	21 55	19.40	21.47	19.50	21.38	19.59	21.30	19.69
30	22.29	20.07	22.31	20.17	23.12	20.27	22.03	20.36
31	23.04	20.74	82.95	20.84	32.86	20.94	22.76	21.04
32 33	23.78 24.52	21.41 22.08	23.69 24 43	21.52	23.59 24.33	21.62	23.50 24.23	21.72 22.40
34	25.27	22 75	25.17	22.86	25.07	22.97	24.97	23.08
35	26.01	23.42	25.91	23.53	25.80	23.65	25.70	23.76
36	26.75	24.09	26.65	24.21	26.54 27.28	24.32	26.44	24-44
37 38	27.50 28.24	24-76 25-43	27.39 28.13	25.55	28.04	25.00	27.17 27.90	25.13 25.79
39	28 98	26.10	28.87	26.22	28.75	26 35	28.64	26.47
40	29.73	26.77	29.61	26.89	29.40	27.02	29.37	27.15
41 42	30.47 31.21	27.43 28.10	30.35 31.09	27.57 28.24	30.23	27.70 28.37	30.11 30.84	27.83 28.51
43	31.96	28.77	31.83	28.91	30.97 31.70	29.05	32.58	29.19
44	32.70	29.44	32.57	29.58	32.44	29.73	32-31	29.87
45	33.44	30.11	33.31	30.26	33.18	30.40	33.04	30.55
46 47	34.18 34.93	30.78 31.45	34.05 34.79	30.93 31.60	33.91 34.65	31.08		31. 22 31.90
48	35.67	32.12	34·/ 9 35· 53	32.27	35.39	32.43		32.58
49	36.41	32.79	36.27	32.95	36.13	33.10	35.98	33.26
50	37.16	33.46	37.01	33.62	36.80	33.78		33.94
51 52		34-13 34-79	37-75 38.49	34.29 34.96	37.60 38.34	34. 46 35.13		34-62 35-30
53		35.46	39.23	35.64	39 08	35.81	38.92	35.98
54	40.13	36.13	39.97	36.31	39.81	36.48	39.65	36.66
55		36.80	40.71	36.98	40.55	37.16		37-33
56	_	37·47 38.14	41.45	37.65 38.32	41.29 42.02	37.83 38.51		38.01
57 58		38.81	42.19	39.00	42.76	39.18	•	39-37
59	43.85	39.48	43.67	39.67	43.50	39.86	43.32	paos
60	44-59	40.15	44-41	40.34	44.24	40.54		10.73
Dist.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
5	01	1	45		30′		15/	
	-	_	4	7 DEG	rees.		•	

				_	E EPIGNAL		•	7,44 7	40
1	U.	0	<u> </u>	1	5/	3	9/	4	5/
ı	1	1_at	Dep.	Lat	Dep.	Lat.	Dep	Lat	Bep.
1	61	45-33	40.81	45-15	41.01 .	44-97	41.41	44-79	4141
	61	46.07	41.49	45.89	41.69	45.71	41.80	45-53	42 09
1	61	46.81	42,16	46.63	42.36	46.45	42-56	45.16	42.76
1	64	47.56	41 82	47-37	43.03	47.19	43-24	47.00	43-44
į	64		43.49	48.17	43.70	47-92	43.9t	47.73	44.10
-1	66	49 05	44,16	48.85	44-38	48.65	44-59	48.47	44.80
-1	6-	49.79	44.83 45.50		45.05	49.40	45.26	49.20	45.48
١	48	51 28	46.17	50.3₫ €1.07	45.72 46.39	50.13	45.94 46.62	49-93 50.67	46.84
ł	70	51.01	46.84		47.07	St. St	47.29	51.40	47-52
ŀ		52.76	47.51	52-56	47.74	52.35		52.14	45.19
1	71 73	53.51	48.18	53.30	48.41	51.08	47:97 48.64	52.87	48 87
1	73	\$4.25	48,85	54-04	49.08	53.82	49 32	53.61	49.55
٦	74	54 99	49.58	54.78	49.76	54-56	49-99	54-34	50.23
ı	75	55-74	50.18	55.53	50.43	55.30	50.67	55.07	50.91
ı	76	56.48	50.85	56.26	51-10	56.03	51-34	55.81	51.59
ı	77.	57.32	51 52	57.00	51.77	56.77	\$2.02	59.54	52.27
1	78"	57.97	\$2.19	57.74	51.44	57-5¢	52.70	57 28	52.95
1	79.	58.71 59-45	53.86	58.48	53 12	58.98	53 37	58.01 58.75	13 63
1	_			59.23	53.29		54-05		54-30
ł	81	60.19	\$4.30 \$4.87	59 96 60.70	54-46	59.71 60.46	54-72	199.48 60.21	54-98 55 66
١	81	61.68	55-54	61.44	\$5,23 \$5,81	61.19	\$ \$.40 \$ 6.07	60.95	56.34
4	84	62.41	56.dr	62.18	16.48	61.93	\$6.75	61.68	57.02
1	8 ;	63.17	56 88	61.g2	57.15	.62.67	57-43	63.43	\$7.70
1	50	63.91	\$7-55	63 66	57.82	63.41	58 LD	63.15	58.38
i	87	64 65	58.24	64.40	58.50	64-14	58.7B	63.89	59.06
1	86	65.40	58.88	65 14	59-17	64.88	59-45	64.62	59.73
4	89	66.88	\$9.55	65.88	59.84	65.62	60.13	65 35	60.41
-	93		60.83	66.62	60 41	66.15	60.80	66.09	61.09
ŀ	91	67.63	60,89	67 36	61.19	67.09	61.48	66.83	61,77
Ī	93	6g.11	61.56	63,10	61.86 61,53	67.83	63.15	67.56 68.29	62.45
-	93	69.86	62.90	69.58	63 20		63.51	69.03	63.81
ı	91	70 00	63 47	70.32	63.87		64.48	69.76	64.49
1	96	71.34	64.24	71.06	64.55	70.78	64.86	70-49	65.16
1	97	71,08	64.gi	71.80	65.22	71.52	65 53	71 33	64.84
1	98	72.83	65.57	72.54	65.89	72.25	66.21	71 96	66 52
1	99	73-57	66.24	73.28	66 56	73.99	65.88	72,70	67.20
ł	100		66.gt	74.02	67.14	73.73	67.56	73.43	67 88
ł	101	75.00	67.58		67.91	74-46	.68.23	74.17	68 56
i	103	75.80 76.54	68,25 6K.92	75.50 76.24	68,58 69.25	75-20	68.91	74.90	69.44;
Ì	104	77.29	69.59	76.98	69 93	75-94	70.26	75 64 76 37	70.60
ľ	205	78.03	70.16	77 72	70 60	77-41	70.94	77.10	71 274
1	106	78.77	70.93	78.45	71.27	78.15	71.61	77.84	71.95
ł	197	79-51	71.60	79.20	71.94	78.80	72.20	28.57	72.53
Į	805	80.26	72.27	79.94	72.62	79.63	72.96	79-3L	73.31
ł	100	\$1,00	72.94	\$0.68	73.29	\$0.36	73.64	80.04	73.99
ŀ	110	81.75	77 60	81.43	73.98	81.10	74 35	80 78	74-67
ł	111	\$449	7427		74-63	81.84	74-99	Bilgr	75.35
	113	82.23	74-94	83.90 83.64	75.31	84.57	75.67	82.24	76.03
ŀ	113 114		75-61 76.18	84.38	75 98 76.65	83 31 84.05	76.34	82.98 83.71	70.70
	115		76 95	\$5.12	77 38	84.79	77.03 77.6g	84.45	77.18
	116		77.62	85.87	77.99		Allie or other	84.18	1
Ì	117	86.95	78.29	18.68	78.67	86-96	78.37 79.04	85.93	78.74
J	118	87.69	78.96	87 35	79-34	87.00	79.73	36.65	80.10
	Zlg.	88.43	79.63	88 09	80,01	87.74	80.42	87.38	80.78
ł	130	8q.18	80 30	88 83	20.68		81.07	88.12	81-46
-	北	Hep-	Lante	, -	Lat.	Dep.	Lat	Dep.	Lat
ŀ	Dist	4	ν, ι	4:	5,	30	7	15	1
1				47 Di	CREE				

W .	• •		15	•	36		,	-
4	Lat.	Dep.	Lat.	Dep.	Let.	Dep.	Lat.	Dep.
1	Q.73°	0.68	0.73	0.69	6.73	0.69	0.72	0.69
3	1.46 2.19.	1.36	1.46	1.37 2.05	1.45	1.38	2.17	1.38
4	4.93	2.73	2.91	2.74	2.90	2.75	2.89	2.77
5;	3.66	3.41	3.64	3.43	3.63	3.44	3.61	3.46
6	439	4.09	4-37	4:11 4:80	4·35 5.08	4.13 4.82	4-33 5.06	4.85 4.84
7	5.85	4-77 5.46	5.10 5.83	5.48	5.80	5.51.	5.78	5.53
9	6.58	6.14 6.82	8.56	6.17	. 6.53	6.20 6.88	6.50	6.22
0	7 31		7.28	7.54	7.25	7-57	7.22	6.92 7.61
11	8.04 8.78	7.5° 8.18	8.01 8.74	8 22	8.70	8.26	7.95 8.67	8.30
13	9.51	8.87	9.47	8.91	9-43	8.95	9-39	8.99
14	10.24 10.97	9.55	10.20	9-59	10.16	g.64 10.33	10.11	9.65 10.37
15	11.70	10.91	11.65	10.96	11.61	11.01	11.56	11.06
17	12.43	11.59	12.38	11.65.	12.33	11.70	12.28	11.76
1 8 19	13.16 13.90	12.28	13.11	12 33 13.02	13.78	12.39 13.08	13.00	13.14 13.14
20	14.63	13.64	14.57	13.70	14.51	13.77	14-45	13.83-
21	15.36	14:32	15.30	14.39	15.23	14-46	15.17	14.52
12 13	16.82	15.00	16.03	15.76	15.96 16.68	15.14	15.89 16.61	15.21 15.90
*	27.55	16.37	17.48	16.44	17-41	16 52	17.34	16.60
2.5	18.28	17.05	18.21	17.13	18.13	17.21	18.06	17.29
26	19.02	17.73 1 8.4 1	18.94 19.67	18.50	18.86 19.59	17.90 18.59	#8.78 19.50	17.98 18.67
17 28	20.48	19.10	20.39	19.19	20.31	19.27	20.23	19.36
29	21.21	19.78	21.12	19.87	21.04	19.96 20.65	20.95 21.67	20.05 20.75
20	21.94	20.46	21.85	20.56 21.24	21.76	21.34	22.39	31.44
32	23 40	21.14 21.82	23.31	21.93	23.49 23.21	12.03	23.12	22.13
13	24.13	22.51	24.04	22.61	23.94	32.72	23.84	12.82
14	24 87 25.60	23.19 23.87	24.76 25.49	23.30 23.98	24.60 25.39	23.40 24.09	24.50 2 9.2 8	23.51 . 34.20
16	26.33	24.55	26.22	2467	26.11	24.78	26.01	24.89
17	27.06	25.23	26:95	25.35	26.84	25.47	26.73	45.99
19	27.79 28.52	25.92 26.60	27.68 28.41	26.04 26.72	27.56 28.29	26.26 26.85	27.45 28.17	26.28 26.97
ρ	29.25	27.28	29.13	27.41	29.01	27-53	28.89	27.66
11	- 29.99	27.96	29.86	28.09	29.74	28.22	29.62	28.35
12	30.72 31.45	28.64 29.33	30.59 31.32	28.78 29.46	30 47. 31.19	18.91 29.60	30.34 31.06	29.04 29.74
13	32:18	30.01	32,05	30.15	31 92	30.29	34.78	30-43
15	32.91	30.69	32.78	30.83	32.64	30.98	32.51	31.12
10	33.64 34.37	34.37 • 32.05	33.51 34.23	31.52	33·37 34.09	31.66 32.35	33. 23 33.95	31.81 32.50
17 18	35.10	32.74	34.96	32.89	34.82	33.04	34.67	33.19
19	35.84	33-42	35.69 36.42	33.57	35.54	33.73	35.40 36.12	33.88
0	37.30	34.78	37.15	34.26 34.94	36.27 36.99.	34.42	36.84	34-58
;I ;2	38.03	35.46	37:88	35.63	37.72	35 79	37.96	\$5.96
13	38.76	36.15	38.60	36.31	38.44	36.48	38.29	36.65
;4 ;5	39 49 40.22	36.83 37.5 F	39-33 40.06	37.69	39.17 39.90	37.17 37.86	39.01 39.73	37·34 38 03
;6	40.96	38.19	40.79	38.37	40.62	38.55	40.45	38.72
17	41.69	38.87	41.52	39.06	41-35	39.24	44 57	39.42
:8	43.42	39.56 40.24	42.25 42.97	39·74 40.43	42.80	39 92 40.61	41.90 42.62	40.17
i9	43.88	40.92	43.70	41.11	43.52	41 30	43.34	41 49
74	Dep.	Lat.	Dep.	Lat	Dep.	Lat.	Dep-	Lat.
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2	44 DEGREES.										
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1	0.72	0.69	-0.72	0.70	0.74	0.70	1.42	0.70 1.41	0.71 1.41		
3	1.44 2.16	1.39 2.08	1.43 2.15	1.40 2:09	1:43 2:14	2.10	2.13	2.11	2.12		
1	2.88	2.78	2.87	2.79	285	2.80	2.84	2.82	2.83		
45	3.60	3.47	3.58	3.49	3.57	3.50	3.55 4.26	3.52 4-22	4-24		
6	4.32 5.04	4.17 4.86	4.30 5.01	4.19	4.28 4.99	4.21 491	4.97	4-93	4.95		
8	5.75	5.56	5.73	5.58	5.71	5.61	5.68	5.63	5.66		
9 10	7.19	6.25	6.45 7.16	6.28 6.98	6.42 7.13	6.31 7.01	6.39 7.10	6.34 7.04	6.36 7.07		
11	791	7.64	7.88	7.68	7.85	7.71	7.81	7.74	7.78		
12	8.63	8.34	8.60	8.37	8.56	8.41	8.52	8.45	8.49		
13	9.35	9.03 9.73	931	9.07. 9.77	9.27 9.99	9.11 9.81	9.23	9.15 9.86	9.90 9.19		
15	10 79	10.42	10.74	10.47	10.70	10.51	10.65	10.56	10.61		
16	11.51	11.11	11.46	11.16	11.41	11.21	11.36	11.26	11.31		
17	12.23	11 81	12.18 12.8g	11.86	12.13	11.92. 12.62	12.07	11.97 12.67	12.02		
19	19.67	13.20	13.61	13.26	13.55	13.32	13.49	13.38	13.44		
20	14.39	13.89	14.33	13.96	14.27	14.02	14.20	14.08	74-14		
21 22	15.83	14.59	19.04 15.76	14 6 5 15.35	14.98	14.72	14 91	14-78	14-85 15.56		
23	16.54	15.98	16.47	16.05	16.40	16.12	16.33	16.19	16.26		
24	17.26	16.67	17.19	16.75	17.12	16.82	17.04	16.90 17.60 ¹	16.97 17.68		
25	17.98	17.37	18.62	18.14	18.54	18 22	18.46	18.30	18.38		
27	19.42	18 76	19.34	18.84	19.26	18.92	19.17	19.01	19.09		
28	20.14 20.86	19.45	20.06	19.54 [.] 20.24	19.97 20.68	19.631	19.8 9 20.60	19.71 20 .42	19.80 20.51		
29 30	21.58	20.15	29.77 21.49	20.93	21 40	20 33, 21.03	21.31	31.12	21.21		
31	22.30	21.53	22:21	21.63	22.11	21.73	22.02	21.82	21.92		
32	25.02	22.23	22.92	22.33	22.82	22.43	22.73	22.53	22.63 23.33		
33, 341	23.74	23.92 23.62	23.64	23.03° 23.72°	23.54	23.13. 23.83	23.44	z3.94	24-04		
35,	25.18	24.31	25.07	24.42	24196	<u>44.53</u>	24.86	24.64	124.75		
36	-25.90	25.01	25.79	25.12	25 68	25.23	25.57	25.34 · 26.05	25-46 26.16		
37 38	26.62	25.70 26.40	26.50 27.22	25.82° 26.52	26.39 27.10	25.93 26.63	26.28	26.75	26.87		
39	28.05	27.09	27.94	27, 21	27.82	27.34	27.70	27.46	27-38 28.28		
40	28.77	27.79	28 65	27.91	28.53	28.04	28.41	28.16	28.99		
42	29:49 - 30 21	28.48 29.18	29.37 30.08	28. 61 29.31	29.24 29.96	28.74 29.44	29.12 29.83	29.57	29.70		
43*	130.93	29.87	30.80	32.01	30.67	30.14	30,54,	30.27	30.41		
44 45 1	31.65	30.56 31.26	31.52	30.70	31.38 32.10	30.84 . 31-54	31.25	30.98. 3:.68	31.11 31.82		
46	33 09-	31,95	32 95	32.10	32.81	72.24	32.67	32.38	32 53		
47	33.81	32.65	33.67	32.80	,33·52	32 94	33-38	33.09	33.23		
48 49	34.53 35.25	33.34 34.04	34.38	33.49	34.24	33.64	34.09 34 80	33.79 34.50	33. 94 34 6 5		
50	35.97	34 73	35 82	34.89	34 9 5 3 5 6 6	34·34 35.05		35.20	35.36		
51	36.69	35.43	36.53	35.59	36.38	35.75	36.22	35 90	36.06		
52	37.41	36.12 36.82	\$7.25 37.96	36.29 36.98	37.80	36.45	36.93 37.64	36.61 37.31	36.77 37.48		
53 54	38 84	37.51	38.68	37.68	38.52	37.85	38.35	28:02	38.88		
55	39:56	38.21	39.40	38.38	39.23	38.55	39.06	18.72	38.89		
56	40.28	38.90 39.60	40. 11 40. 83	39.08 5 9.77	39.94 40.66	39.25	39.77	39-42 40-13	39.60 40.31		
57 58	41.00 41.72	40.29	41.55	40.47	41.37	39.95 40.65	40.48	40.83	41.01		
59	42.44	40 98	42.26	41.17	42.08	41-35	41.90	41.54	41.72 42.43		
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TABLE 6.

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50 55 60 65 70	6 5 4 4 5	9 10 11 13	2 44 2 53 3 2 3 10 3 19 3 27	35	5 5 5 15 5 39 6 4 6 27	21 2 3 4 6 7 8 3 2 3 4 5 6 7 31 2 3 4 5 6 6 4 2 3 4 5 5 6 5 2 3 4 6 8
80 85	0	16 16 17 18	3 36 3 42 3 50 3 57 4 4	60 70 80	7 3 1 8 3 9 6 9 3	1

TABLE 10.

The Semi-diameter of the Sun.

	-				*			
Mosta	Day	Sun's Semi-di-	_	Day.	Sun's Semi-di.	Mesth	Day	Sem's Semi-di-
January.	7 13 19	16' 19' 26 19 26 19 16 18 16 17	May.	7 13 19 25	15/54" 15/53 25/53 25/54 15/54 25/54		7 13 19 25	15 56 15 58 15 59 16 8
Behruary	7 23 29 26	16 16 16 15 16 14 16 23 16 23	June	1 7 译版	15 49 25 48 15 47 15 47 15 47	October.	7 23 29 25	16 3 16 4 15 5 15 8 16 9
March	7 33 19.5	16 10 16 9 16 7 16 8 16 4	July.	7. 13 19 25	15 47 15 47 15 47 15 48 15 48	Nov ember.	7 13 19 25	16 18 16 13 16 14 16 15 16 16
Apel	7 72 19	16 1 16 t 15 59 15 \$7 15 \$6	August.	1 7 13 19	15 49 15 50 15 51 15 52 15 53	December, Nov	1 7 13 19	16 17 16 18 16 18 16 19 16 19

TABLE 11.

Apparent Time of Transit of Pole Star.

This table is adapted to leap year; particularly 1808. In order to make it serve for other years, the time of transit must be taken for the day following that given in the months of January and February. For the first year after leap year, one minute is to be added to the time of transit given in the table; two minutes for the second, and three minutes for the third after leap year.

Again, to reduce this table to a different meridian than that to which it is adapted, viz. Greenwich; if the longitude is between 45° E, and 45° W, there is no correction to be applied. If the longitude is between 45° and 135° E, one minute is to be added; but if it is between 45° and 135° W, one minute is to be subtracted. If the longitude is between 135° E, and 180°, two minutes are to be added, but subtracted if the given longitude is between 135° W, and 180°.

This table is useful to find the time when the altitude of the pole star ought to be observed, to find the latitude by its meridian altitude; it is

also useful in finding the variation of the compass by the pole star.

P	J	an.	Feb).	M	larc	A	oril.	M	ay.	IJ	ine.	ιJυ	ıly.	Ā	ug.	Se	pt.	0	ct.	IN	ov.	I)cc
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12	5	20	_	2	1	23	11	33	9	37	7	32	5	28	3	26		34	11	41	9	41	7	34
13	_	16	-	8	I	20	11	20	9	33	7	28	5	24	3	23	1	30	11	•	9	37	7	30
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25	4	25	2 2		0	36	10	42	80 80 80 80	46	6	38	4	36	2	39		47	10	52	8		6	36
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Difference of Altitude of the Pole Star and the Pole, at different distances of the Stur from the Meridian.

As the pole star is generally known, that no opportunity, therefore, may be lost for determining the latitude, this table is inserted, the use of which is as follows:—

Find the interval between the time of observation of the altitude of the pole star, and that of its passing the meridian, and take out the corresponding equation from the table; which added to, or subtracted from the true altitude of the pole star, will give the latitude of the place of observation.

EXAMPLES.

I. Let the corrected altitude of the pole star be 46° 10' N, observed 8h. 30' before its passage over the meridian. Required the latitude?

True altitude of the pole star - 46° 10′ N. Equation from table 12 to 8b. 30′ - + 1 5

Latitude - - 47 15 N.

II. At 1h. 10' after the passage of the pole star over the meridian, its altitude corrected was 58° 51' N. Required the latitude?

True altitude of the pole star - 58° 51' N. Equation from table 12 to 1h. 10' - 1 42

Latitude - 57 9 N.

TABLE 12.

Difference of Altitude of Pole Star and Pole.

Argument. Distance of the Star from the Meridian, in Sidereal Time
Subtract.

Min.	0	Hour.	1	Hour.	2	Hours.	13 F	lours.	4	lours.	5 E	lours.													
0	1	46'9	1"	43'3	10	32,6	10	15'6	00	53.4	00	27.7	60												
5	1	46.9	1	42.7	1	31.4	I	13.9	0	51.4	0	25.4	55												
10	1	46.8	E	42.0	I	30.2	I	12.2	0	49.4	0	23.2	50												
15	1	46 7	1	41.2	1	28.9	I	10.5	0	47.3	0	20.9	45												
20	1	46.5	I	40.4	I	27.6	I	8.7	0	45.2	0	18.6	40												
25	. 1	46.3	1	39.6	1	26.2	I	6.9	0	43.1	0	16.3	35												
30	I.	46.0	E	38.8	I	24.8	1	5.1	0	40.9	0	14.0	30												
35	1	45.7	1	37.9	1	23.4	1	3.2	0	38.8	0	11.6	25												
40	1	45.3	1	36.9	1	21.9	X	1.3	0	36.6	0	9.3	20												
45	1	449	I	35.9	I	20.4	0	59.4	0	34.4	0	7.0	15												
50	1	44-4	1	34.8	I	18.8	0	57.4	0	32.2	0	4-7	10												
55	I	43.9	1	33.7	1	17.2	0	55.4	0	29.9	0	2.3	5												
60	1	43.3	I	32.6	I	15.6	0	53.4	0	27.7	0	0.0	0												
	11	Hours	10	Hours.	9 1	lours.	8 H	lours	7 H	lours.	6 H														

Sun's Declination for the Years 1868, 1812, 1816, 1820.

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EXPLANATION AND USE OF THIS TABLE.

The Declination of the Sun is an arch of a meridian contained between its centre and the equinoctial, which arch is reckoned in

degrees, minutes, &c.

In the first quadrant of the ecliptic, from about the 21st of March, to the 21st of June, the Sun's declination is North, and increasing; and in the third quadrant, between the 22d of September and 21st of December, the Sun's declination is South, and increasing In the second quadrant of the ecliptic, from about the 21st of June to the 22d of September, the Sun's declination is North, and decreasing; and in the fourth quadrant, between the 21st of December and the 21st of March, the Sun's declination is South, and decreasing; which will be readily perceived by inspecting the table.

In this table, the Sun's declination is given, from the year 1808 to 1823 inclusive, calculated for the instant of noon, each day, at

Sun's Declination for the Years 1809, 1813, 1817, 1821.

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2	22	56	_	50	-	14	4	53	15		22	11	23	5		50	8			31	14	43	21	58
3	22	51	16	33	6	51	5		15			18	_		17	3 5	l .	38		54	15	2	22	7
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19	20	22	11	18	0	36	11		19	44	-	27	20	55	i e	52	1	33	9		19	27	23	26
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the Meridian of Greenwich, or the meridian, at which we begin to reckon the Longitude. It is to be taken out with the month at the top, and the day in the left hand column, at the same time, noting whether it be North, or South, as expressed at the top of each column. The declination being here given to the nearest minute, it will be found sufficiently exact tor the most common and useful problems, wherein it is concerned.

The sun's declination is necessary to find the latitude, whether at sea or land, from the meridian altitude observed; it is also requisite for finding the latitude from two altitudes observed with the interval of time measured by a watch; it serves for computing the sun's azimuth, having his altitude and the latitude of the place given, in order to find the variation of the compass; it is required, jointly with the latitude of the place and the sun's horary angle, to compute his altitude, if neglected to be observed at the time of taking the moon's distance from the sun for finding the longitude, being itseful to facilitate the calculation of the effect

Sun's Declination for the Years 1810, 1814, 1818, 1822.

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3		52	_	3 7		57	5	10	15	33	22	10	23	3	17	39	1	43				58		5
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13	21	33	13	28	•	4	8	55	18	17	23	12	21	55	14	50	3	58	7	38	17	53	23	9
14	21	22	13	8	2	40								46	14	31	3	35		0	18	9	23	13
15	21	11	12	47	2	16	9	38	18	47	23	19	21	37	14	13	3	12	8	23	18	25	23	16
16	21	0	12	27	1	53	9	59	19	1	23	21	21	28	13	54	2	49	8	45	18	40	23	19
17	20	49	13	6	1	29	10	20	19	14	23	23	21	18	13	35	2	26	9	7	18	55	23	22
18	20	37	11	45	1	5	10	42	19	28	23	25	21	8	13	16	2	2	9	29	19	10	23	24
19	20	25	11	24	0	42	11	2	19	41	23	26	20	57	12	56	I	39	9	51	19	24	23	26
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23	19	31	9	57	0	53	12	24		30		27	20	12		37	0	6	11	17	20	18	23	27
24	19	17	9	35	1	17	18	44	20	42						_		18			20	30	23	27
25	19	_3	9	13	1	40	13	4	20	<u>53</u>	23	25	19	47	10	56	0	41	11	59	20	42	23	25
26	18	48	8	50	2	4	13	23	21	4	23	24	10	34	10	35	1	5	12	20	20	54	23	24
27	18	33		28		27.		43	21		23		19	20		14		28	12 12	40	21	5	23	22
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of refraction and parallax upon the distance; it is also necessary to calculate the apparent time from an obsered altitude of the sun at a distance from the meridian, the latitude being given; or to compute the time of the sun's setting or rising; which, though a less accurate method than the former of obtaining the time, may yet be useful when that cannot be had. For any of these purposes the sun's declination must be found to the time given nearly, reduced to the meridian of Greenwich, making proportion according to its daily increase, or decrease, by the help of table 14, as in the following examples.

1st Required the Sun's Declination at noon in New-York, in Longitude 74° 8' West, on the 1st of April, 1811.

Dec. for April 1st, 1811, at Greenwich, in Tab. 13 = 4° 18' N. Equation for Long. Table 14. = +4 50"

. Required Declination = 4° 22′ 50″.N.

Sun's Declination for the Years 1811, 1815, 1819, 1823.

, 00	Jan Feb			h. J	M	ar.	Ap	ril.	M	2V.	Ju	ne.	Ju	lv.	Au	g.	30	ept	O	:t.	No	v.	1)e	c.
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		48		24	•_	40	_	28	15		22	22	22	58	17	27	7	27	4	6	15	12	22	11
5		41		6		17	5	50	16	4	22	29	22	52	17	11	7	5	4	29	15	31	22	19
6	32	35		47	5	53	6	13	16	31	22	36	22	47	16	55	6	42,	4	52	15	49	22	27
7	22	27		39		30	_	36		38	22	42	22	41	16	38	6	20	5	15	16	7	22	34
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	21	54	14	13	3	57	8	5	17	43	23	3	22			30	4	49	6	47	17	16	22	58
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N. B. To find the equations in Table 14,—seek the Sun's declination to the nearest degree in the top line of the table; then, under this declination and against the given Lon. in the left hand column, is found the equation for Lon. and in the same column with the dec. and against the given time from Noon, in the right hand column, is found the equation for time; both which equations must be added, or subtracted, according to the directions at the head of the Table.

2d Required the Sun's Declination on the 1st of May, 1811, at 5 h. 48 min. P. M. in Longitude 72° W.

When Sun's dec. increases.

Add in W. lon. | Add af. noon. | Sub. in W. lon. | Sub. af. noon.

Sub. in E. lon. | Sub. be. noon. | Add in E. lon. | Add be. noon.

5	Sub. i	n E. lo	n.	Sub. be	.noon.	Add	in E. l	on.	Add bo	e. noon-
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Ì	15	0 59	0 59	1	0 57	0 56	0 55	0 54	0 53	1 0
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Į	30	r 58		' ' '	1 54	1 51	1 49	1 48	1 45	2 0
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ı	36	2 22	2 2	1	1 '	2 14	2 12	2 10	2 6	2 24
1	39	2 33	2 3	•	2 39	2 25	2 23	2 20	2 16	2 36
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1	90	5 53	5 5	- /			5 29	5 23	5 16	6 0
1	93	6 5	_	6 0		5 46	5 41	5 34	5 27	6 12
1	96	6 17 6 28	6 1	1 -		5 57 6 8	5 52 6 3	5 45	5 37	6 24
1	99	6 40	6 39		1	6 19	6 14	5 56 6 7	5 48 5 58	6 36 6 48
1	105	0 52	6 5	6 46	6 39	1		6 17	6 9	6 48 7 d
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1	144	9 25	9 23	9 18	9 8	8 55	8 46	8 37	8 26	9 36
	147	9 37	9 35	•	,	9 6	8 57 9 8	8 48 8 58	8 36 8 47	9 48
- 4	150	9 48	9 45			9 17				10 0
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	156 159	10 24		10 16	10 5	•	9 41	_		10 24 10 36
1	162	10 36	10 33	10 27	10 16	10 1	9 52	9 42		10 48
1	165		10 44				10 3	9 52	9 39	0 11
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When Sun's dec. increases. When Sun's dec. decreases.

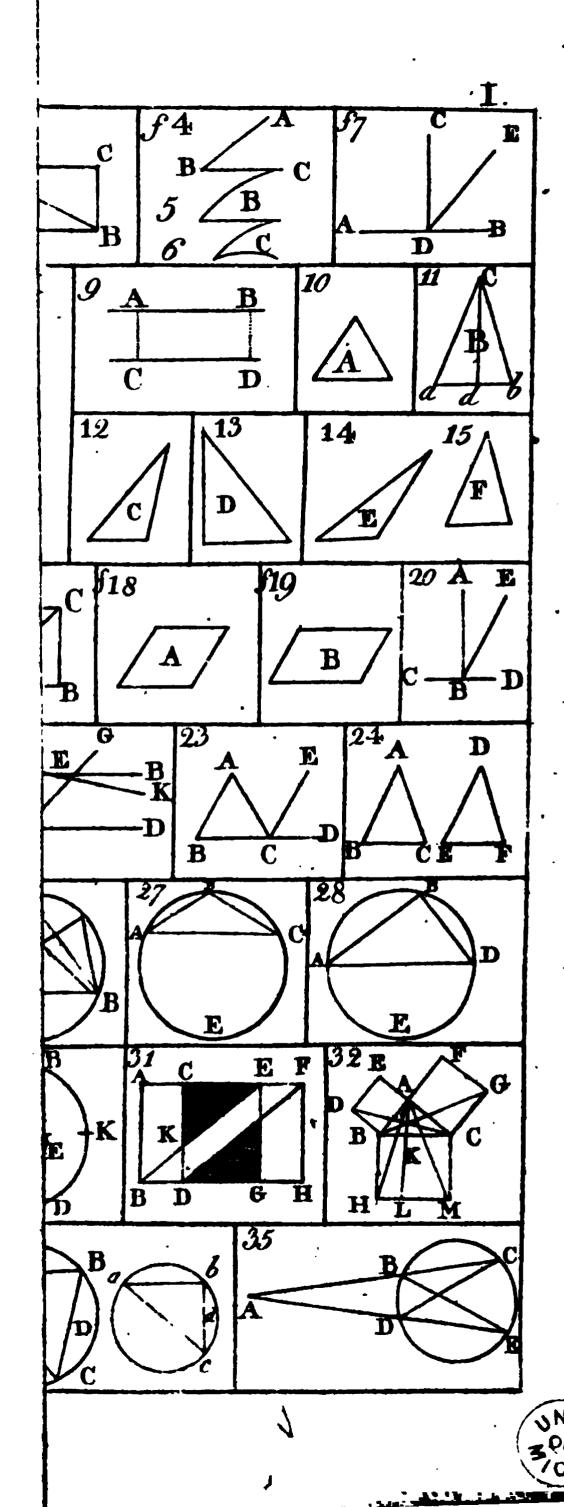
Add in W lon. Add af. noon. Sub. in W lon. Sub af noon.

Su in E. lon. Sub be noon Add in E lon. Addbe noon.

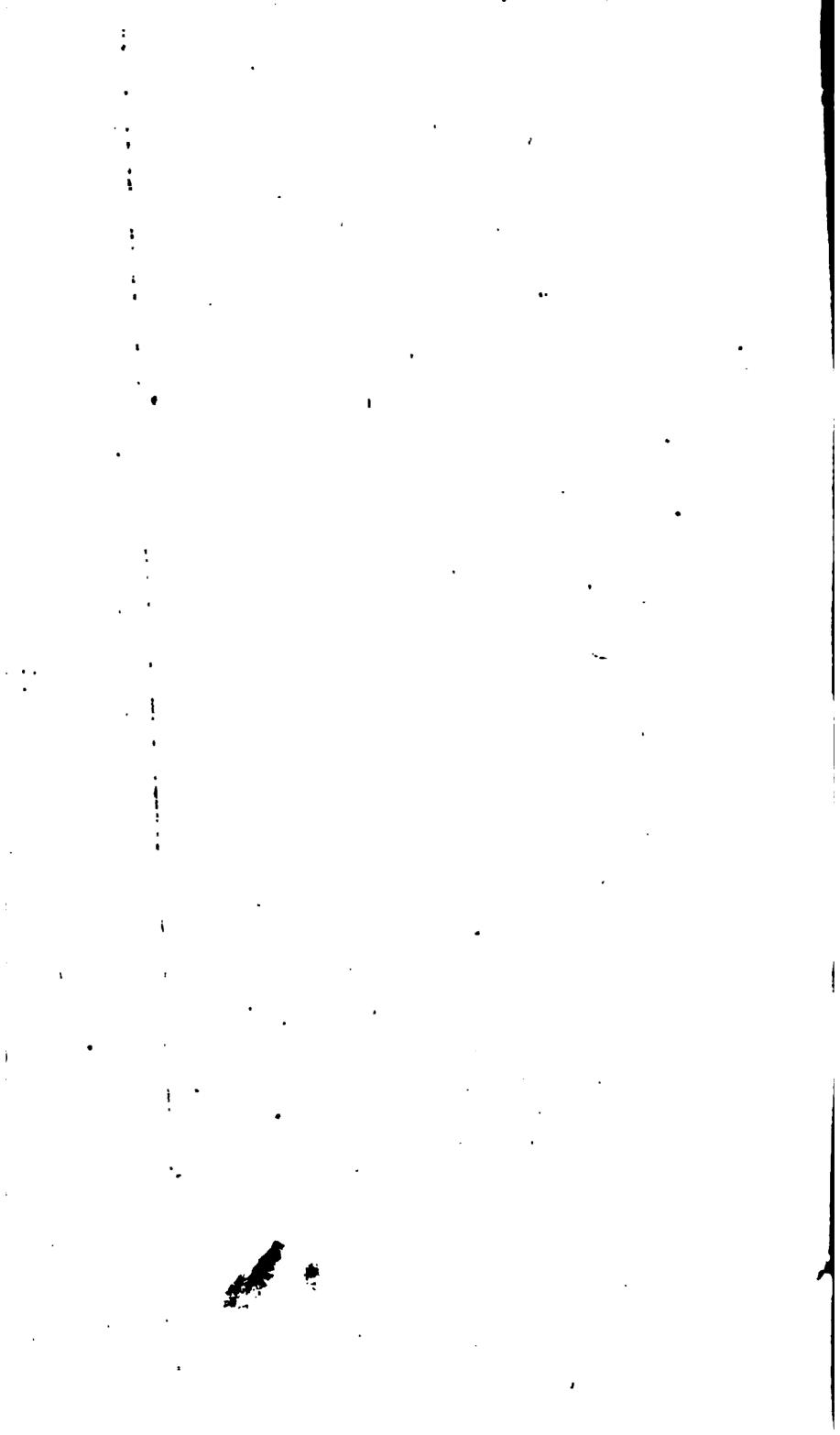
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	156	8	54	8	34	3	21	8	0	7	39	7	13	6		6	11	10	2.1	
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When Sun's dec. decreases.

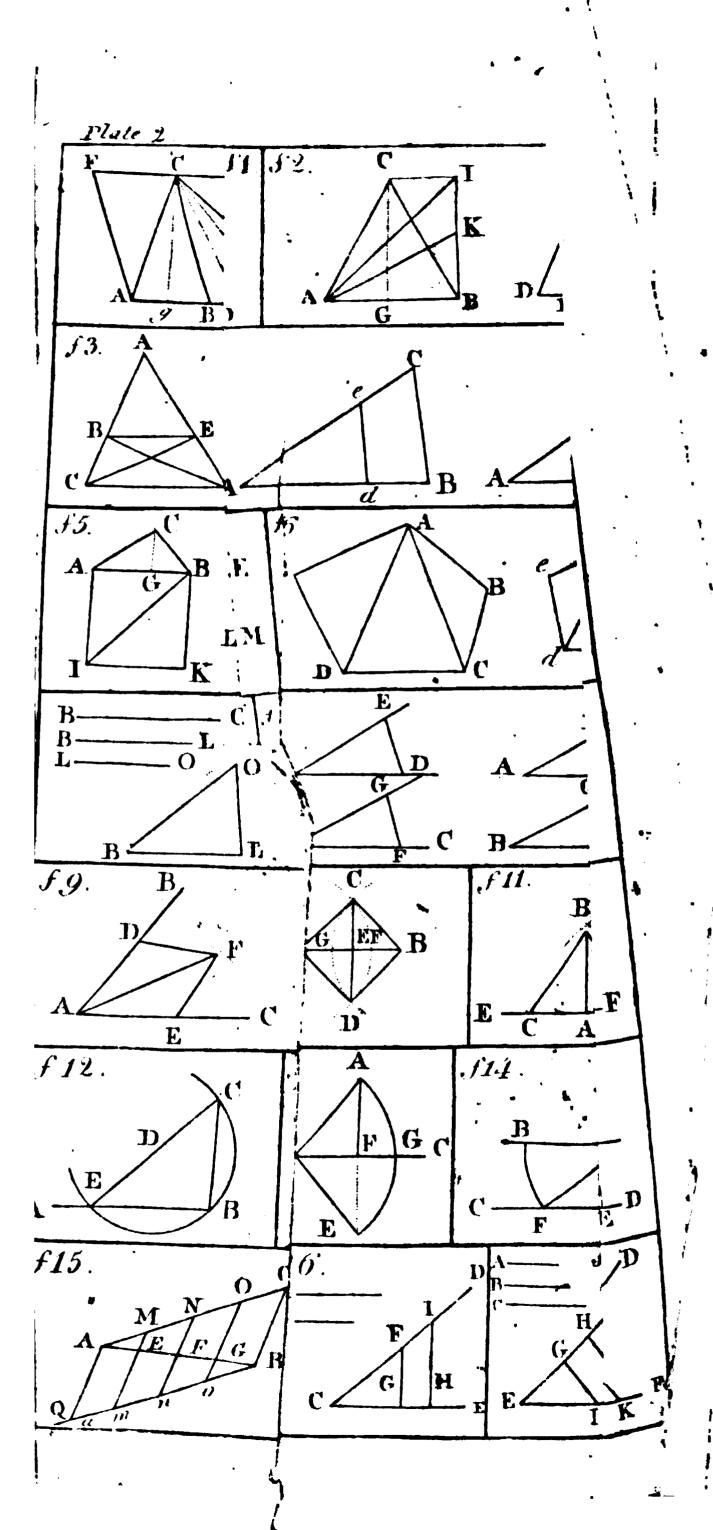
When Sun's dec. increases.

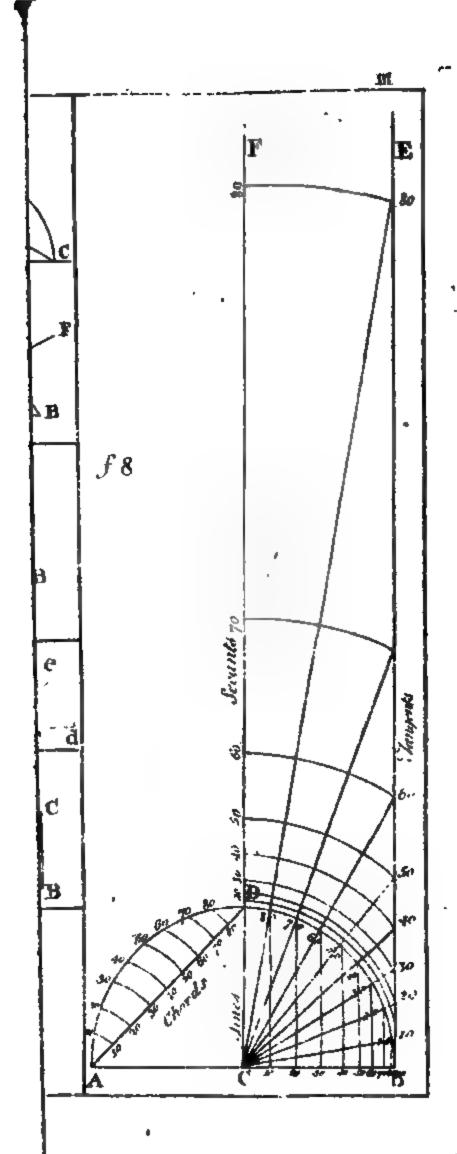




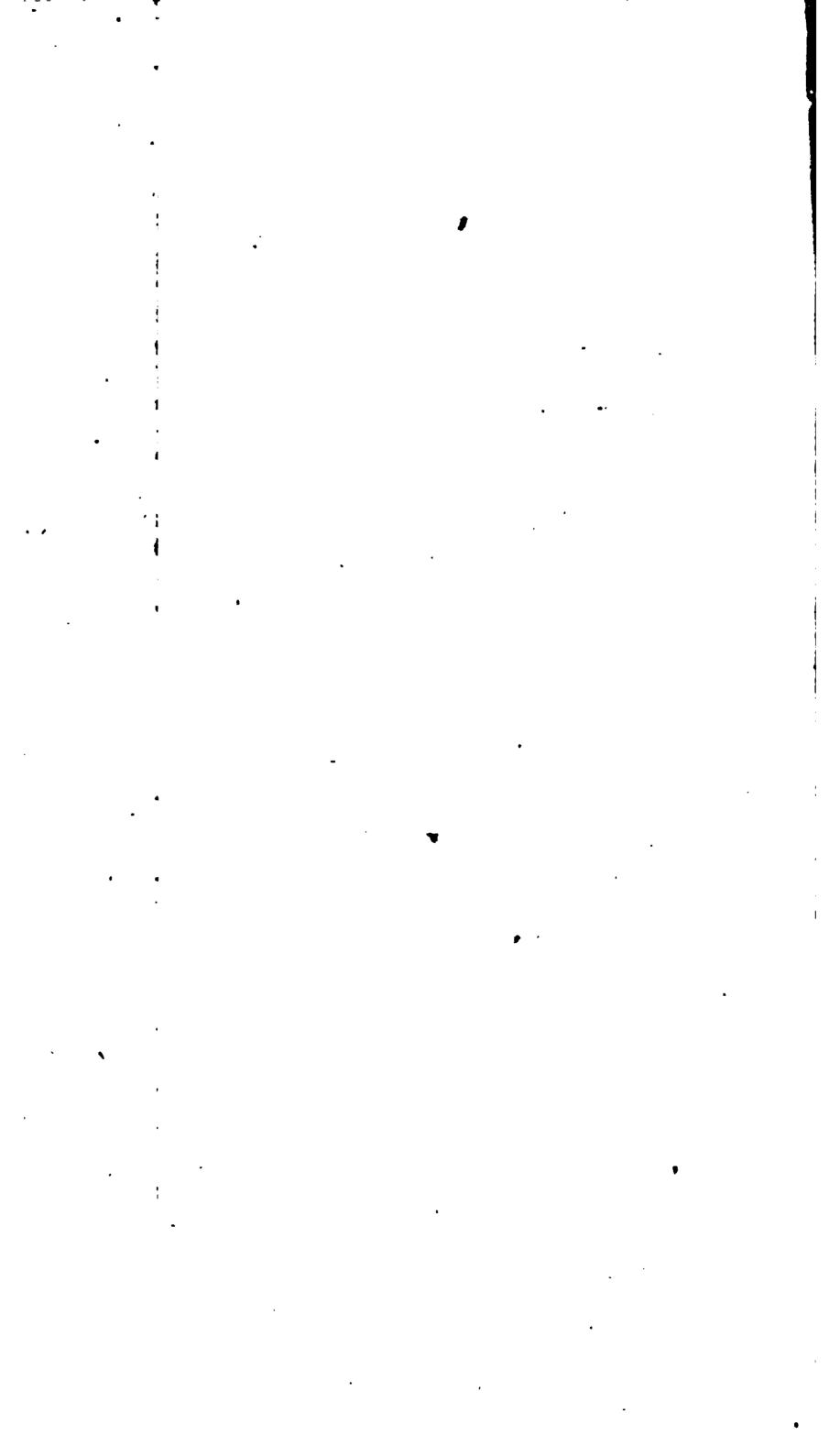


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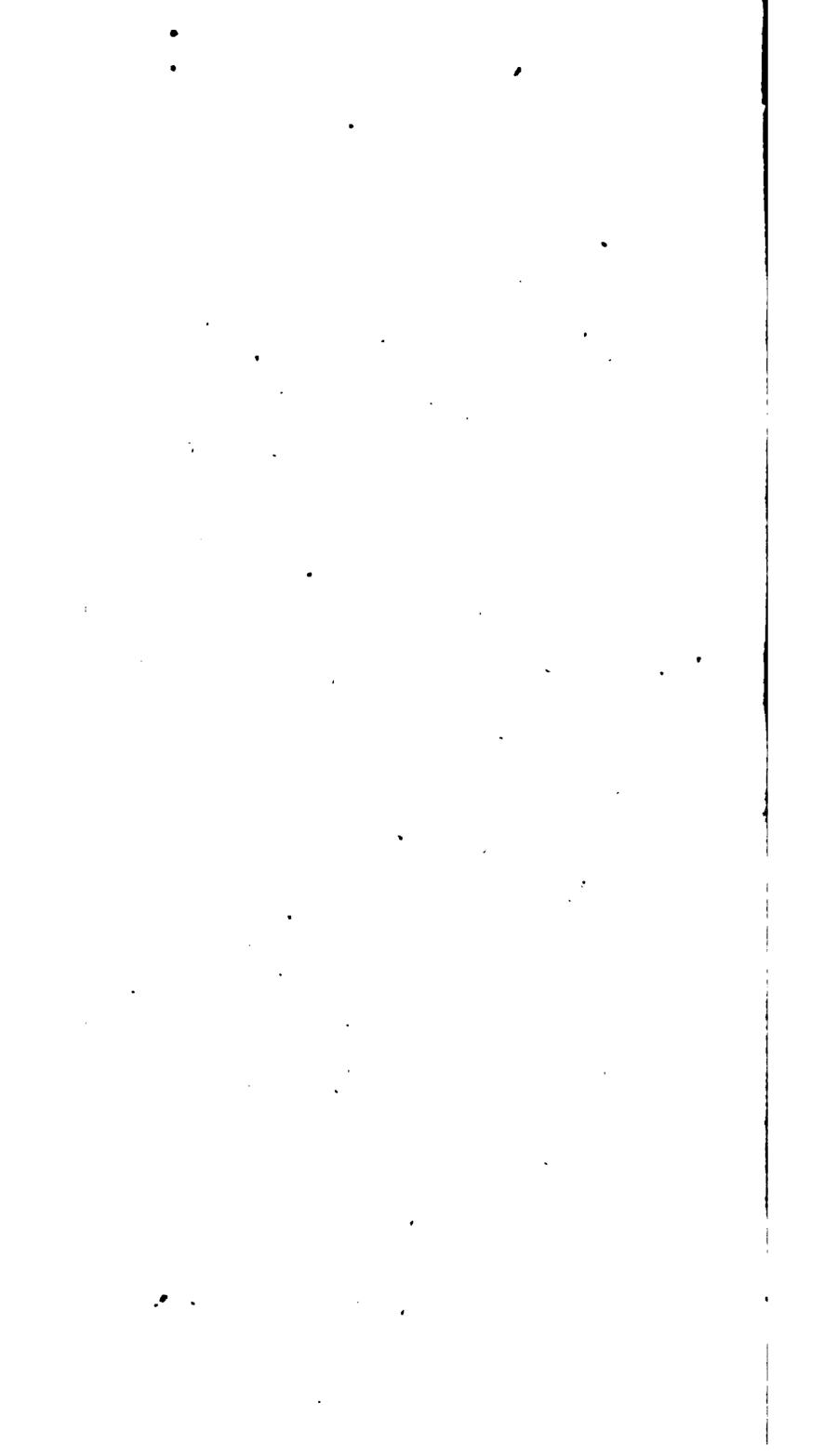


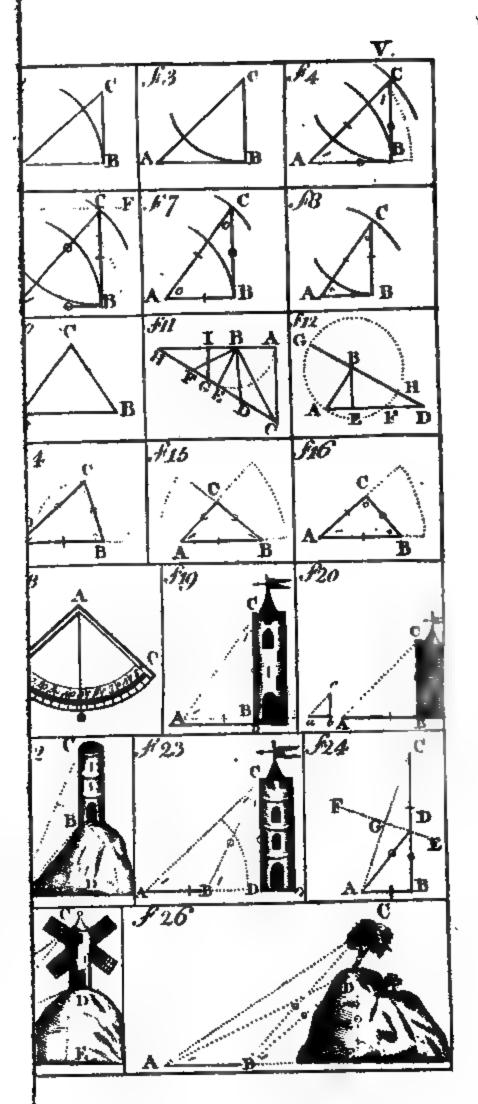
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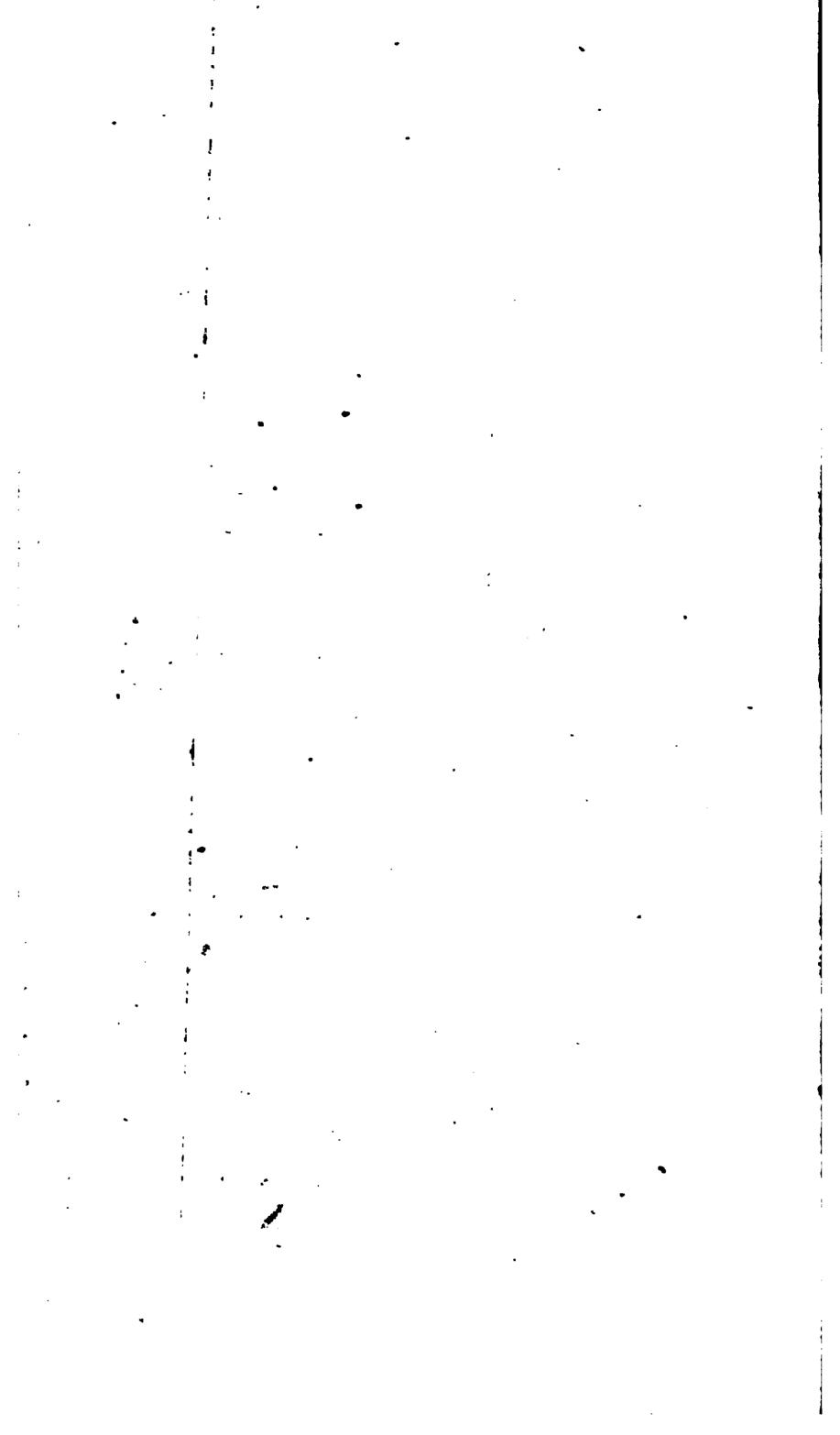
The Proportions for the Solution of 6 lases of Right Angled Plain Trangles TA AC R AB Se'C AC TC AB Sa'C'AC..R'BC Jan A. A.C. TA BC R: AC: SA: BC R: ac :: SC : AB Case 1. ं धिट्र B SA: BC: SC: AB × SA:BC::R:AC TC AB: SecCAC TA ·BC :: Ja·A·AC TA'BC..R.AB TC:AB::R:BC Car 3. TA AB.R :: AC: Sec A AC:R::BC: SA R'AC :: SC : AB BC:R::AC:SecC R:AB::TA:BC R:BC::TC:AB · Case 5.

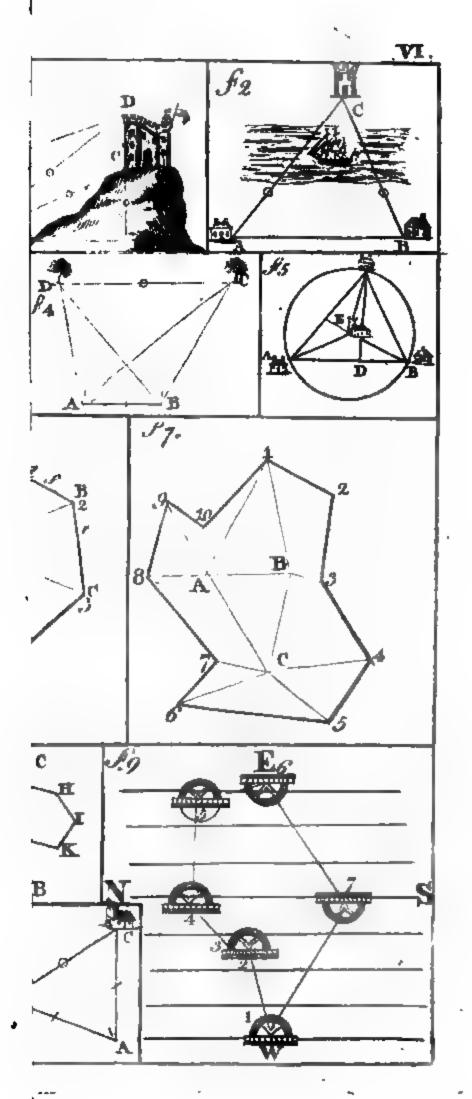
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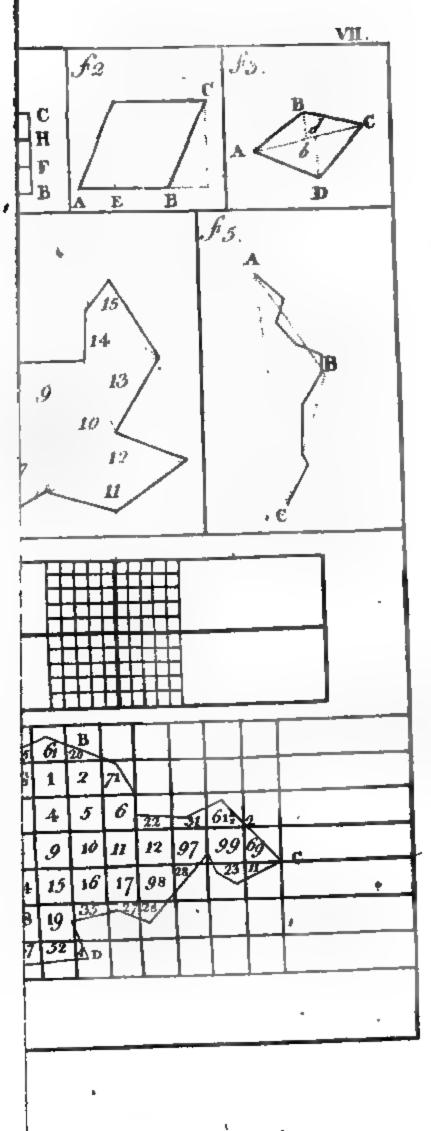






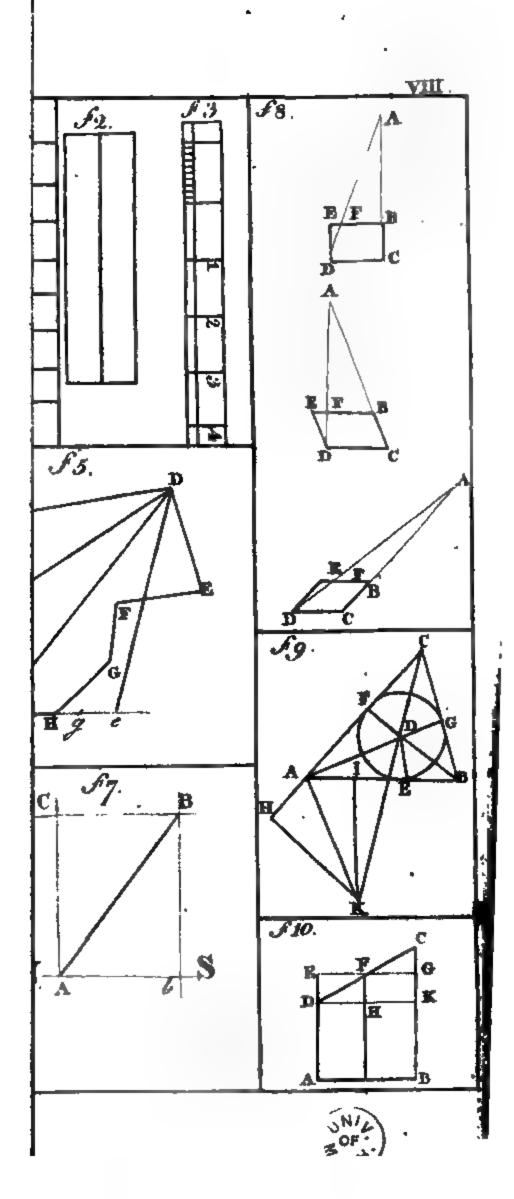


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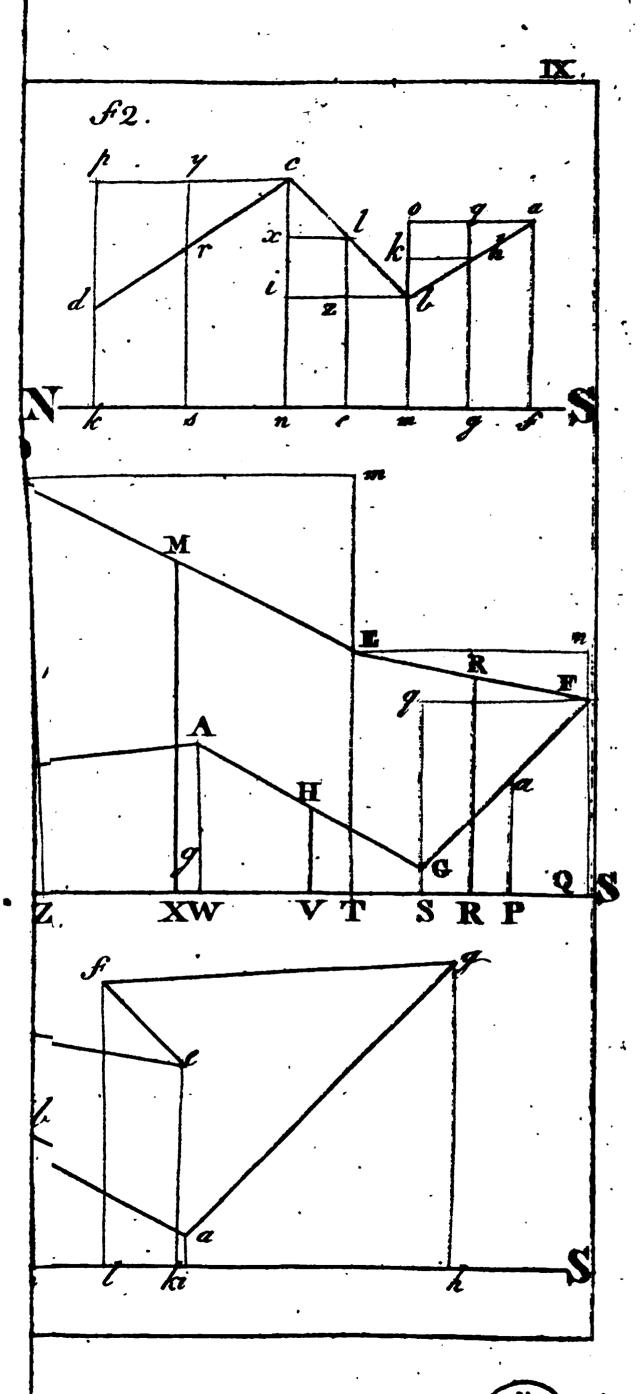
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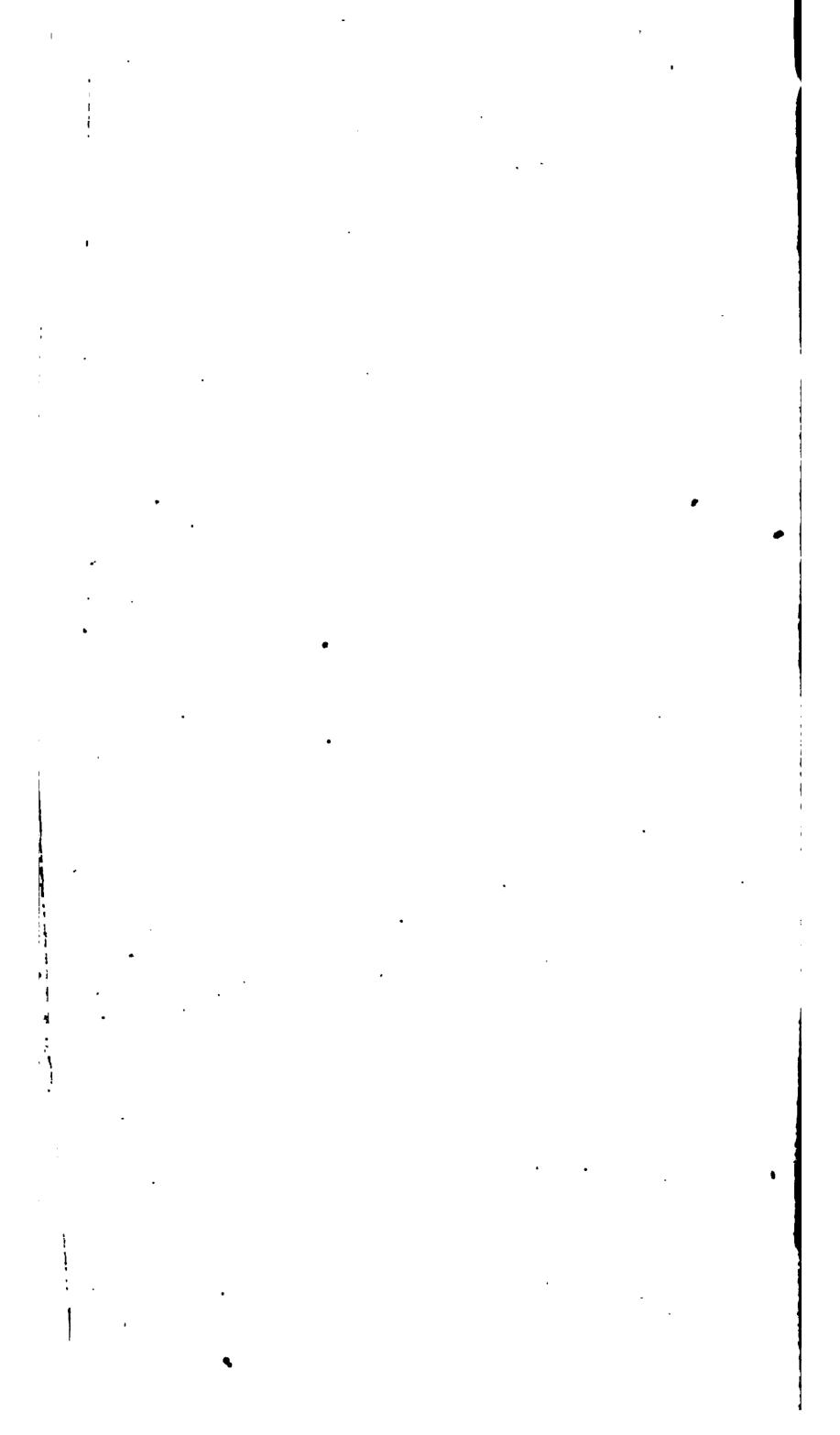


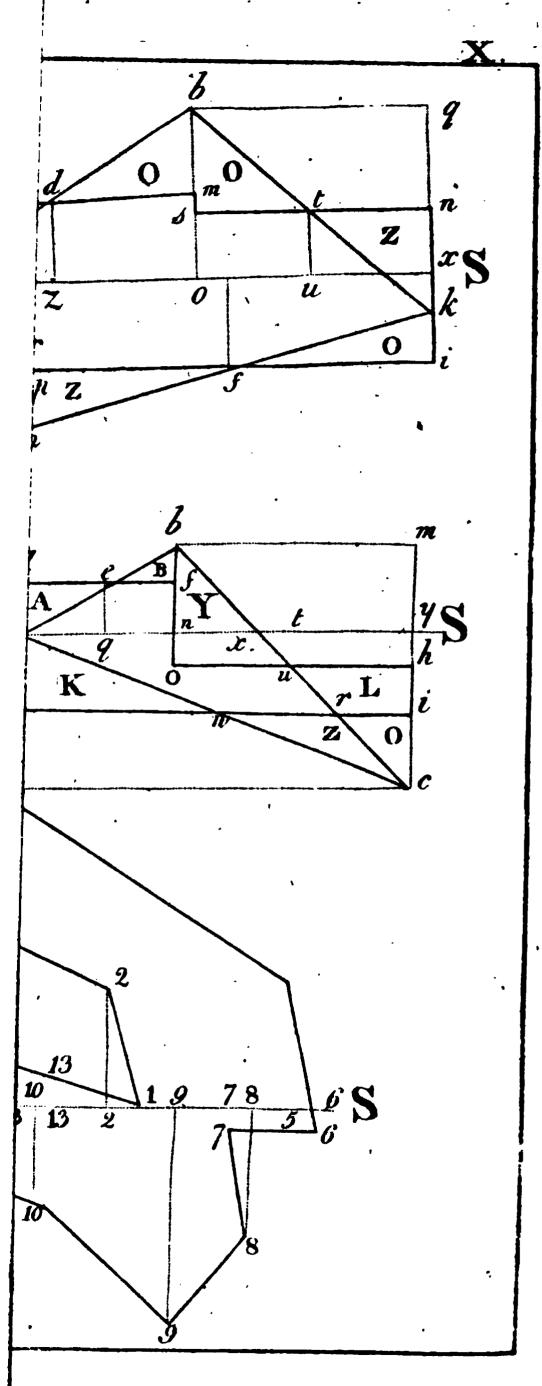
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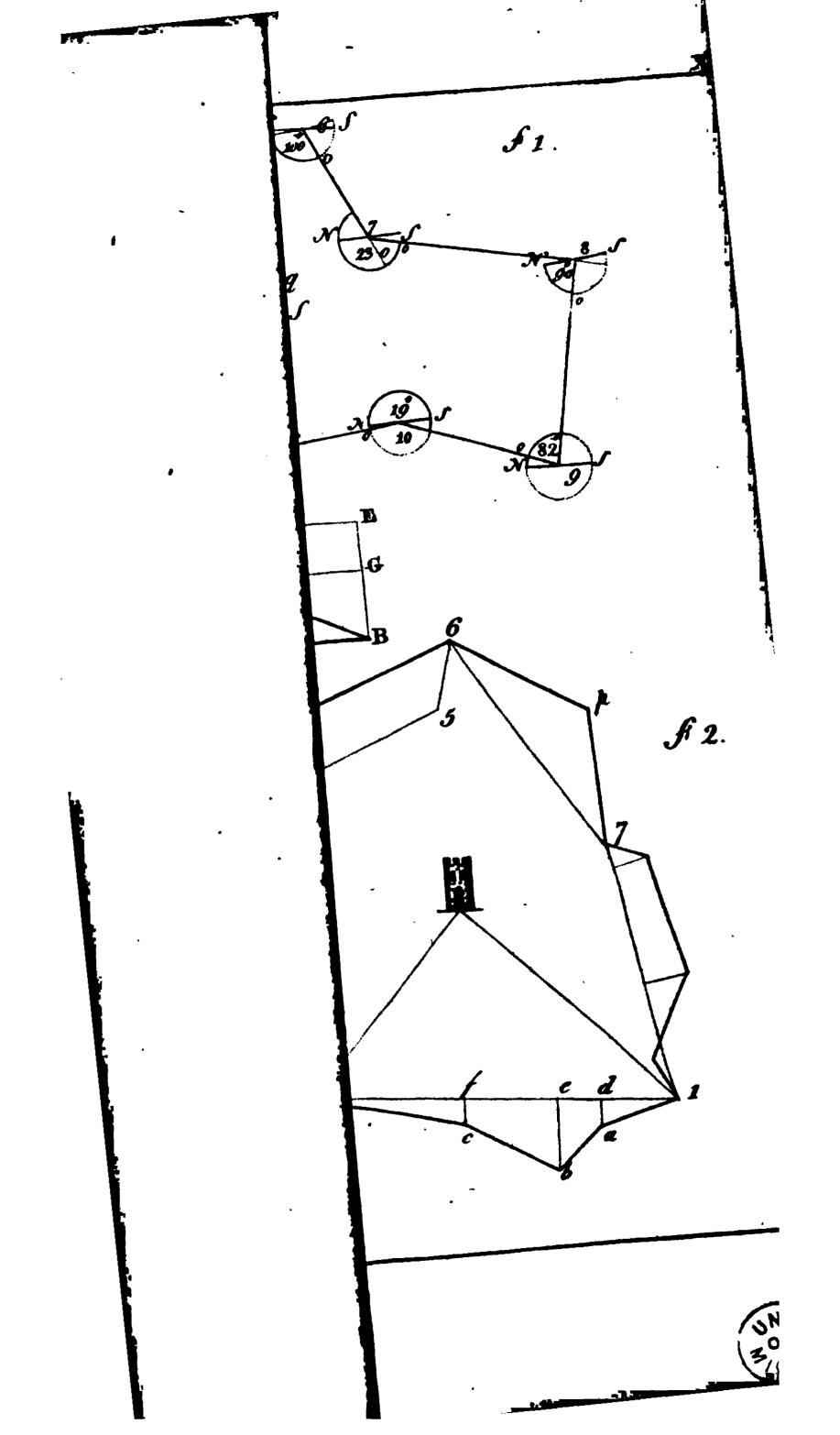
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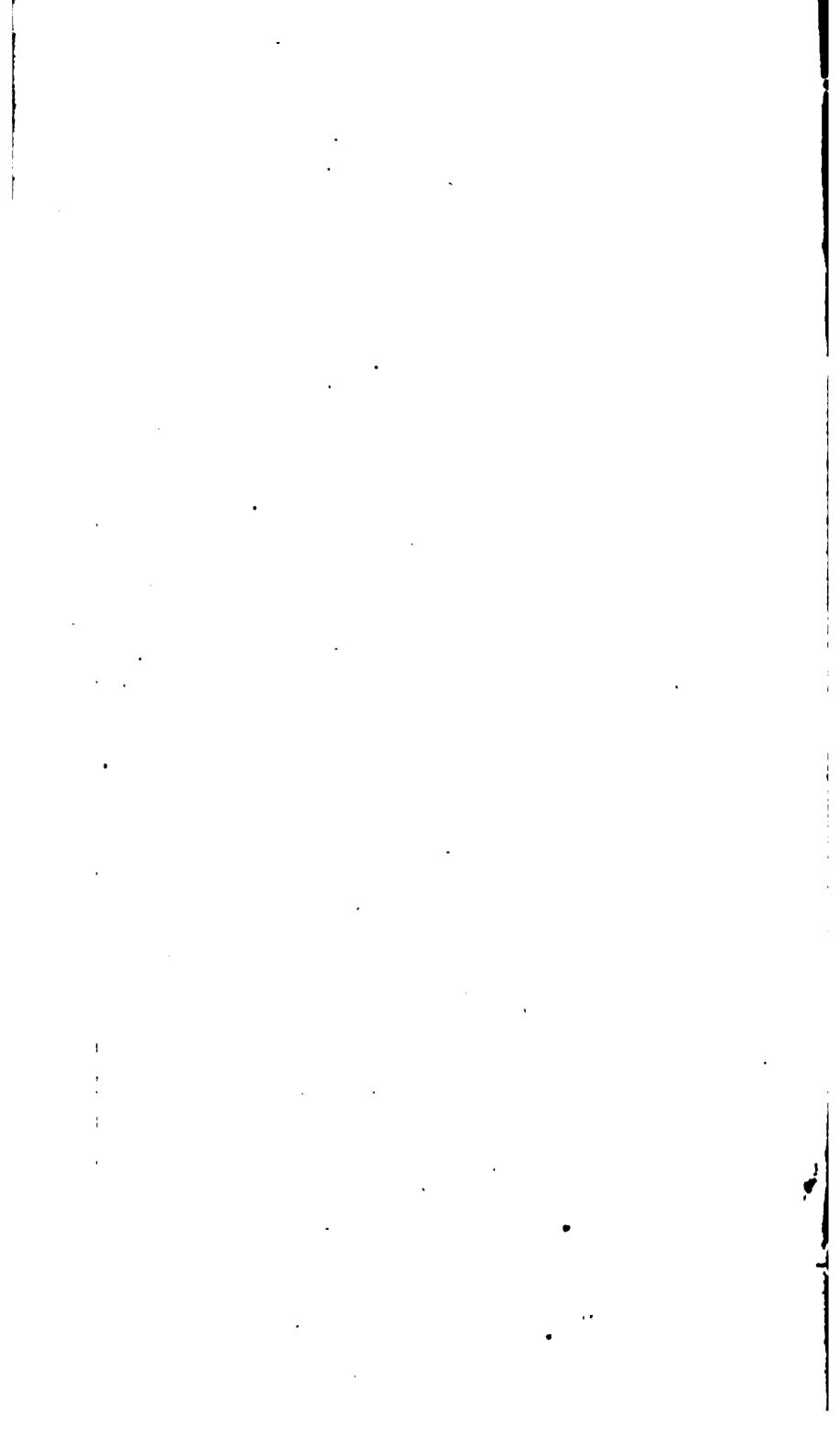




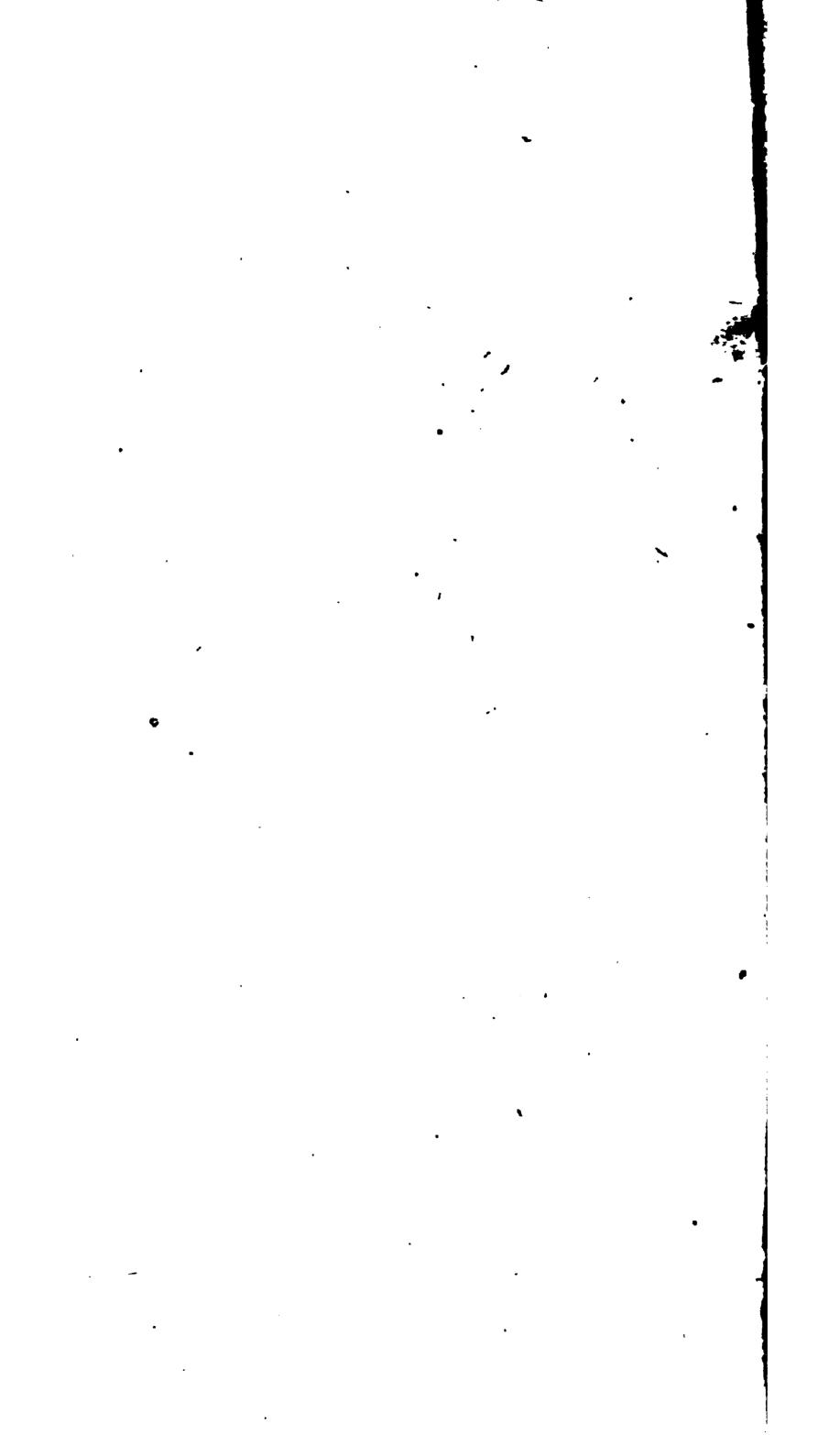
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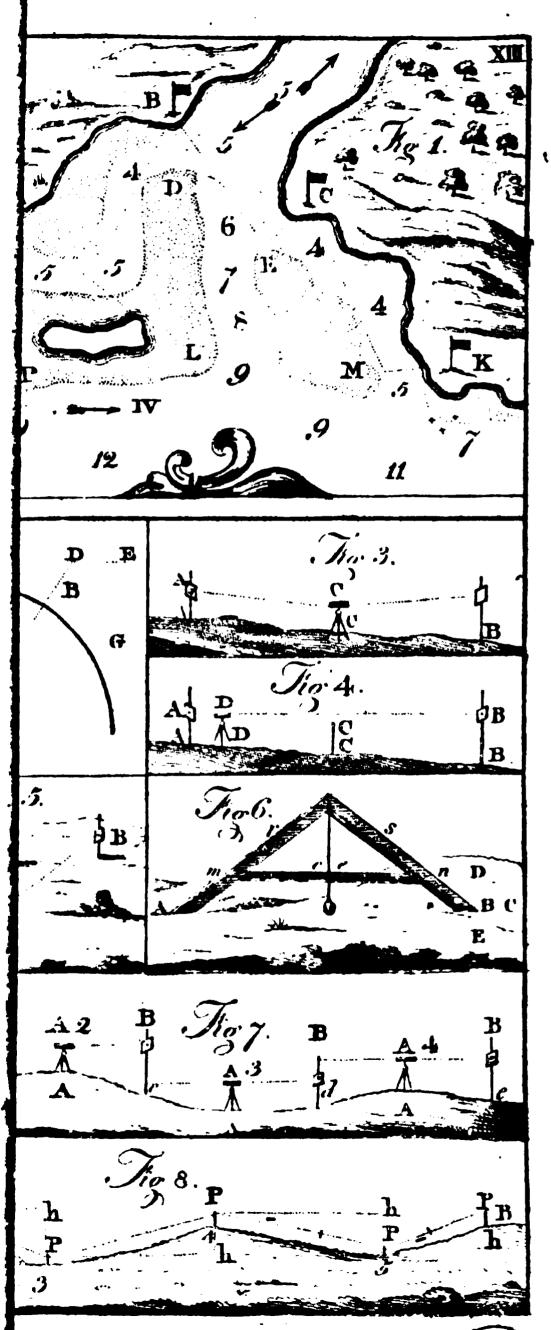
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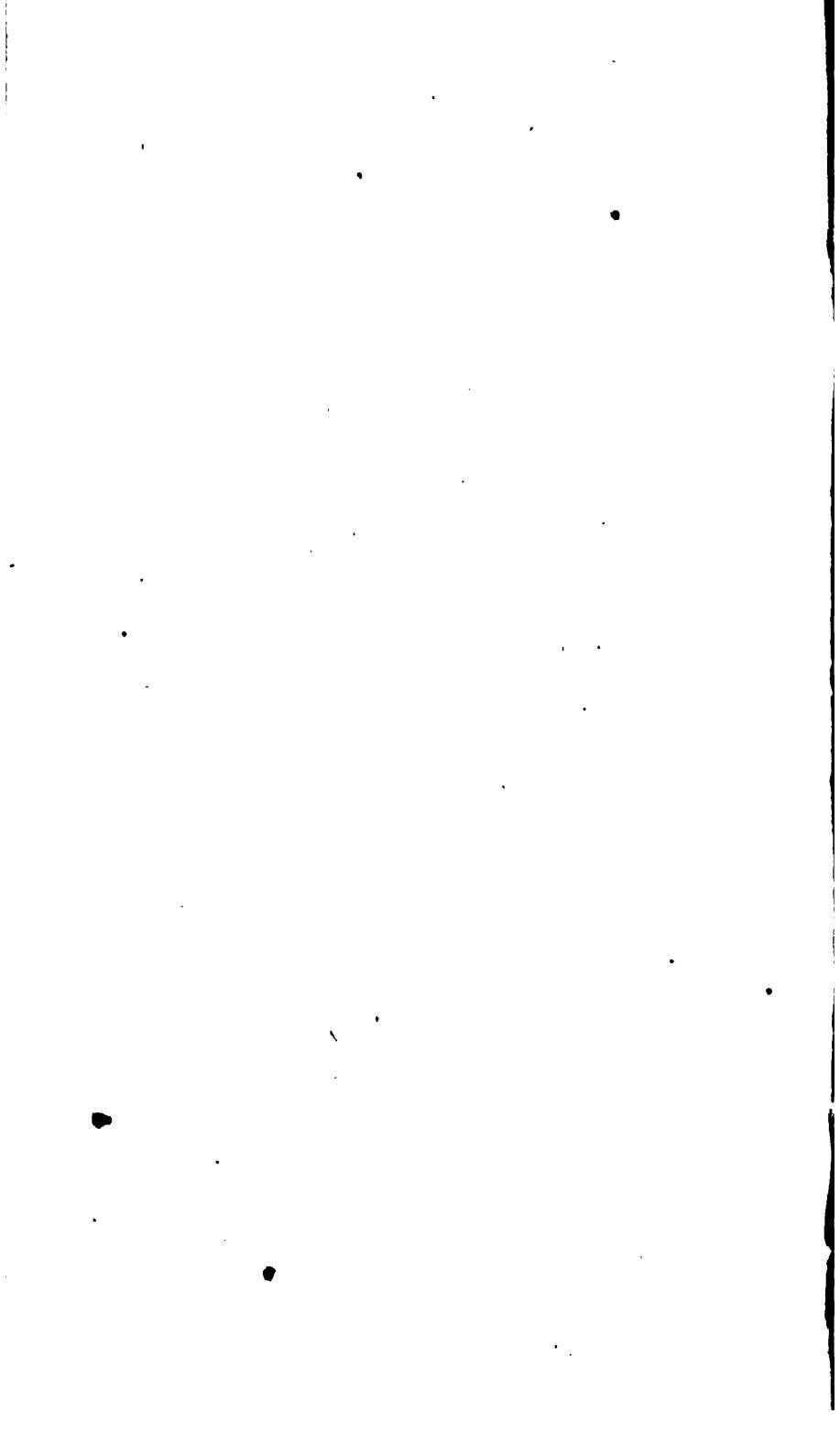




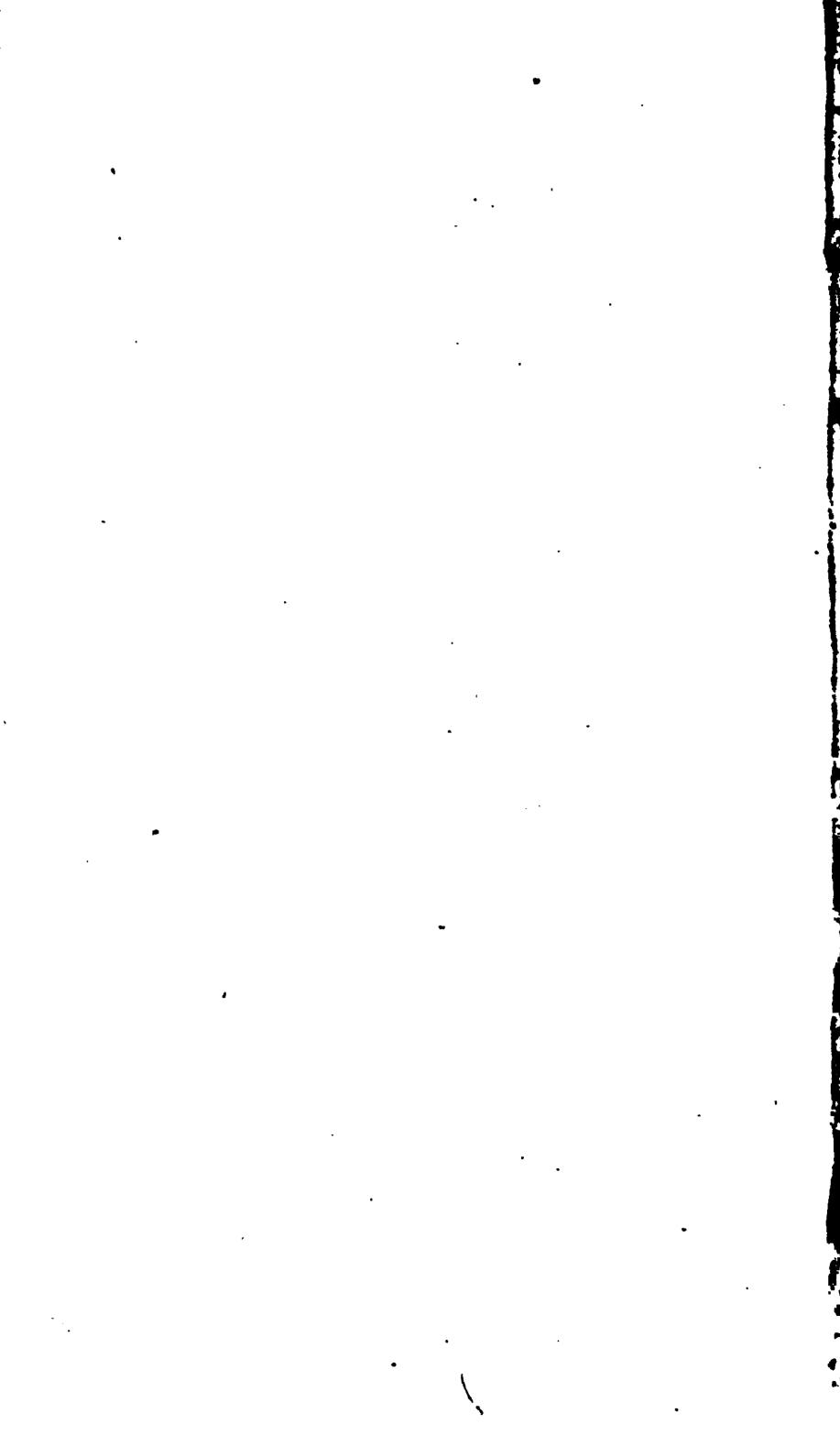
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